

Plastics and Composites under Dynamic Loading From Deformation To Failure

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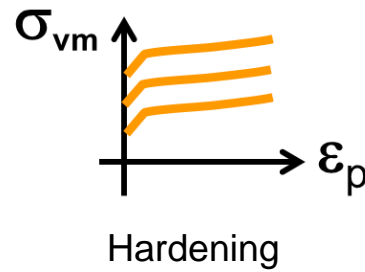
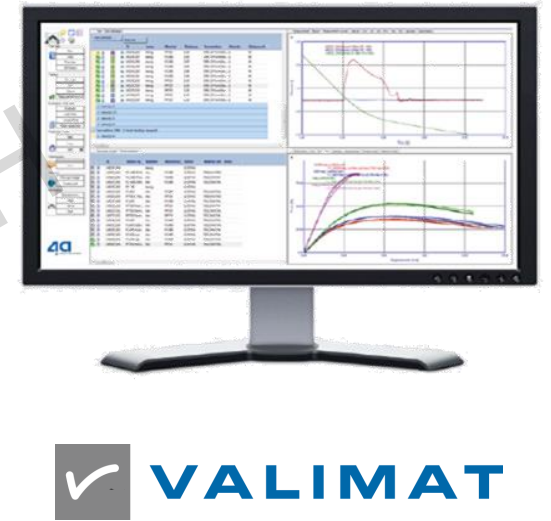
JSOL CORPORATION

7th Resin-Composite Analysis Seminar

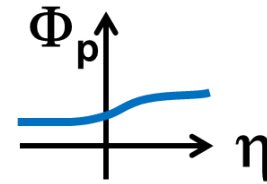
24th January, Nagoya, Japan

Outline

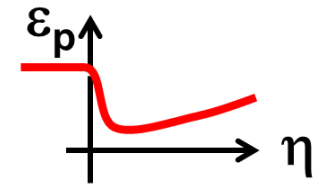
- Introduction
- Thermoplastic materials
- SFRT & LFRT
short and long fiber reinforced thermoplastics
- Composites
- Outlook / Summary



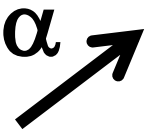
Hardening



Triaxiality



Damage/Failure



Anisotropic

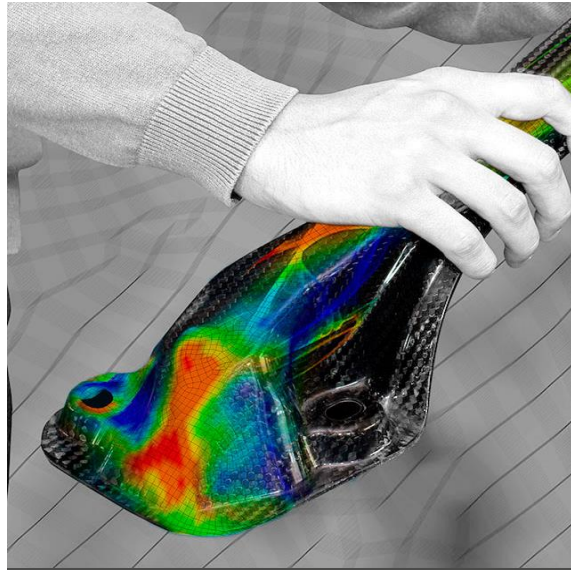
excellence in
plastics&simulation
testing equipment
lightweight products



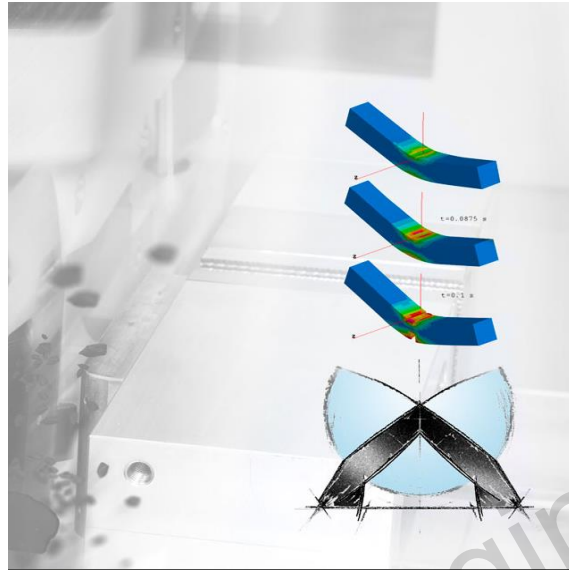
excellence in
plastics&simulation
testing equipment
lightweight products



4a business units



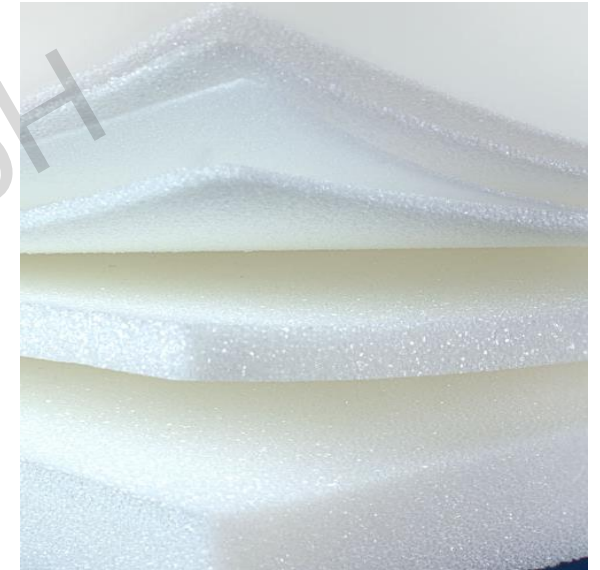
4a engineering
Engineering and simulation for plastic products and composites



Impetus
Testing equipment generating material data for the dynamic simulation of plastics



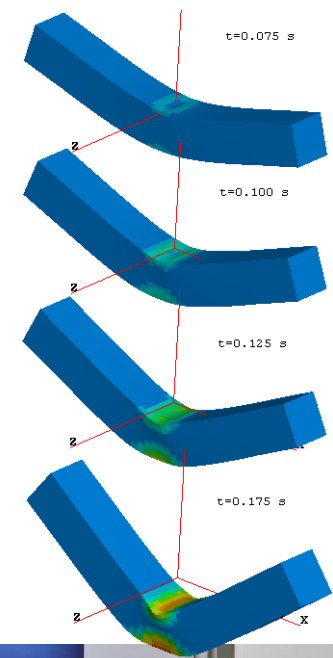
4activeSystems
Dummies and testing facilities for active vehicle safety



4a manufacturing
Specialized thin foams and multi layer materials

Material characterization - services

- efficient high-dynamic testing
- dynamic material behaviour
- plastics, foams, composites, ...
- **validated material cards ready to use for your crash-simulation**



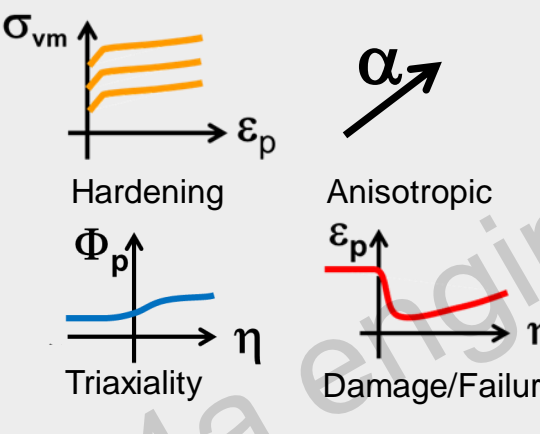
Intelligent reliable solutions for plastics, composites, metals, foams, ...

IMPETUS



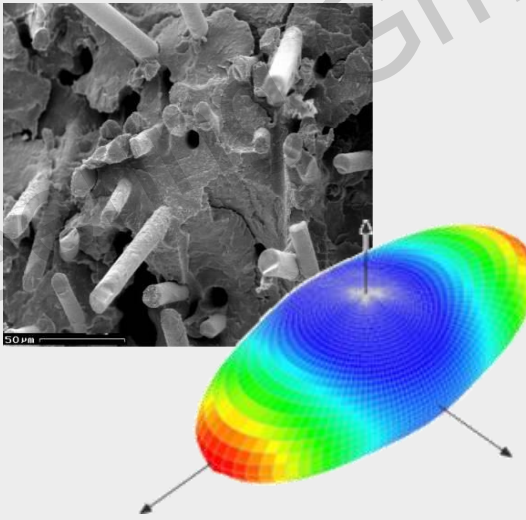
efficient dynamic testing

VALIMAT



from test to validated material cards

MICROMECH



3D anisotropic material cards

FIBERMAP



individual mapping process information

Intelligent reliable solutions for plastics, composites, metals, foams, ...

◀ **IMPETUS**

✓ **VALIMAT**

◉ **MICROMECH**

➔ **FIBERMAP**

Foams

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

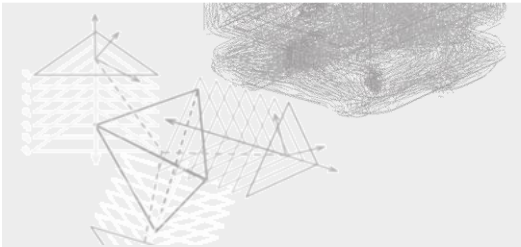
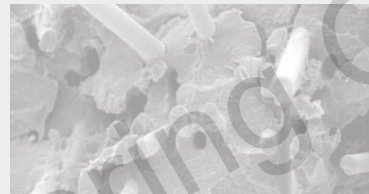
Metals

efficient
dynamic testing

from test to validated
material cards

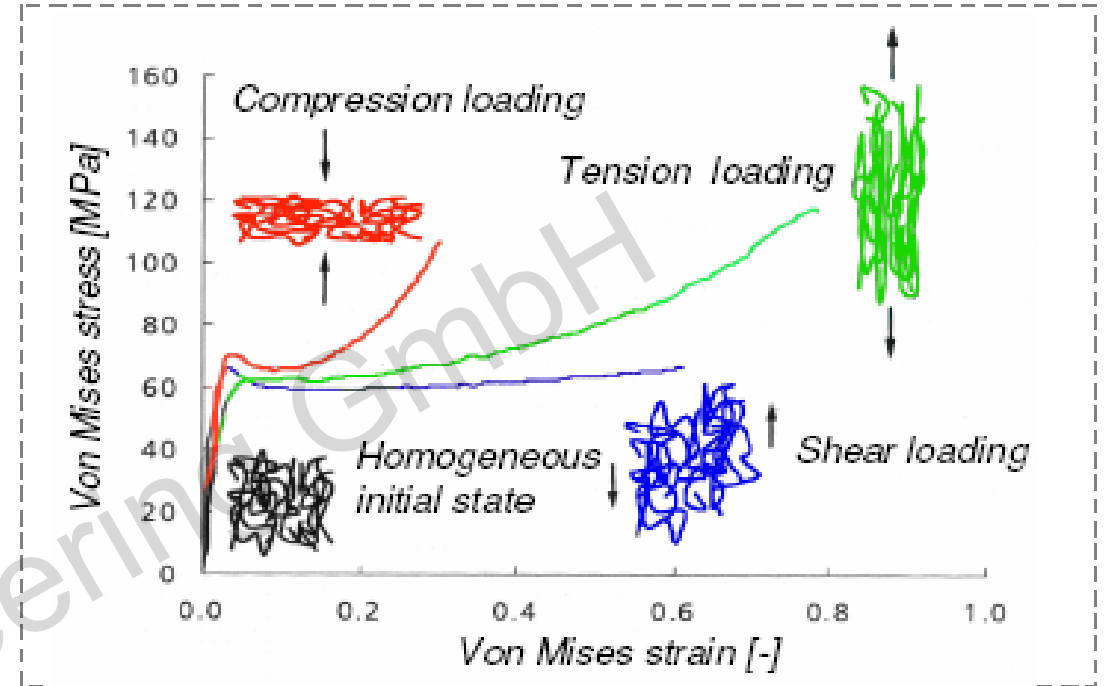
3D anisotropic
material cards

individual mapping
process information

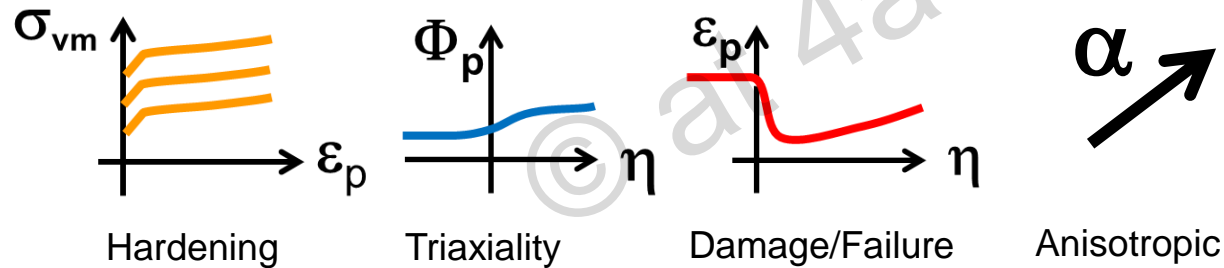


Thermoplastic materials

- Motivation
- Material and failure models
- Material characterization
 - IMPETUS™ - dynamic impact tensile testing
 - typical test results PP T10
- First validation results

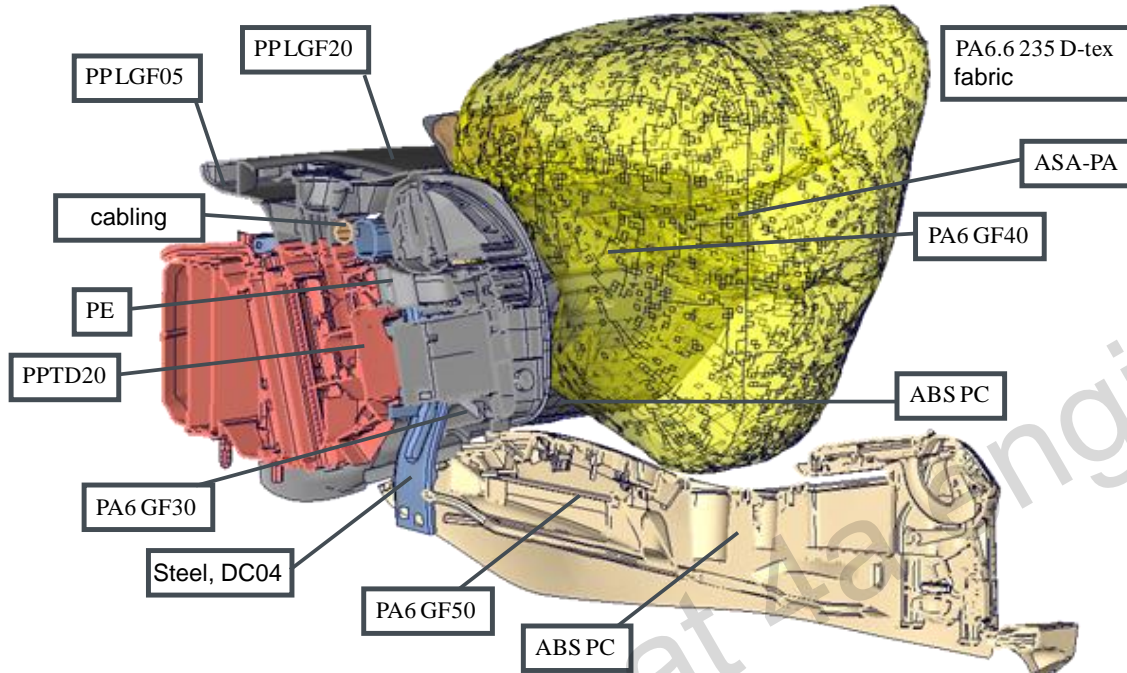


Source: Mechanik der Kunststoffe W. Retting, Hanser Verlag 1991



Motivation

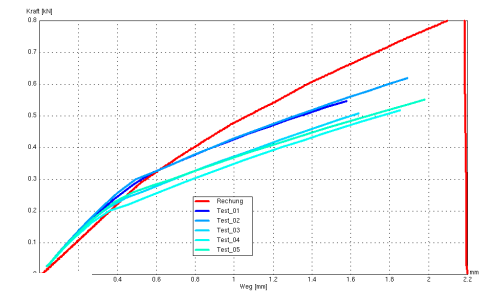
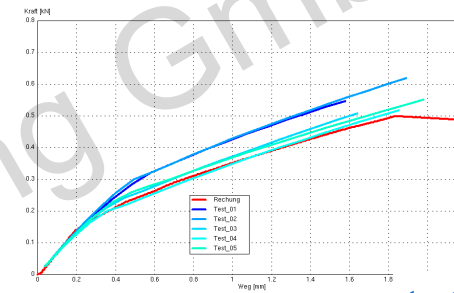
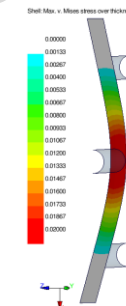
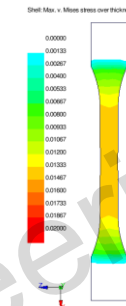
material variety



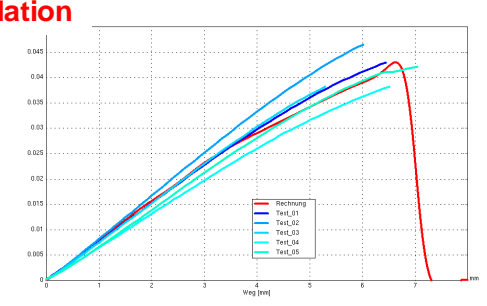
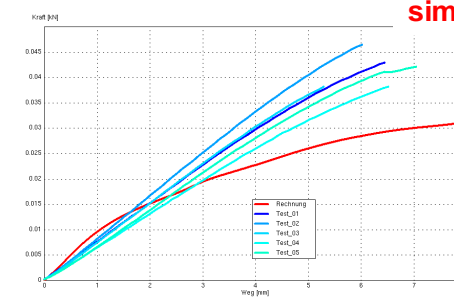
bending load case

original test curve tension

scaling 1.25



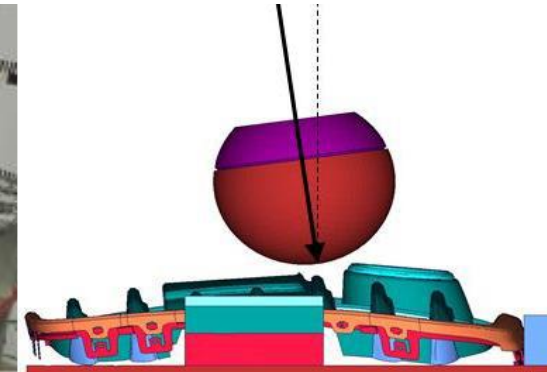
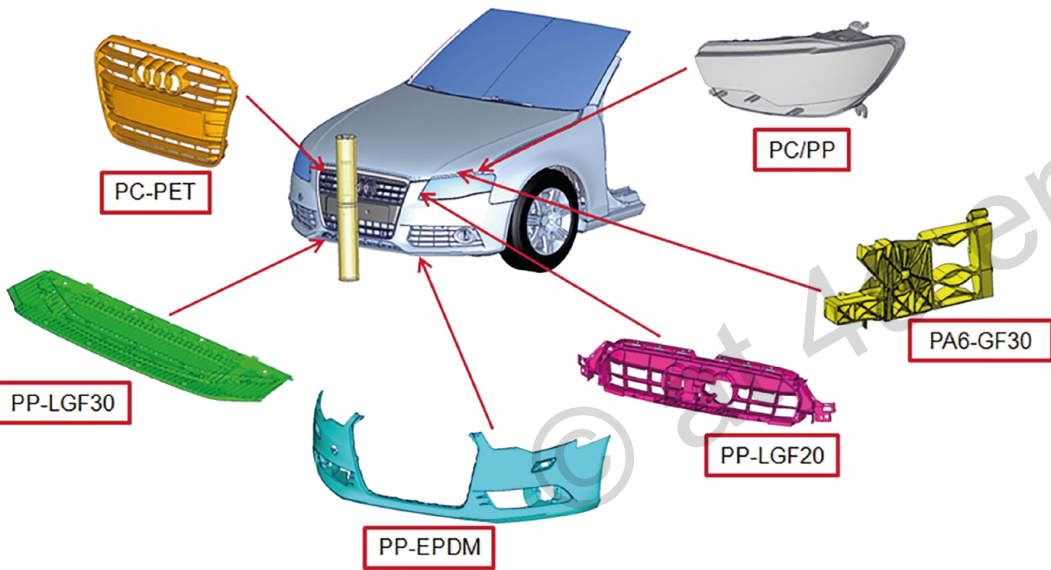
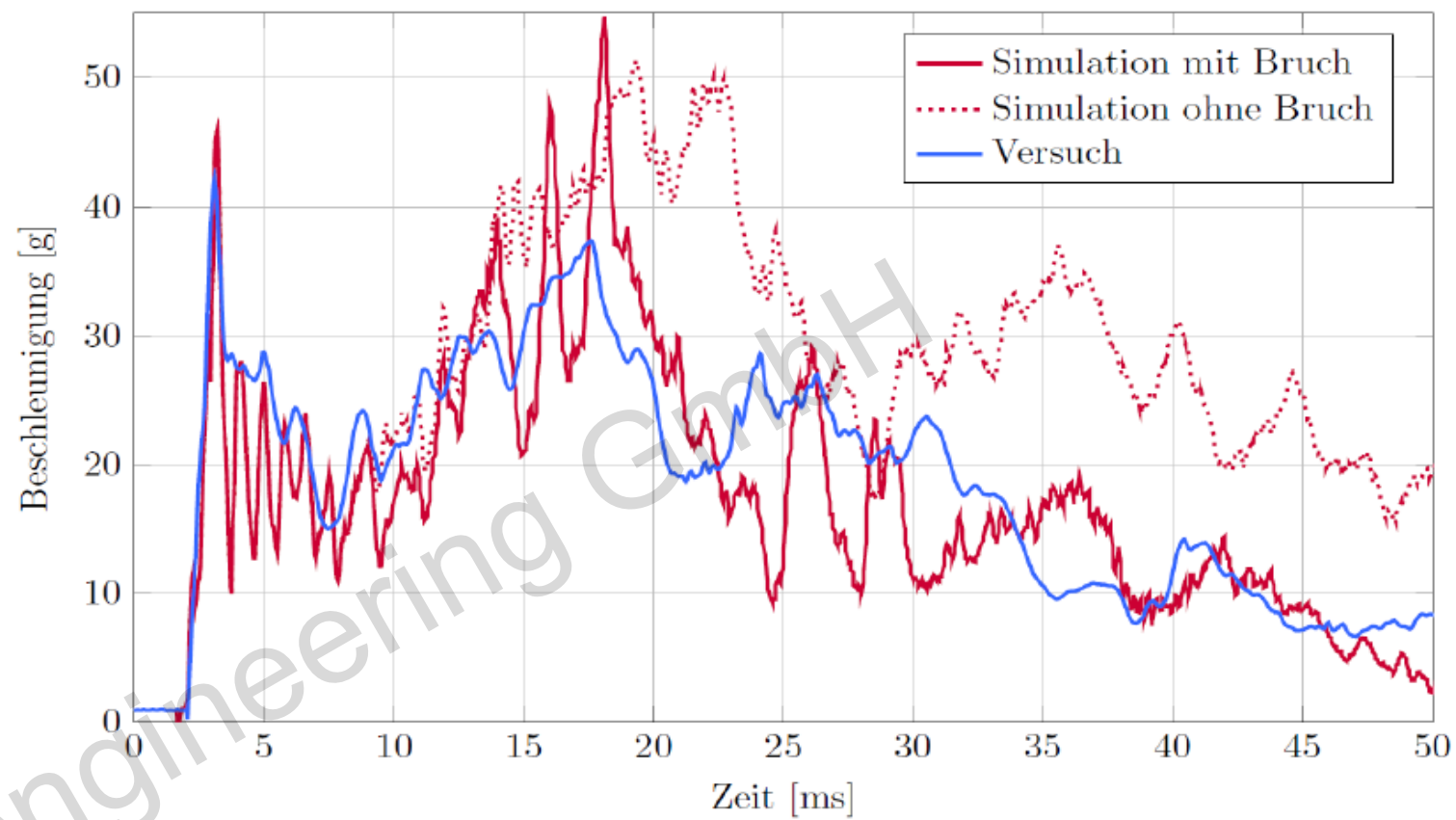
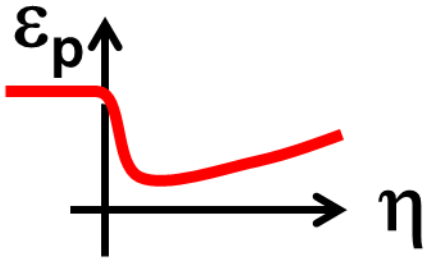
test simulation



Source: R. Luijckx - *Kunststoffmaterialien in der Interieur Funktionsauslegung bei Audi AG*, 4a Technologietag 2010

Motivation

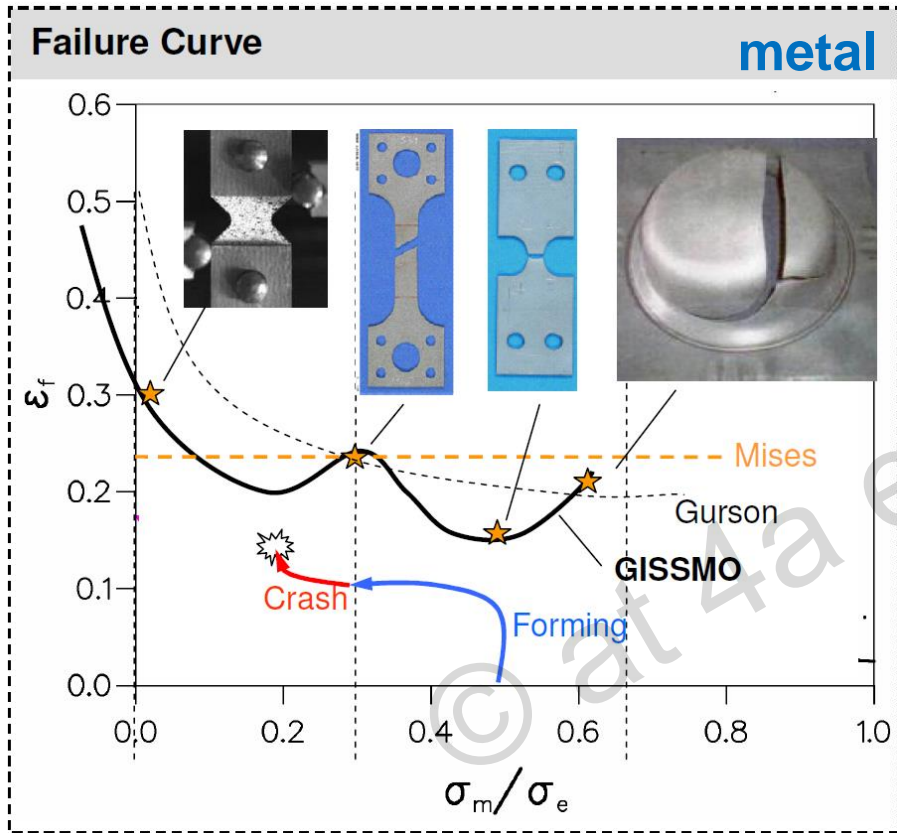
Damage/Failure



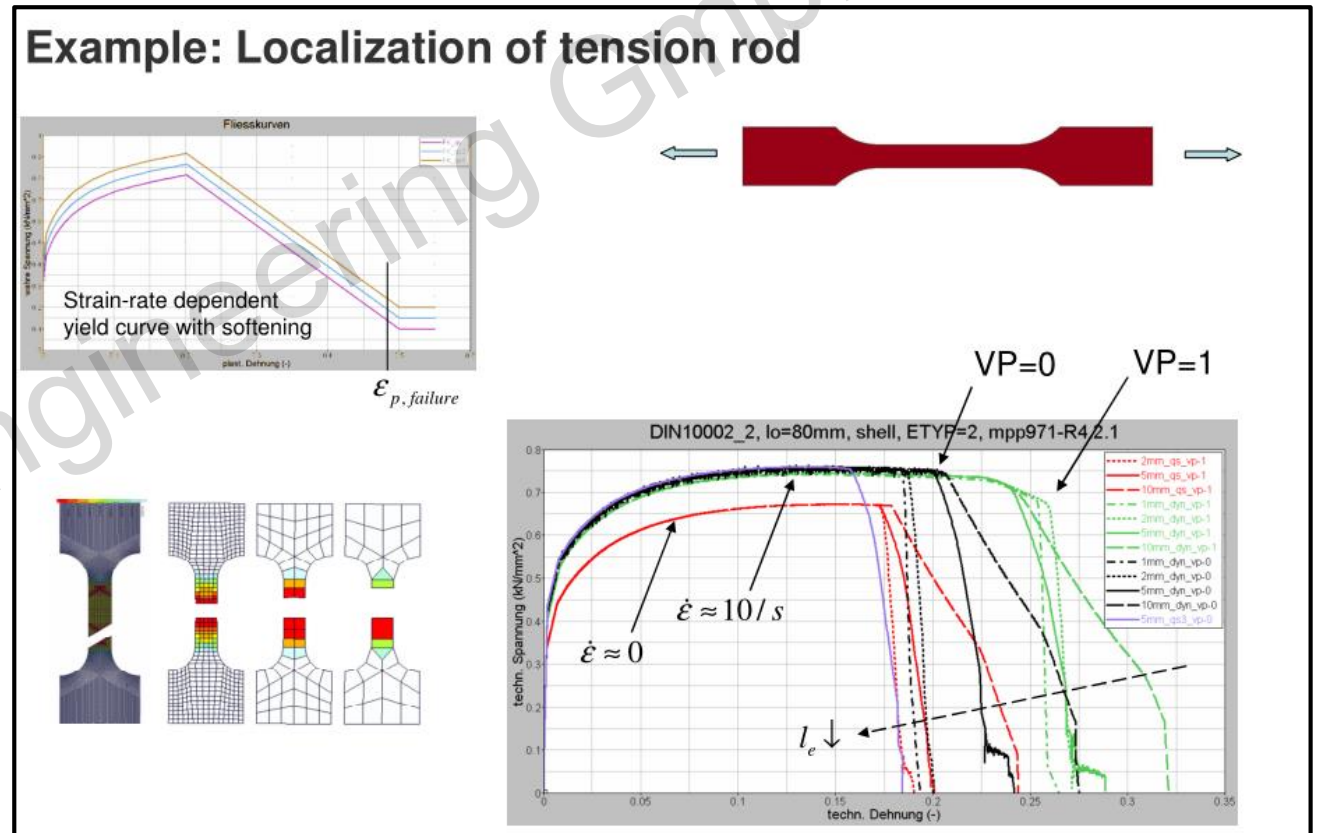
Source: H. Staack, Audi AG: Anforderungsgerechte Material- und Bruchmodellierung für die Fahrzeugsicherheit, TT16 Schladming

Motivation

- typical customers request for plastics
 - **GISSMO with *MAT_024** (***MAT_187** internal failure model)



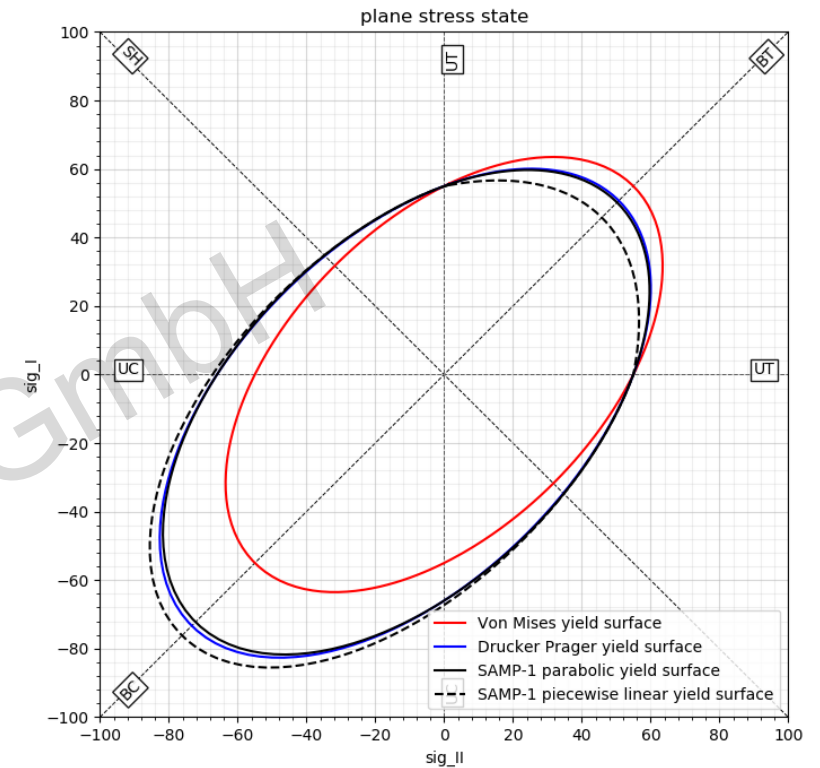
source: F. Neukamm – GISSMO – Material modeling with a sophisticated failure criteria, LS-Dyna Developer Forum 2011, Stuttgart



source: Damage and Failure Models in LS-DYNA; M. Feucht; A. Haufe ;(2009)

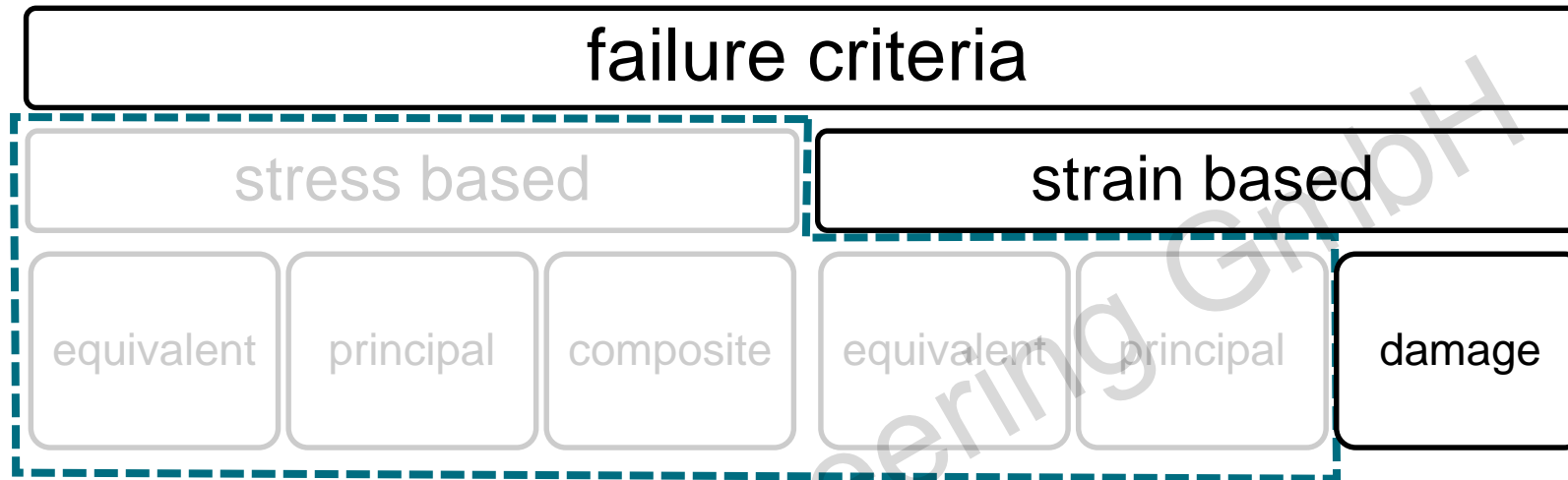
Commonly Used Material Models For Plastics

- ***MAT_024 - The workhorse**
(*MAT_081, *MAT_089, *MAT_123, ...)
- ***MAT_124 - The hidden**
- ***MAT_187 - The plastic expert**
- ***MAT_187L – efficient version (R11)**
- ***MAT_ADD_INELASTIC – promising (R11)**



Material model	yield surface	Visco-elasticity	Visco-plasticity	Comp./tension asymmetry	plastic Poisson's ratio
*MAT_024	von Mises	✗	✓	✗	0.5
*MAT_124	2x von Mises	✓ Pronyseries	✓	✓	0.5
*MAT_187L	linear	✗	✓	✓	✓
*MAT_187	general	✓ Table	✓	✓	✓

Available failure models in LS-DYNA®



additional failure models

***MAT_ADD_EROSION**

strain damage based

- *before R11 optional DIEM / GISSMO*
- *since R11 *MAT_ADD_DAMAGE_DIEM*
- *since R11 *MAT_ADD_DAMAGE_GISSMO*

included damage model in

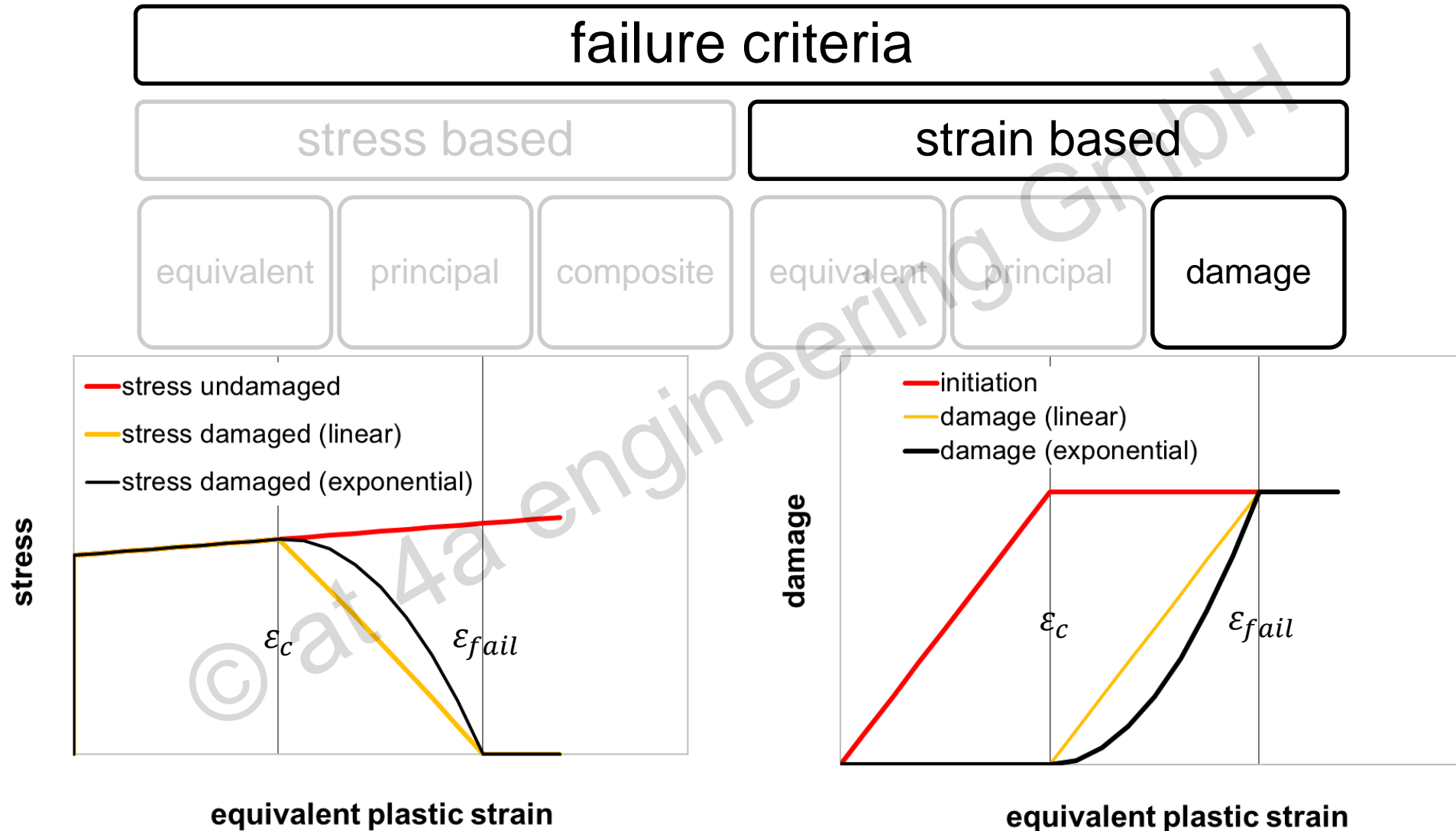
***MAT_SAMP-1**

GISSMO like

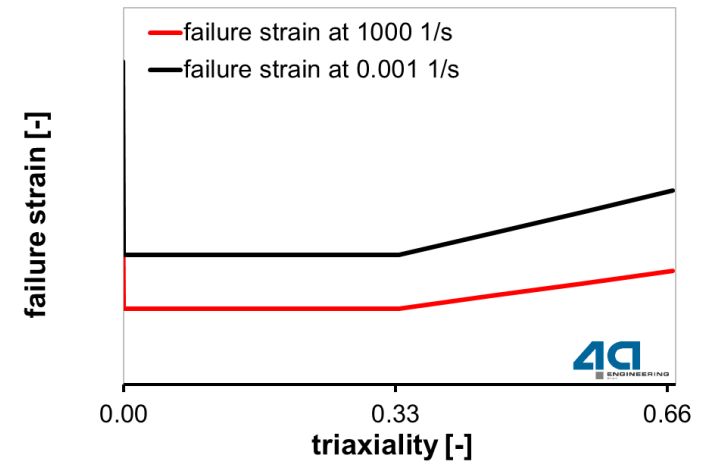
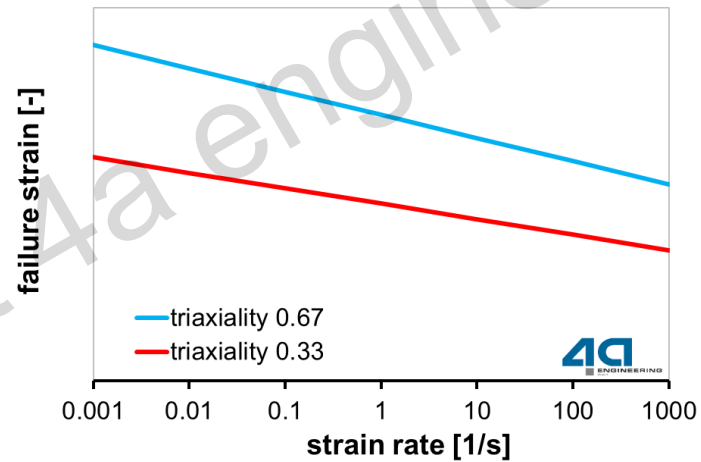
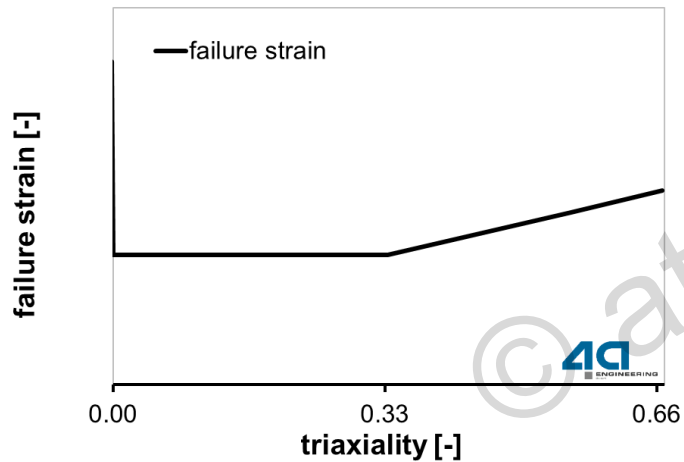
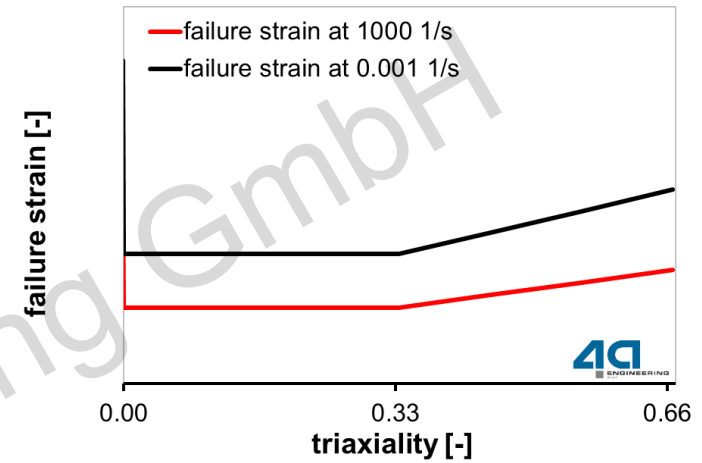
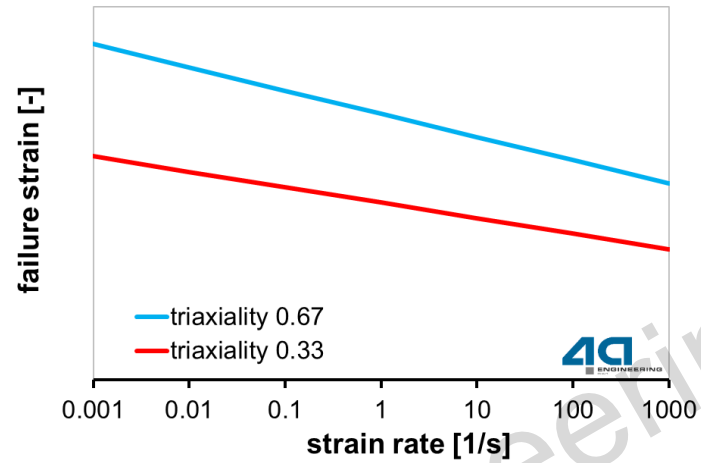
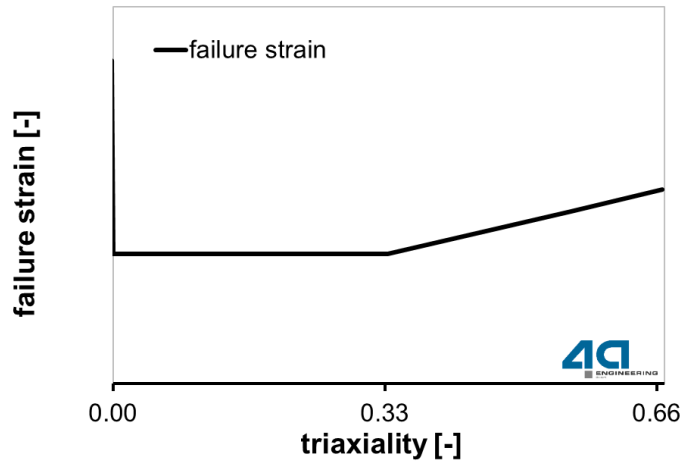
***MAT_4A_MICROMECH**

DIEM for matrix failure

Available failure models – incremental damage formulation



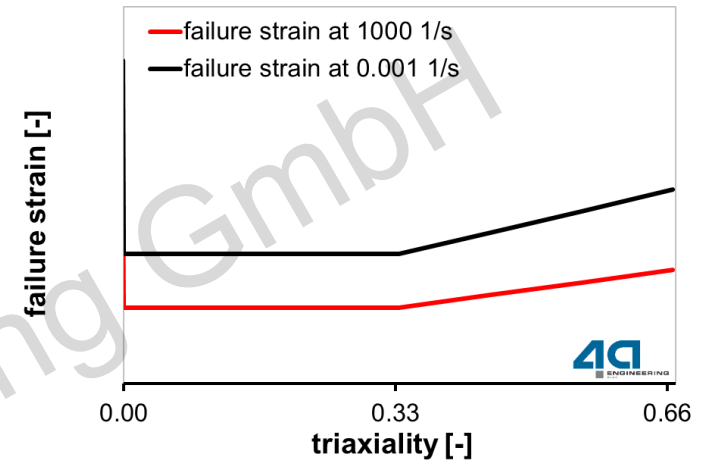
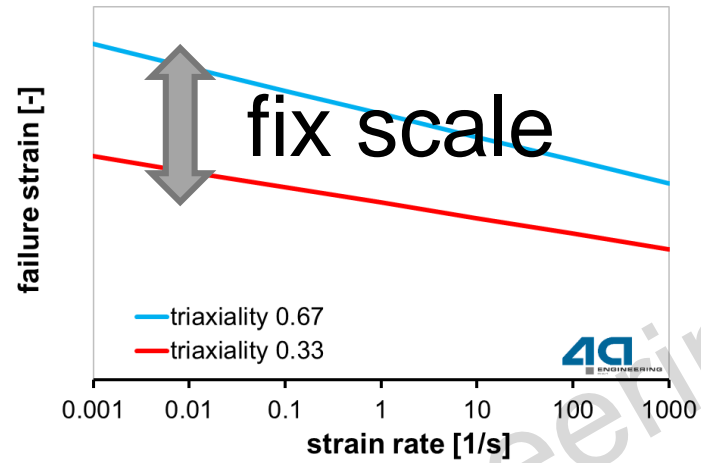
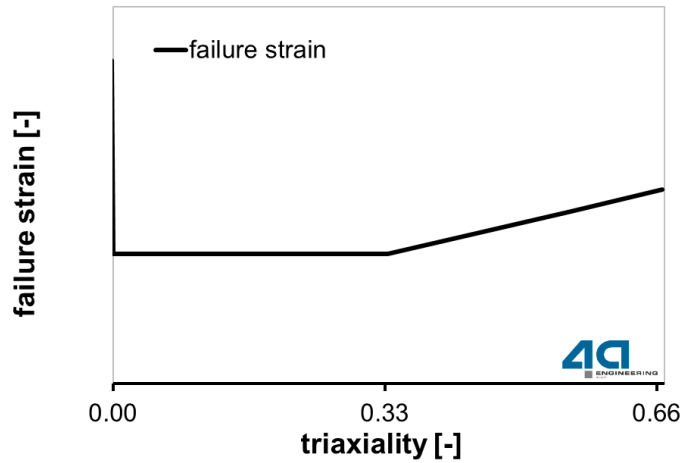
Comparison DIEM-GISSMO visualized



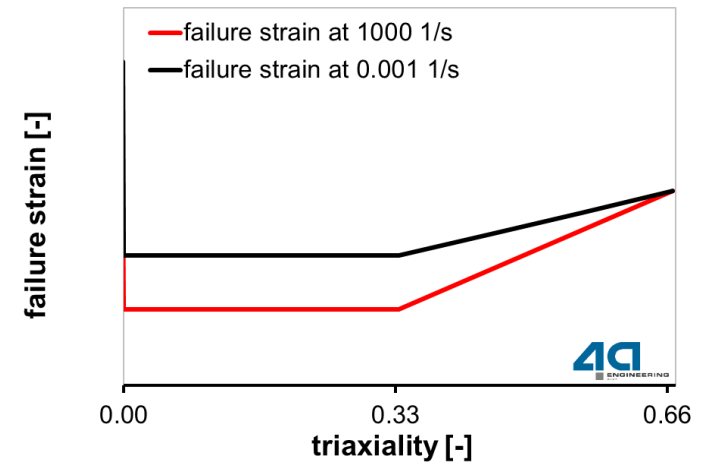
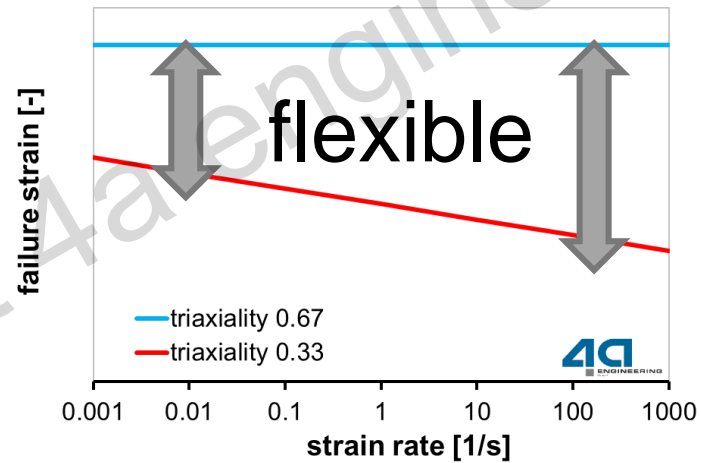
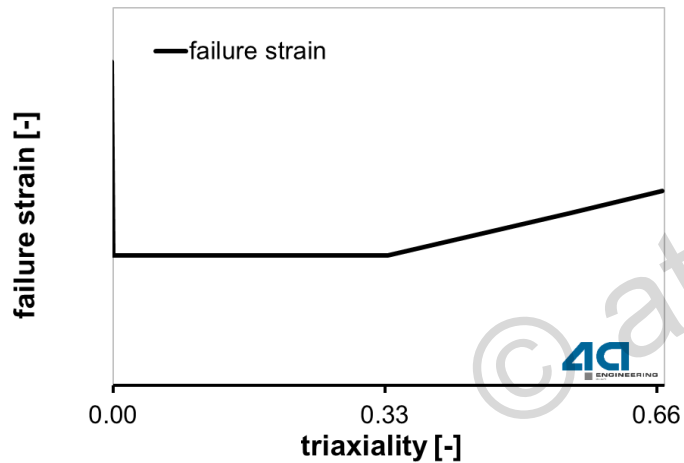
GISSMO

DIEM

Comparison DIEM-GISSMO visualized



GISSMO



DIEM

Fracture models → *MAT_ADD_EROSION



Parameter model* Model database

170503_024 Material Designvariables Layers

Materialcard MMEC
Image Comment

- Material behaviour
 - Material source
 - Elasticity
 - Plasticity
 - Failure/Damage
 - Material card
 - Materialcardcase
 - Damage/Failurecase
 - Materialcard id
 - Density
 - Plasticity
 - Function (Hardening, Elastic curve form)
 - Curve 1
 - Curve 2
 - Strain range upto
 - Sampling points
 - Bias factor
 - Strain rate dependency
 - Strain rate dependency
 - Fracture
 - Ductile Damage Settings
 - lower triax value
 - upper triax value
 - step size triax
 - Shear Damage Settings
 - FLC Damage Settings
 - Strainrate Settings
 - Postfracture
 - Loadcases
 - Results

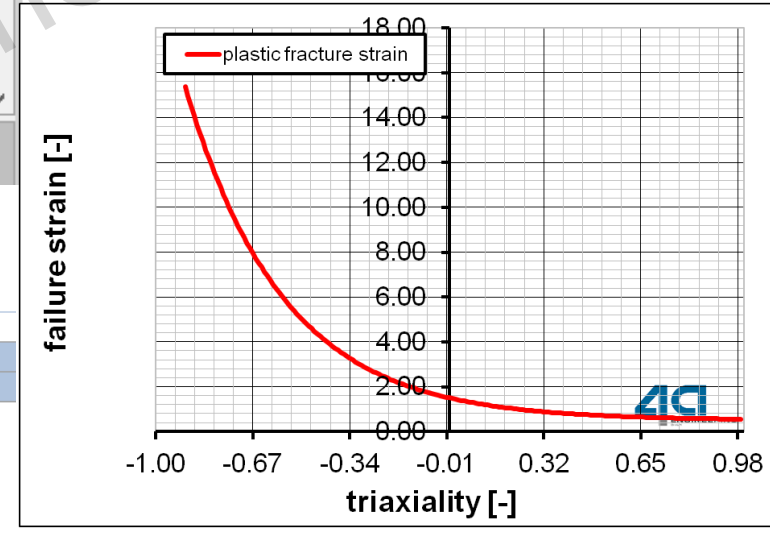
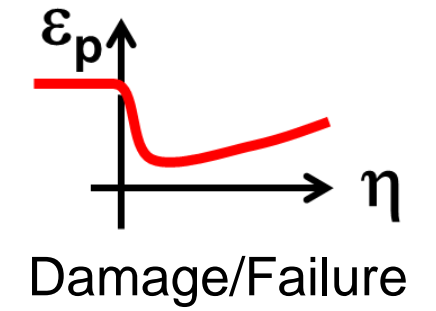
Density	-1
Plasticity	vonMISES
Function (Hardening, Elastic cur	
Strain rate dependency	Table
Fracture	Damage
Ductile Damage Settings	Johnson Cook
Shear Damage Settings	None
FLC Damage Settings	plastic equivalent strain
Strainrate Settings	simple criteria
Postfracture	4a picewise linear
Loadcases	Johnson Cook
Casename	mod Xue-Wierzbicki
Tests	Xue-Wierzbicki
Settings optimization	Mohr-Coulomb
Weighting case	1

Ductile Damage Settings

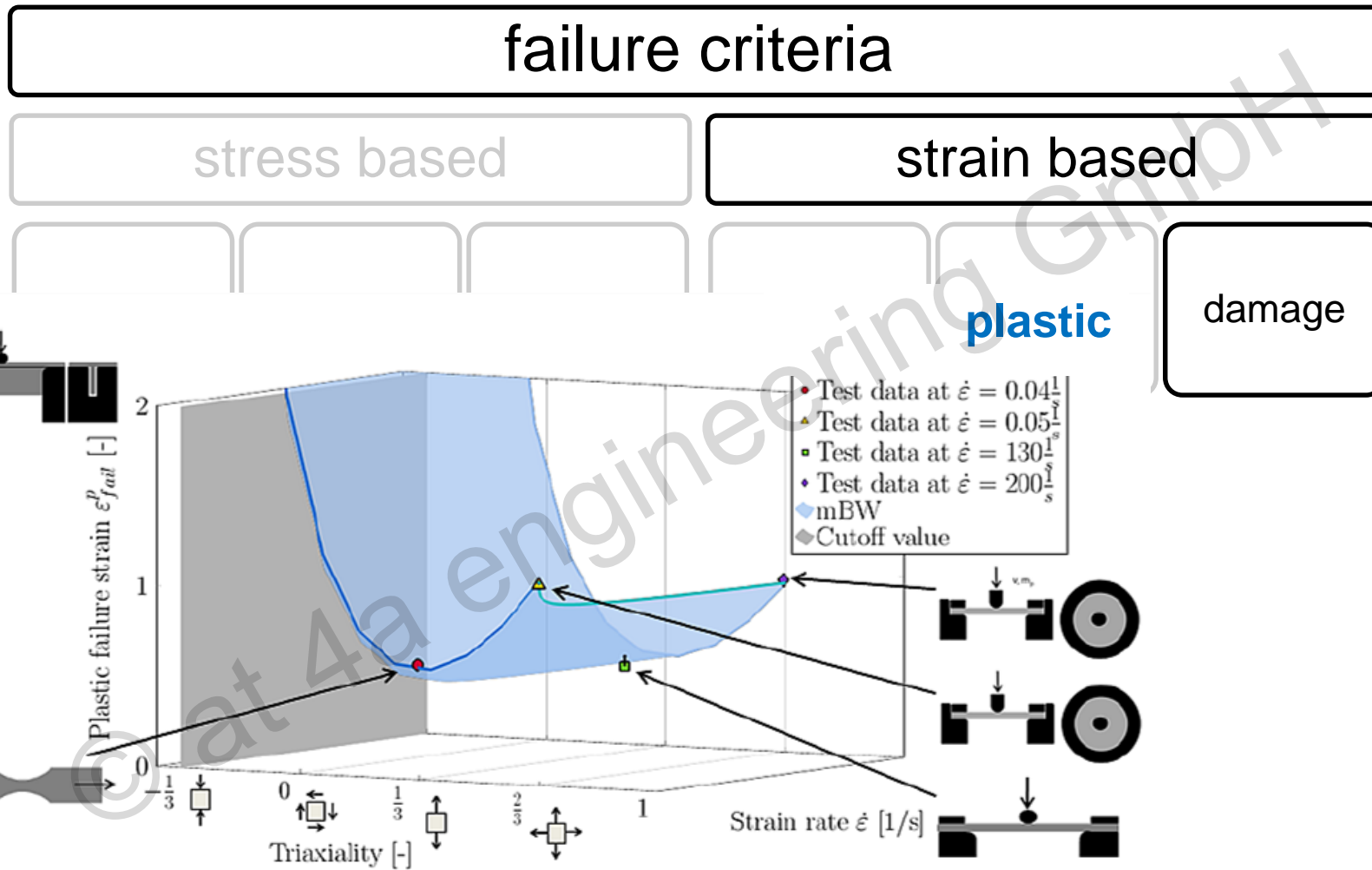
	0.33	Johnson Cook
	None	mod Xue-Wierzbicki
	None	Xue-Wierzbicki
	Johnson Cook	Mohr-Coulomb
	Fracture Energy (TRIAX)	

Materialcard MMEC
Image Comment

fd_{JCD1} + fd_{JCD2} · e^{-fd_{JCD3} · η}

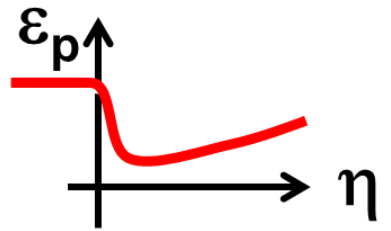
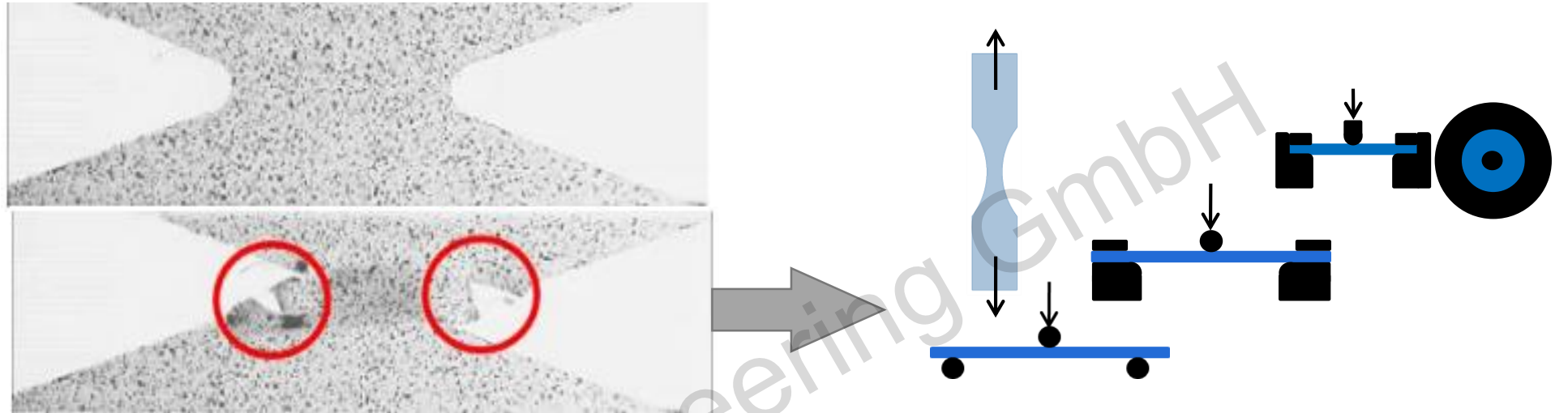


Available failure models – typical curves

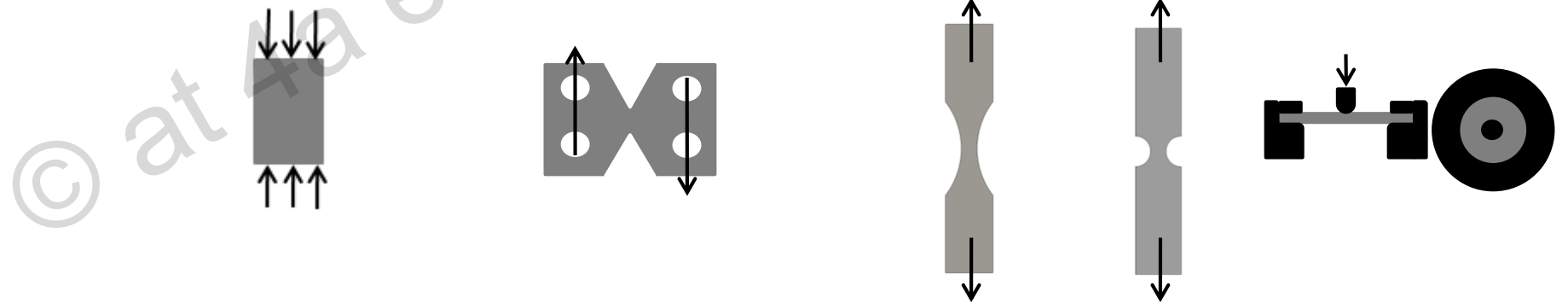


source: H. Staack, - Application oriented failure modeling and characterization for polymers in automotive pedestrian protection, COMPLAS 2015, Barcelona

From test to material card

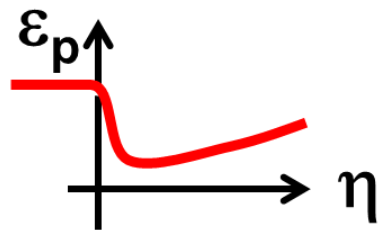


Damage/Failure

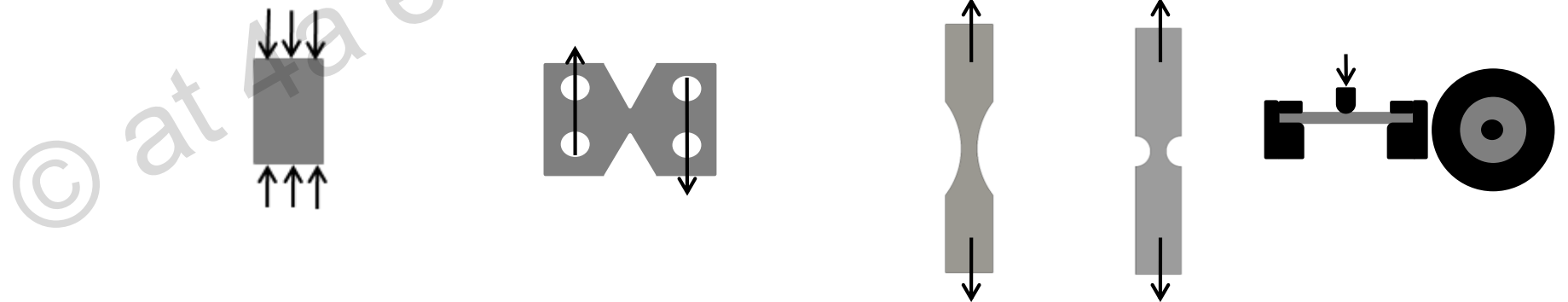


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From test to material card



Damage/Failure

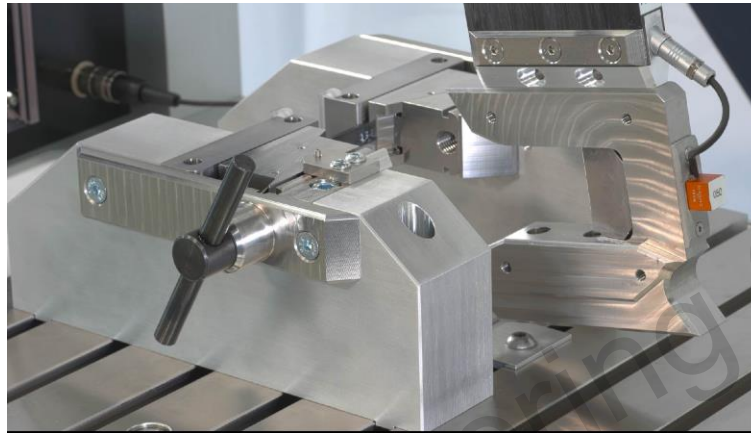


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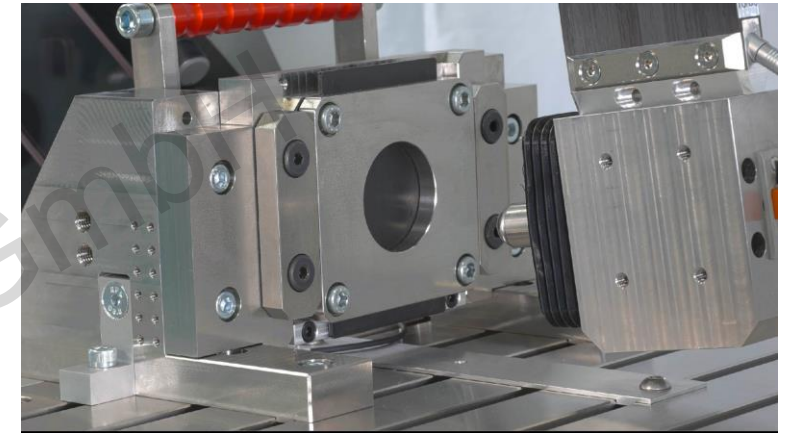
IMPETUS™ - efficient dynamic testing



3 POINT BENDING

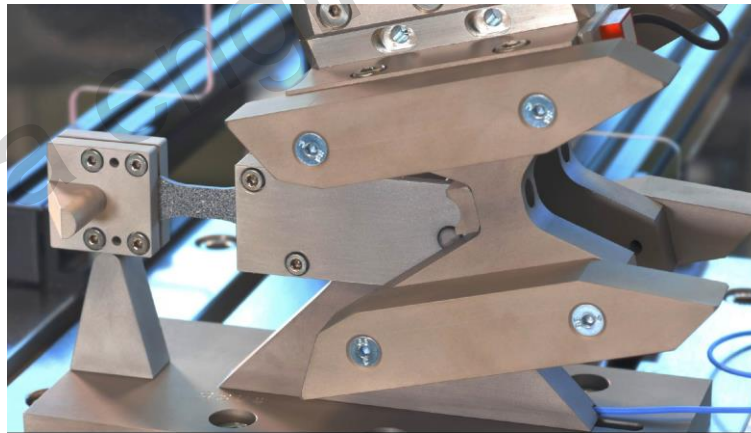


TENSION BENDING

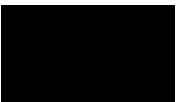
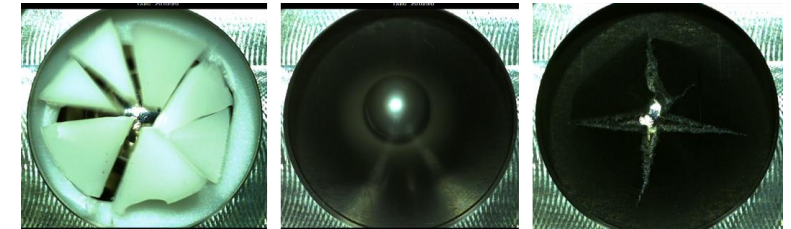


PUNCTURE TEST

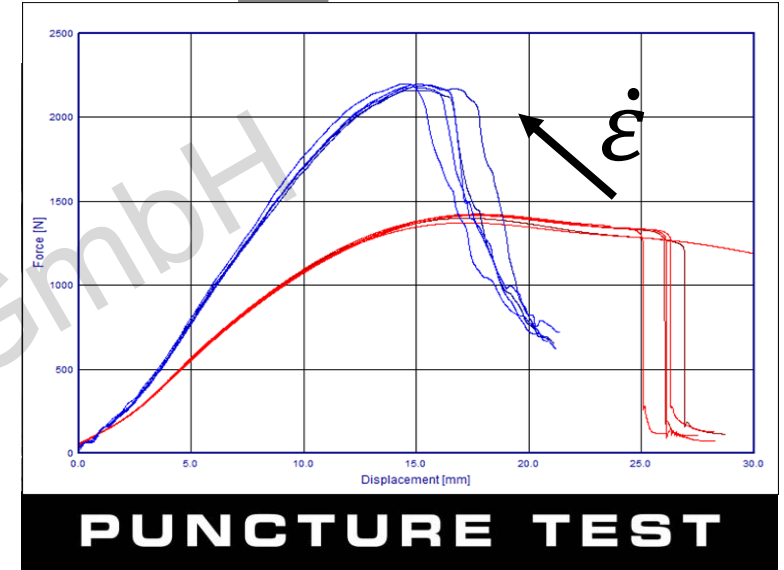
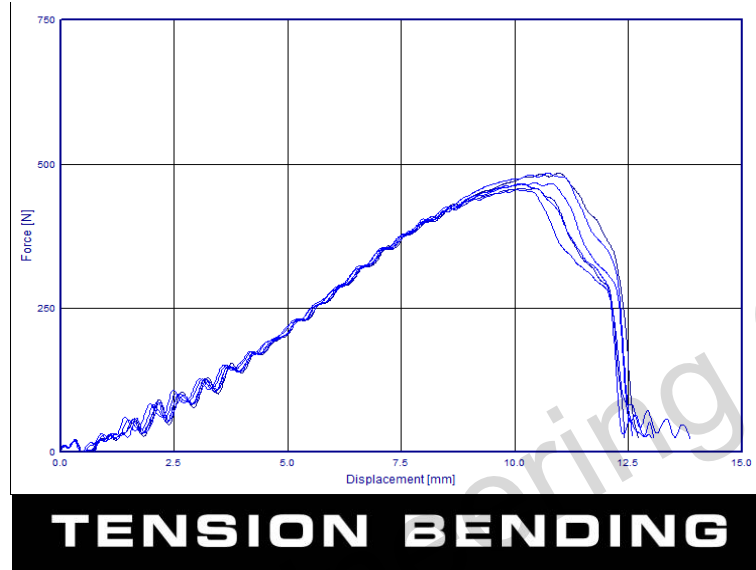
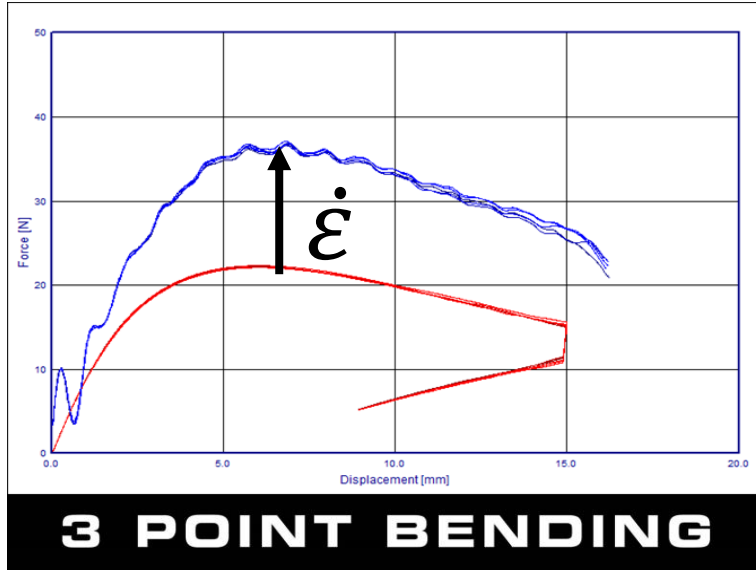
IMPETUS™ ~ 3 m/s
static ~ 1mm/s



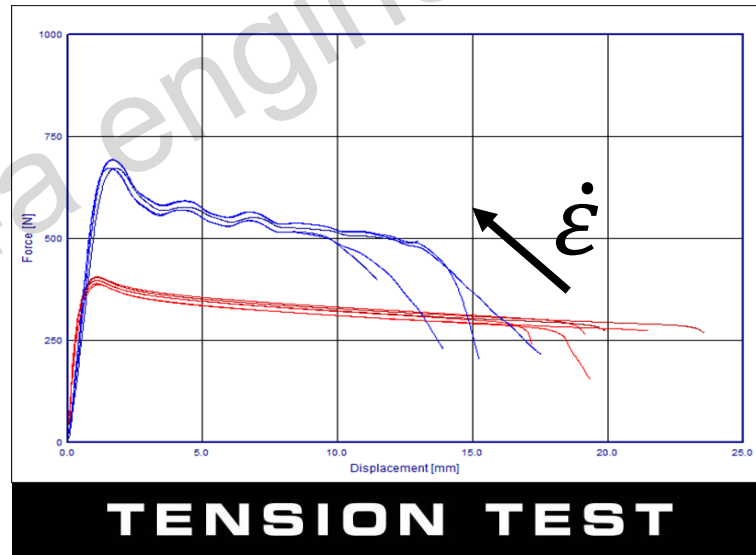
TENSION TEST



IMPETUS™ - efficient dynamic testing



IMPETUS™ ~ 3 m/s
static ~ 1 mm/s

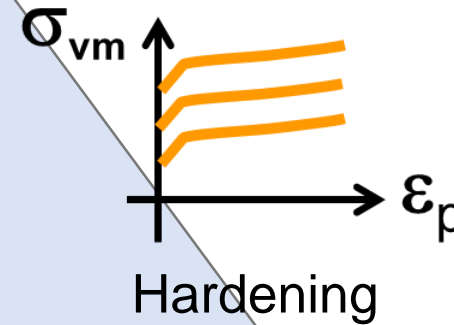
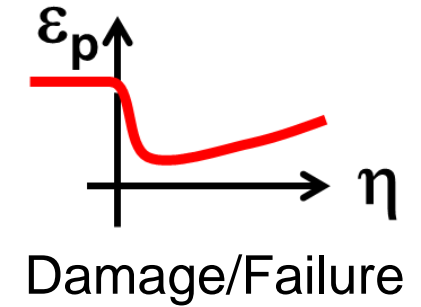
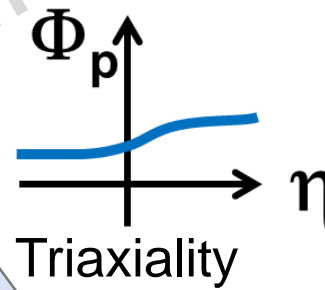
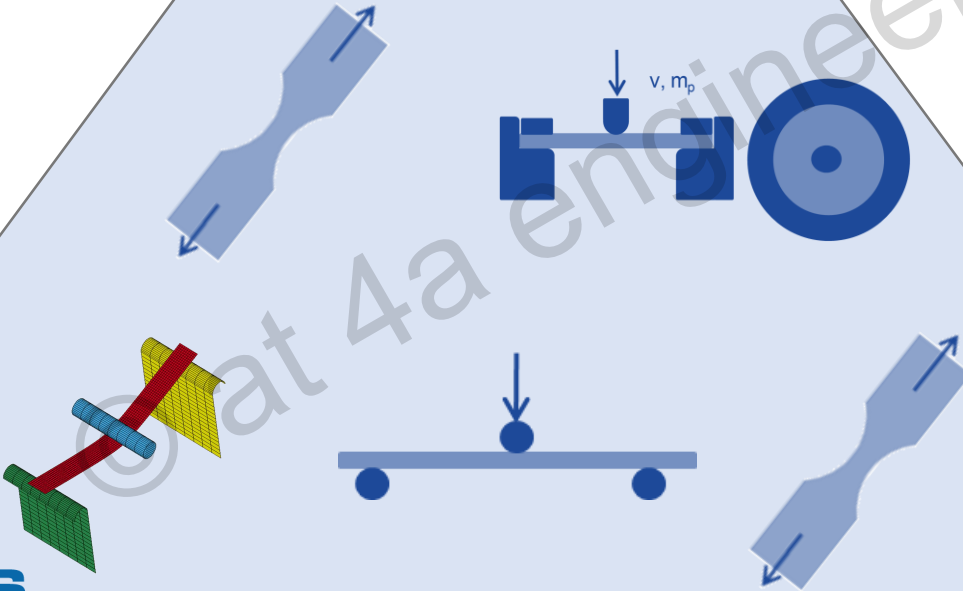
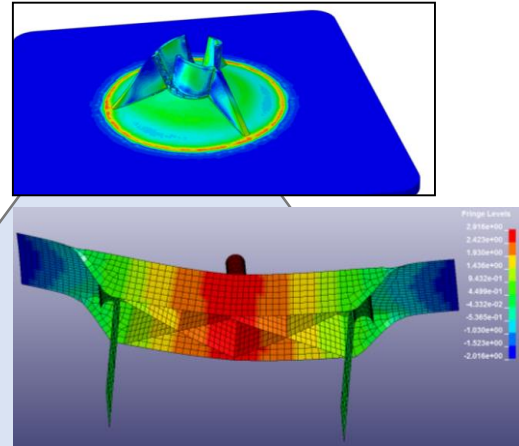


From test to material card



VALIMAT

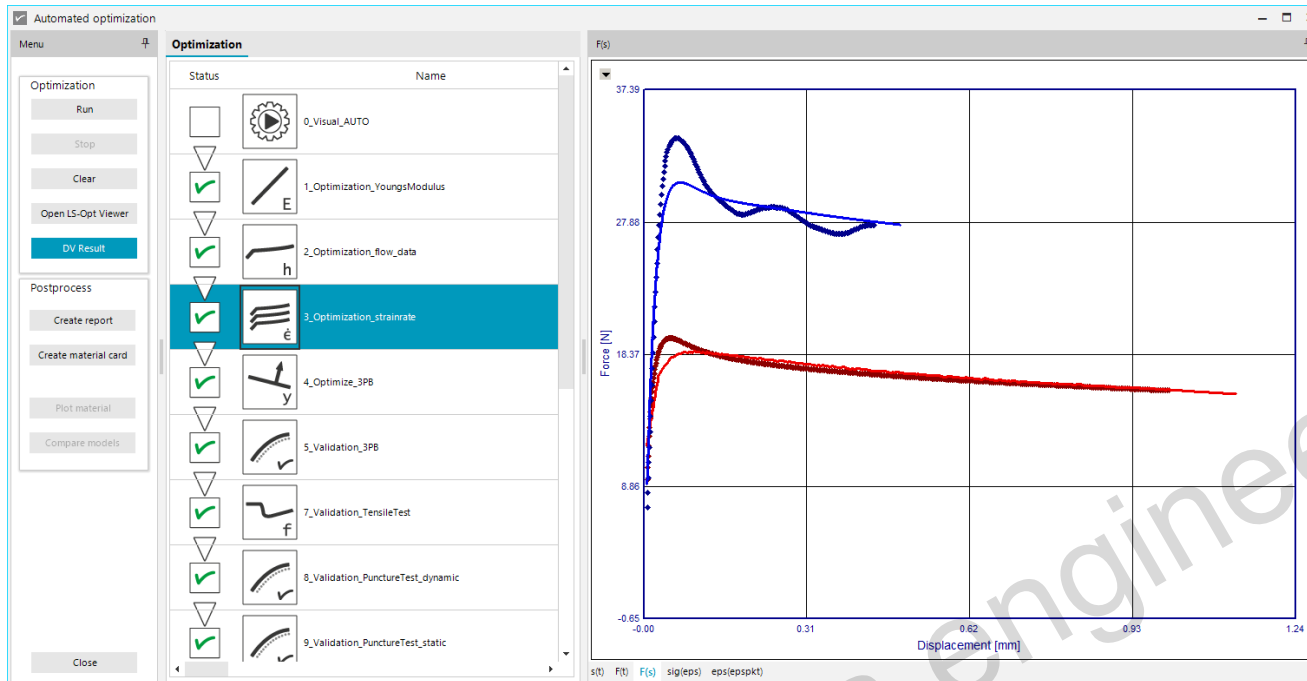
Deformation → Failure
 Creep → Static → Crash
 ISOTROPIC → ANISOTROPIC



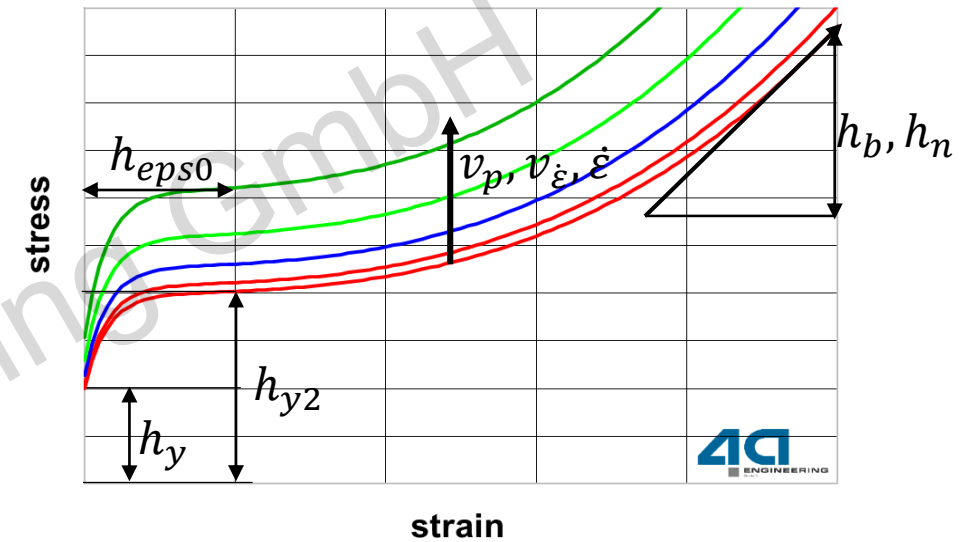
IMPETUS



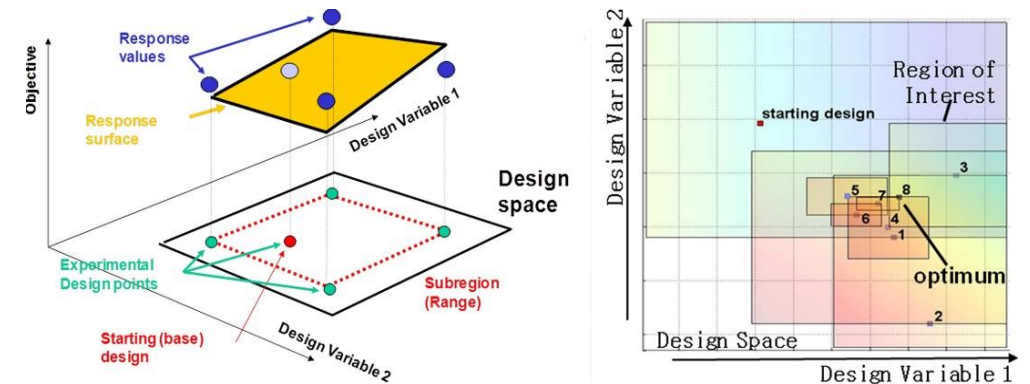
Workflow for material card generation - AUTOFIT



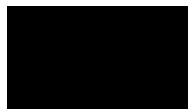
parametrized material card



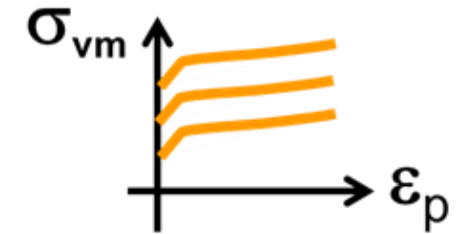
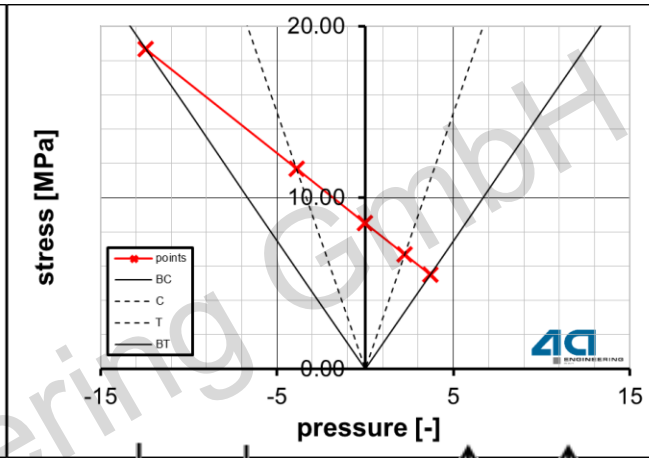
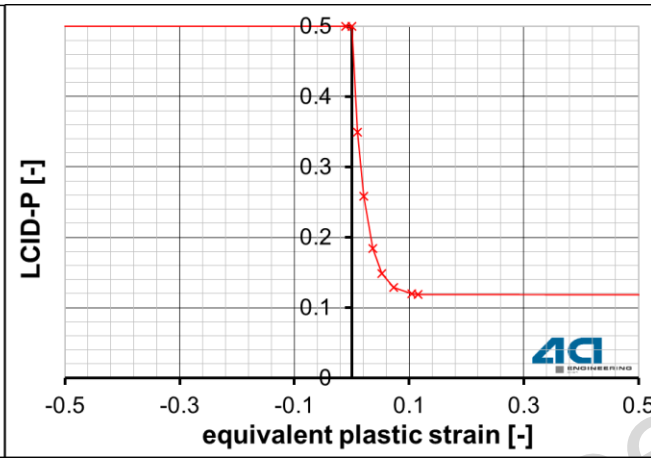
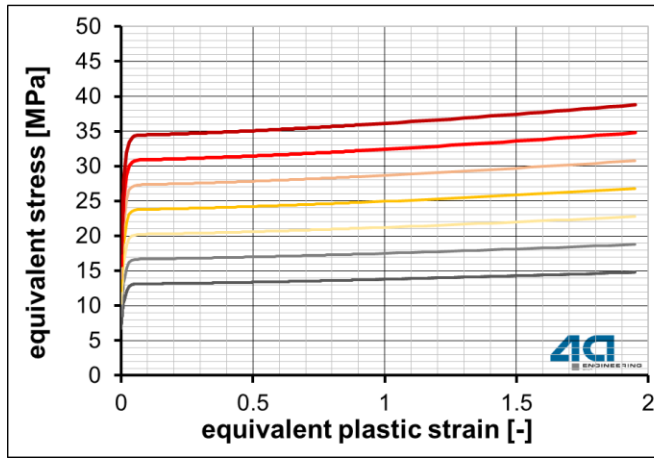
optimization – successive response surface method



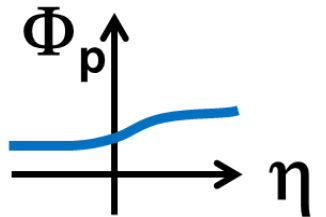
© at 4a engineering GmbH



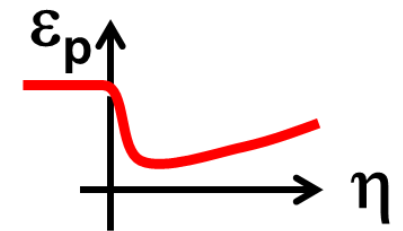
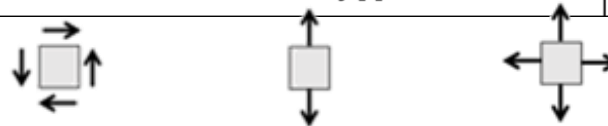
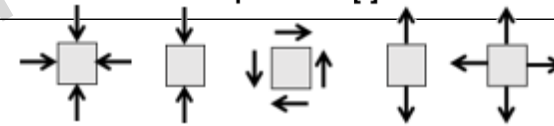
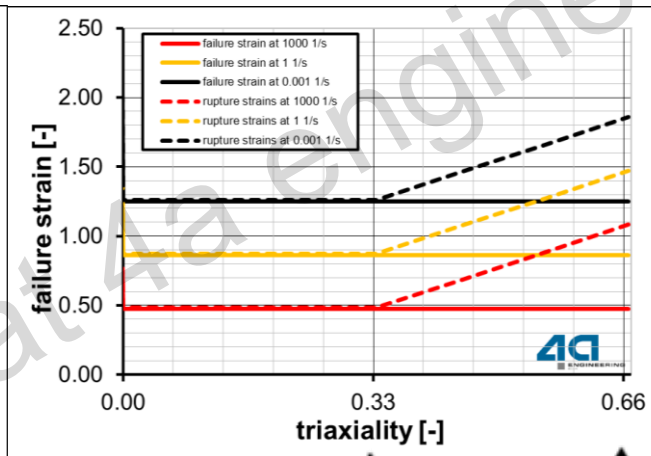
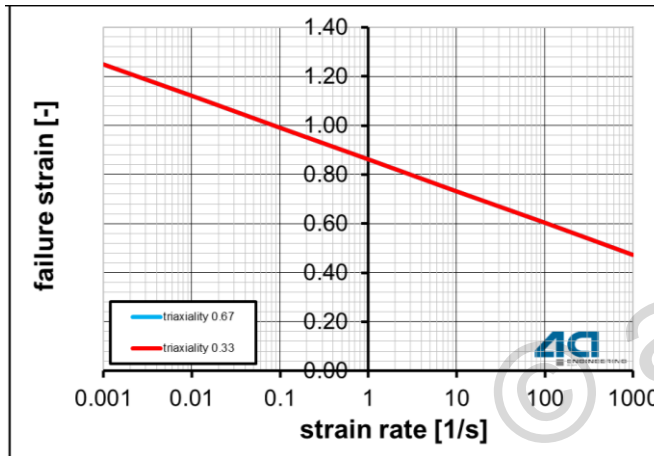
*MAT-SAMP 1 with internal FM – result AUTOFIT



Hardening



Triaxiality

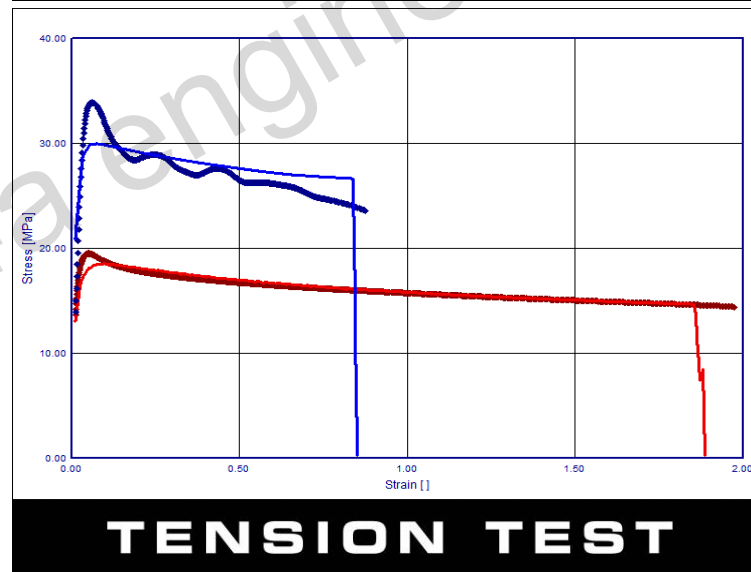
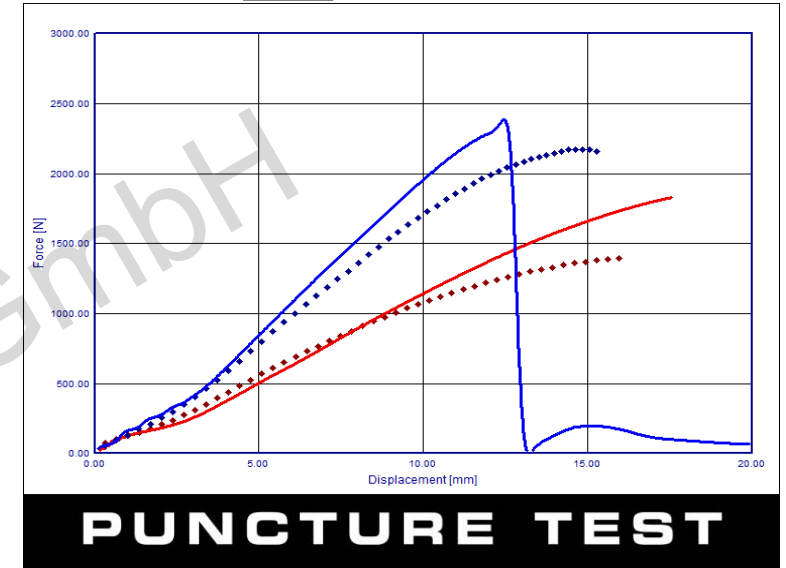
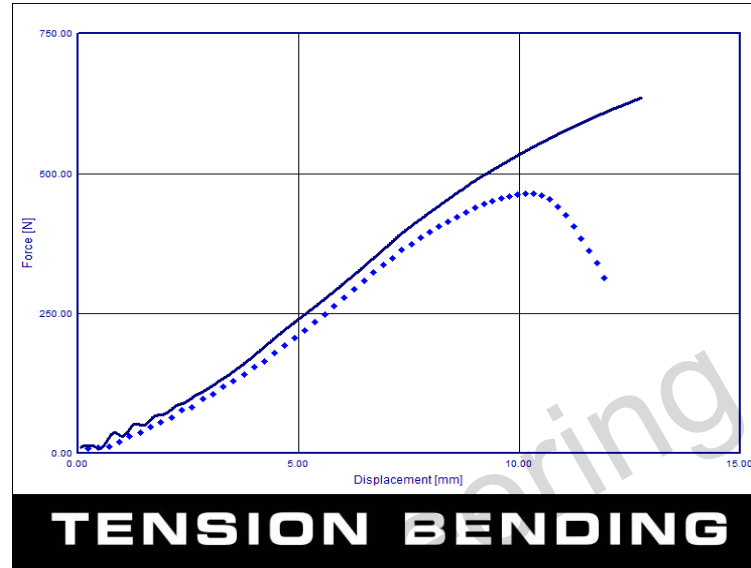
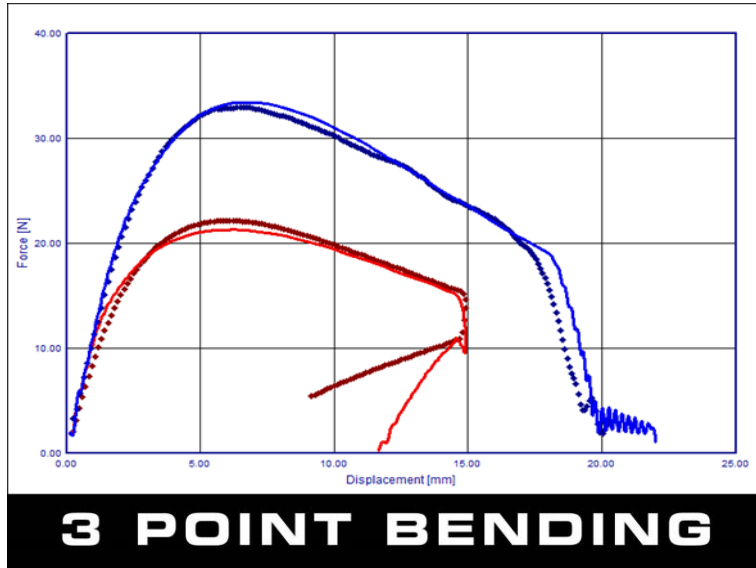


Damage/Failure

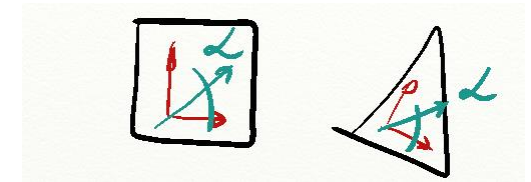
source: Benjamin Hirschmann, master thesis



*MAT-SAMP 1 with internal failure model - validation



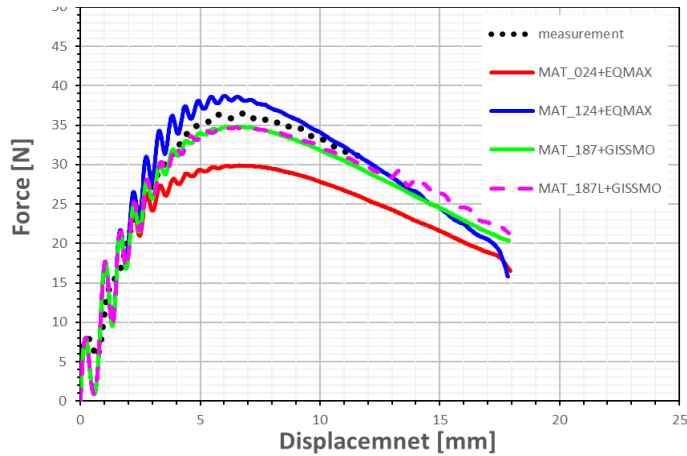
IMPETUS™ ~ 3 m/s
static ~ 1 mm/s



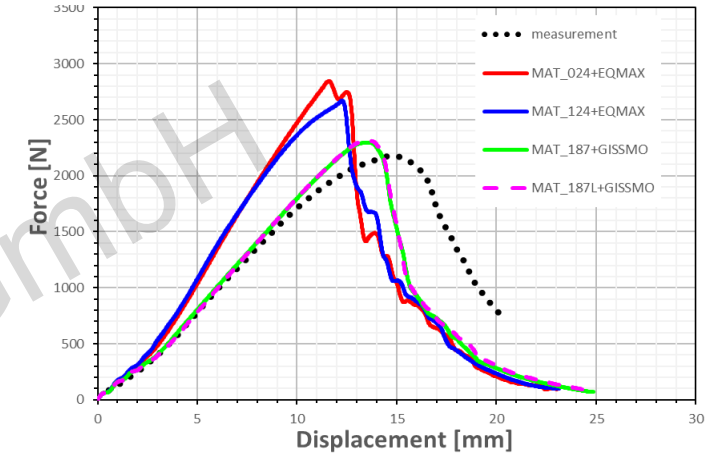
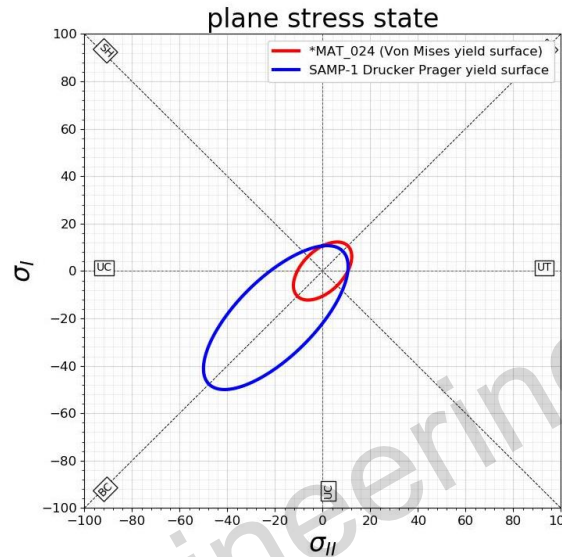
..... averaged test curves
— result of simulation

source: Benjamin Hirschmann, master thesis

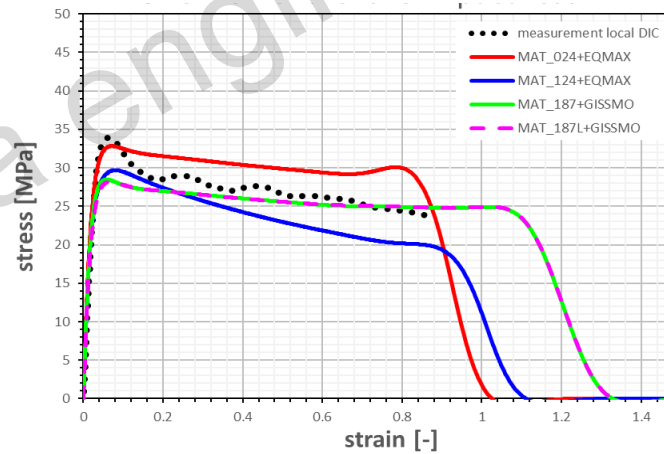
Comparison of different material models



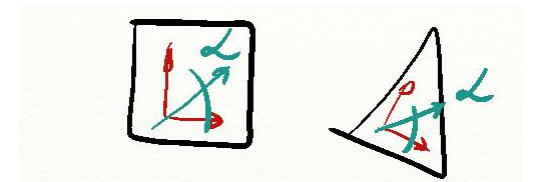
3 POINT BENDING



PUNCTURE TEST



TENSION TEST

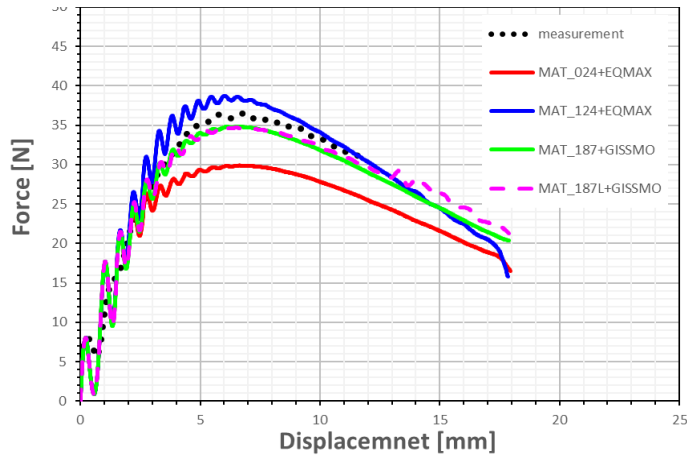


..... averaged test curves
 — result of simulation

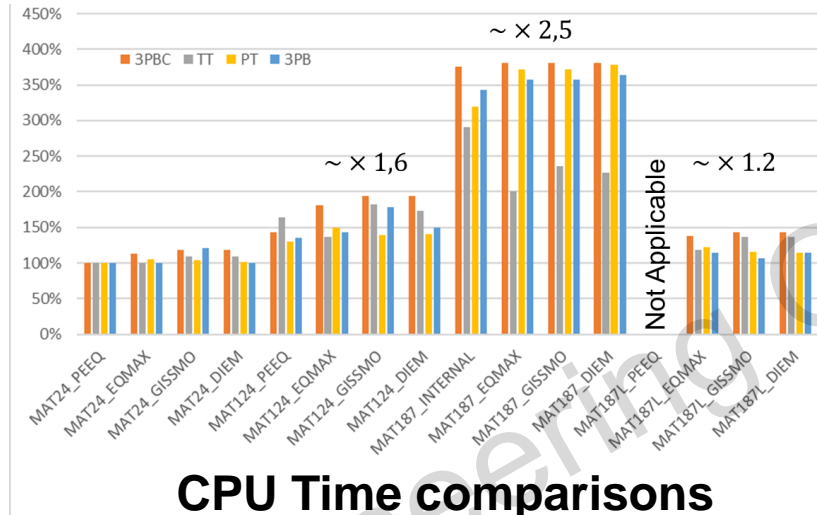
IMPETUS™ ~ 3 m/s

source: Benjamin Hirschmann, master thesis

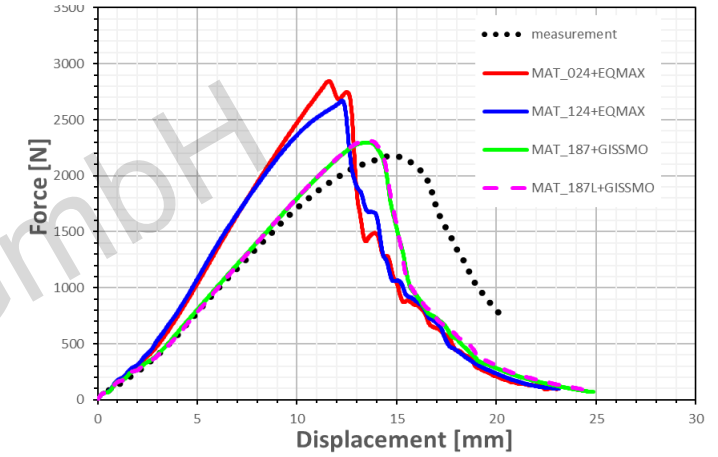
Comparison of different material models



3 POINT BENDING

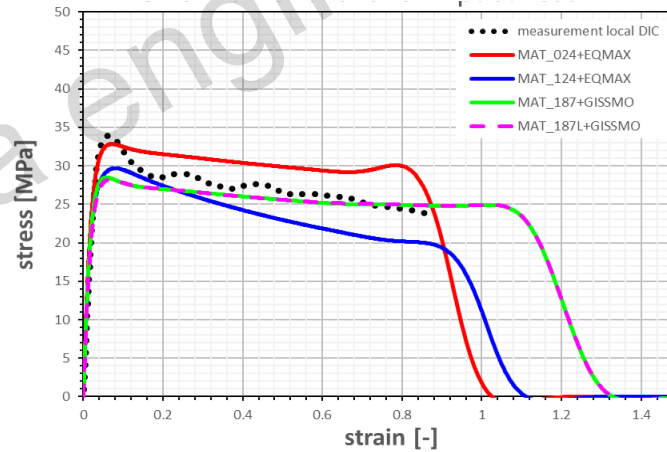


CPU Time comparisons

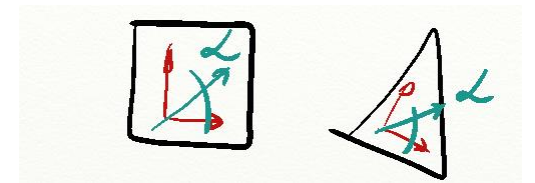


PUNCTURE TEST

IMPETUS™ ~ 3 m/s

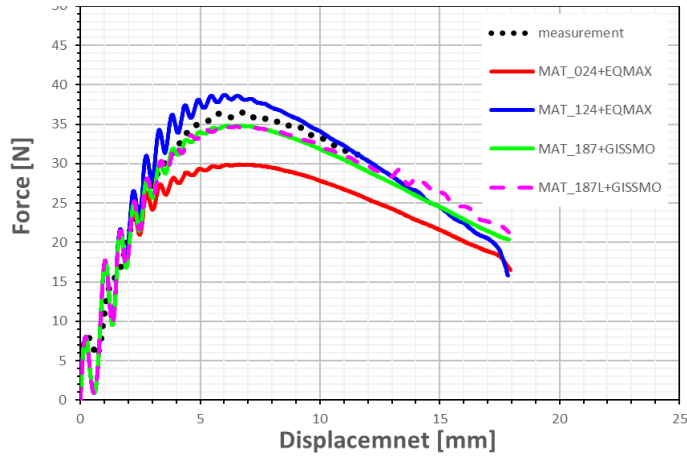


TENSION TEST



source: Benjamin Hirschmann, master thesis

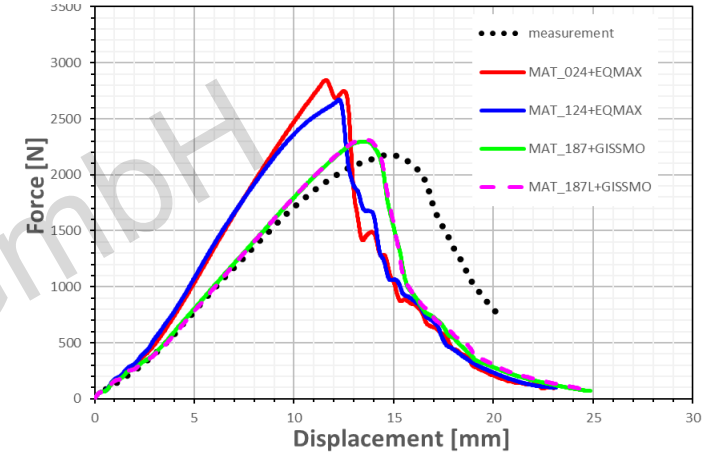
Comparison of different material models



3 POINT BENDING

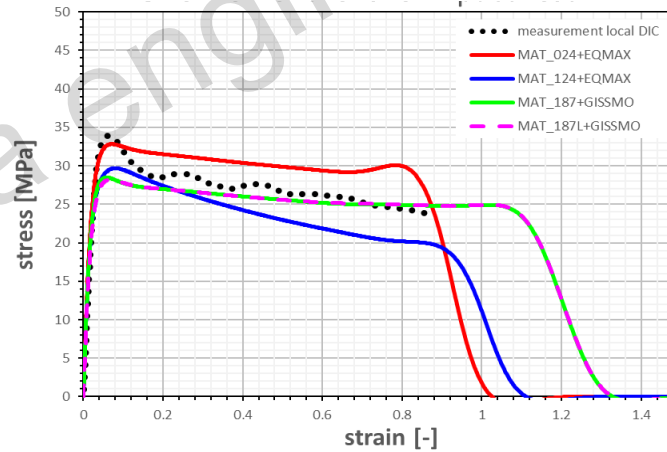
Material model	CPU Time
<i>*MAT_024</i>	1
<i>*MAT_124</i>	1.6
<i>*MAT_187</i>	2.5
<i>*MAT_187L</i>	1.2

CPU Time comparisons

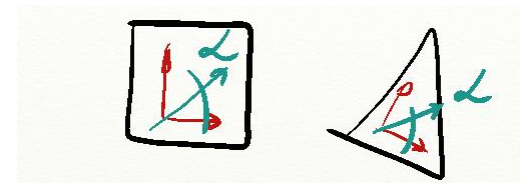


PUNCTURE TEST

IMPETUS™ ~ 3 m/s

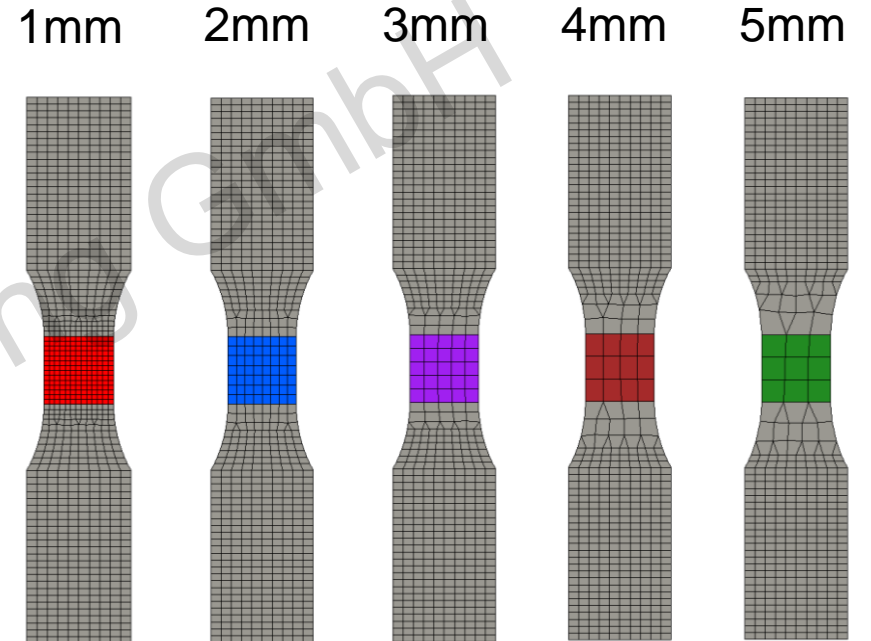
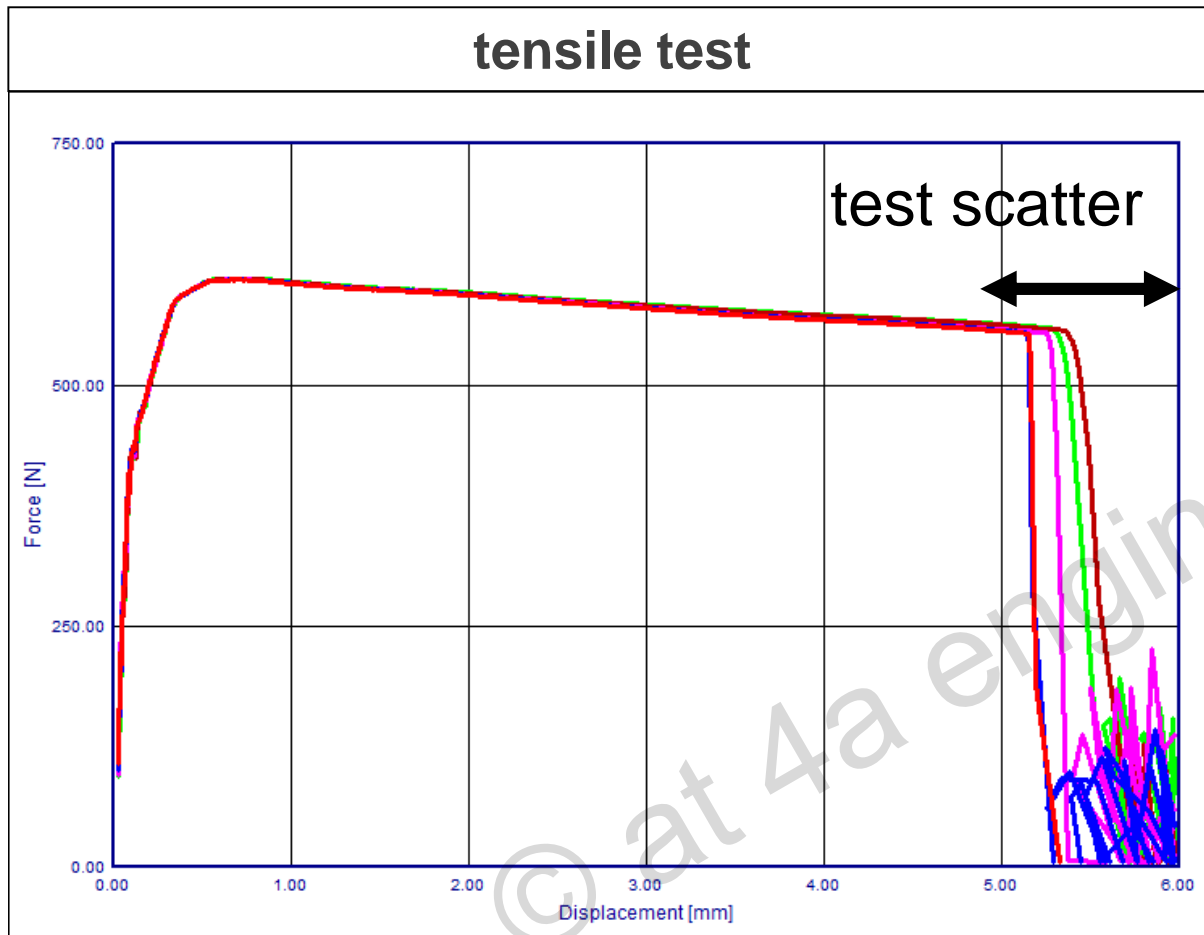


TENSION TEST



source: Benjamin Hirschmann, master thesis

*MAT-SAMP 1 with internal failure model – influence element size



source: Benjamin Hirschmann, master thesis

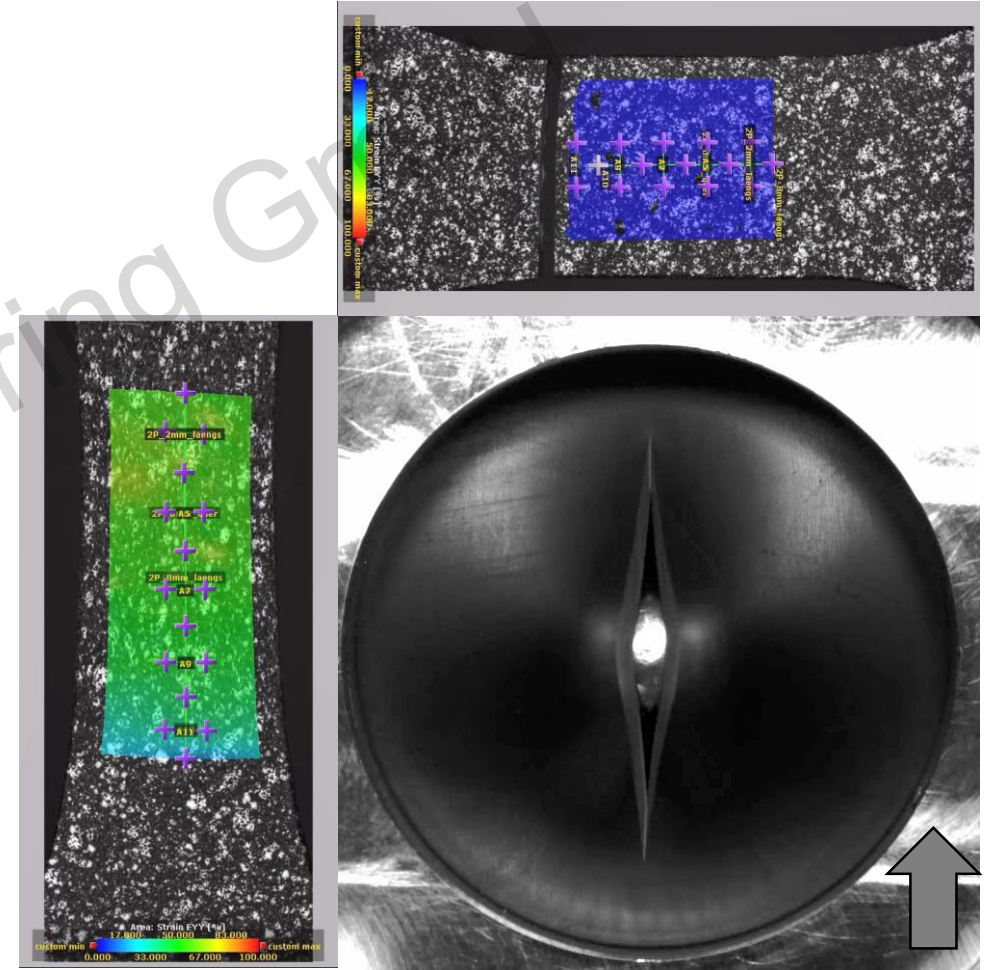
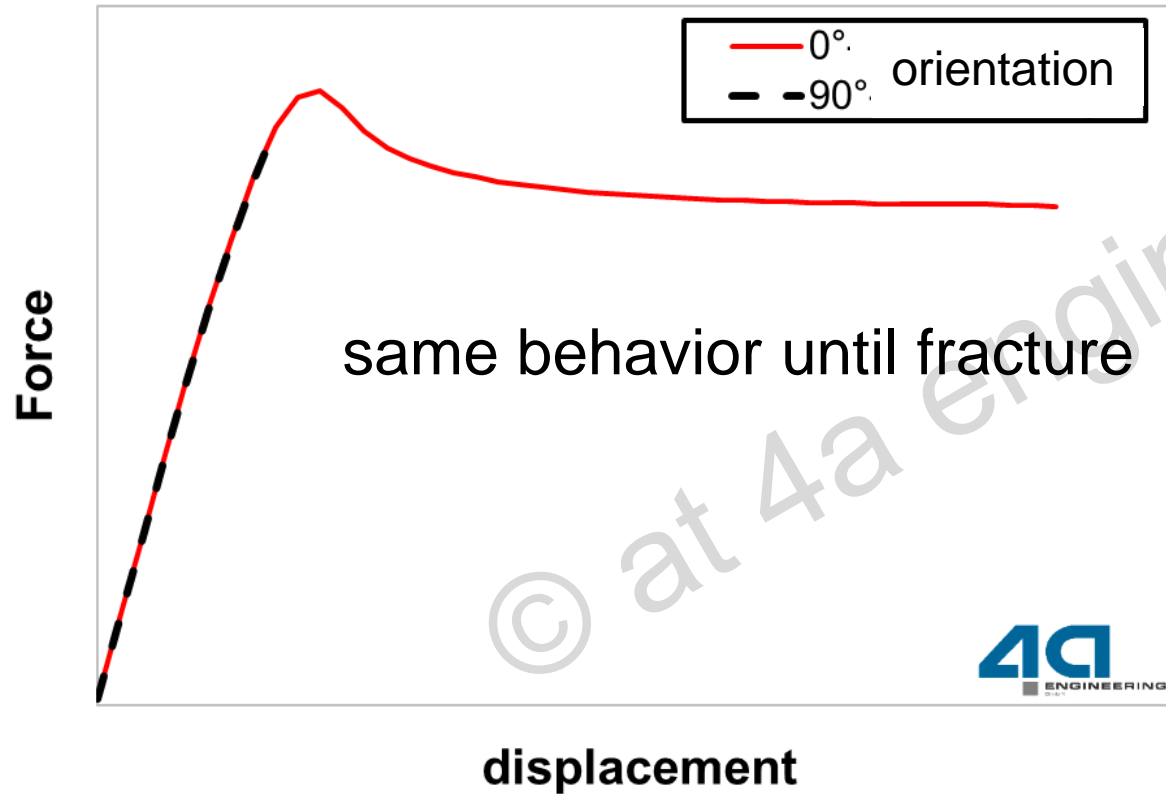
Anisotropic Failure **(**MAT_ADD_GENERALIZED_DAMAGE*)**

Plastics ?

© at 4a engineering GmbH

Influence of manufacturing process on failure

- example: ABS
 - The induced orientation by the injection molding process leads to an anisotropic failure behavior.



Intelligent reliable solutions for plastics, composites, metals, foams, ...

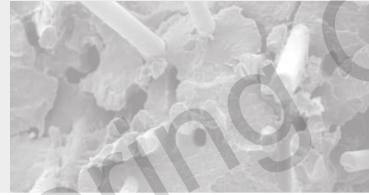
 **IMPETUS**



 **VALIMAT**



 **MICROMECH**



 **FIBERMAP**



Fiber reinforced Plastics (SFRT & LFRT)



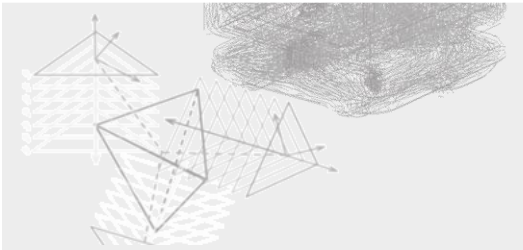
efficient
dynamic testing



from test to validated
material cards



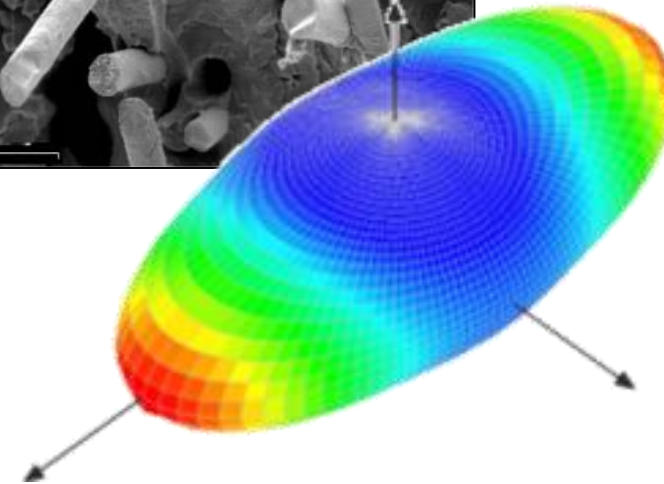
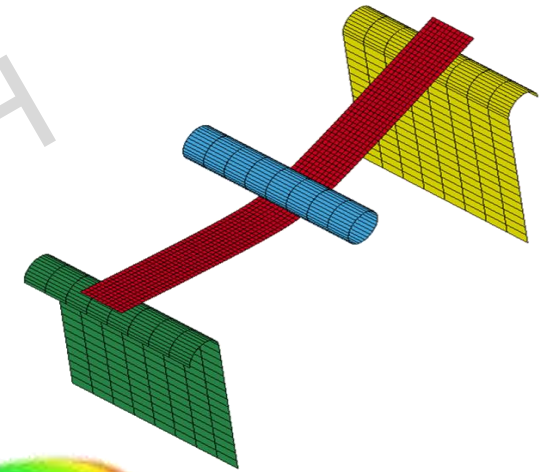
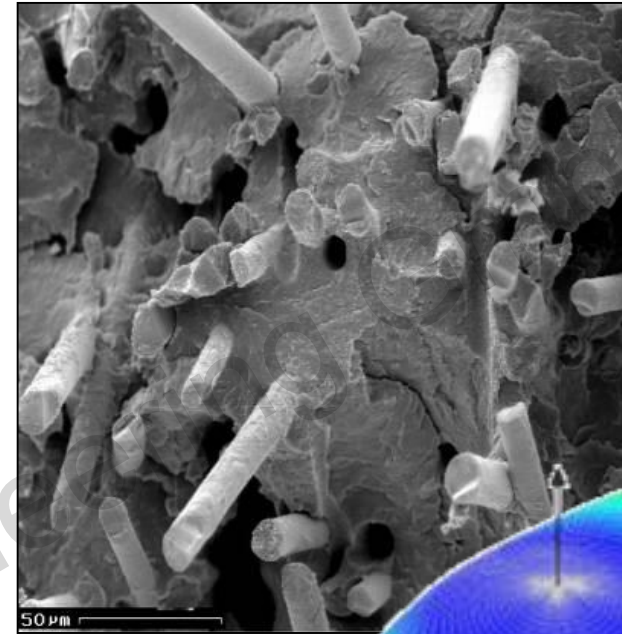
3D anisotropic
material cards



individual mapping
process information

Short and long fiber reinforced thermoplastics

- Motivation
- Manufacturing influence
- Material model approaches
- Material characterization
- Casestudy - sleeve

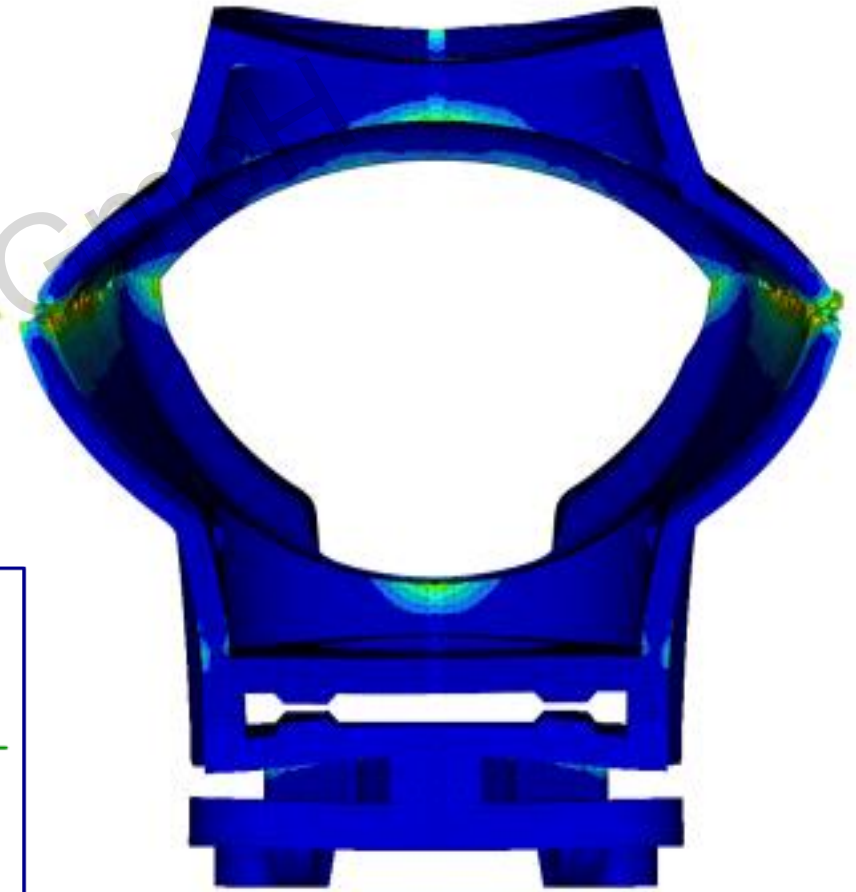
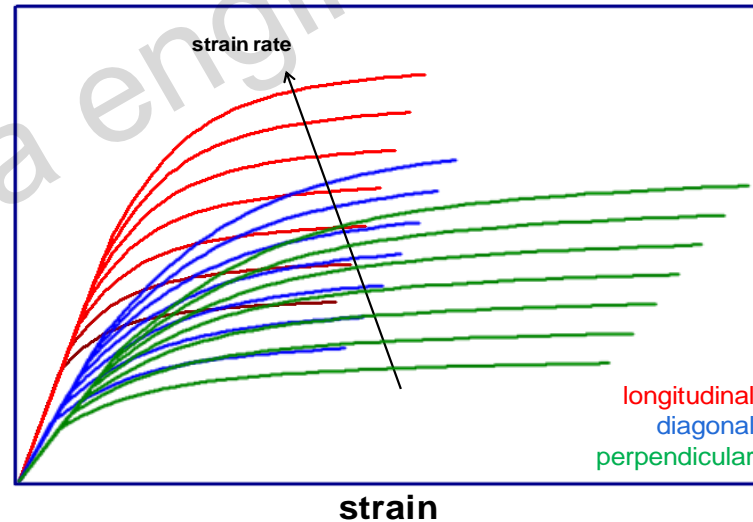


© at 4a engineering

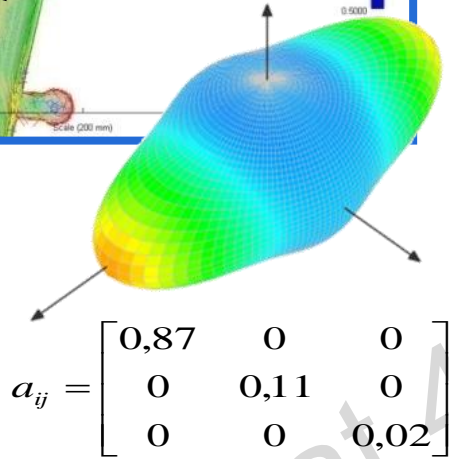
Motivation – current simulation standard



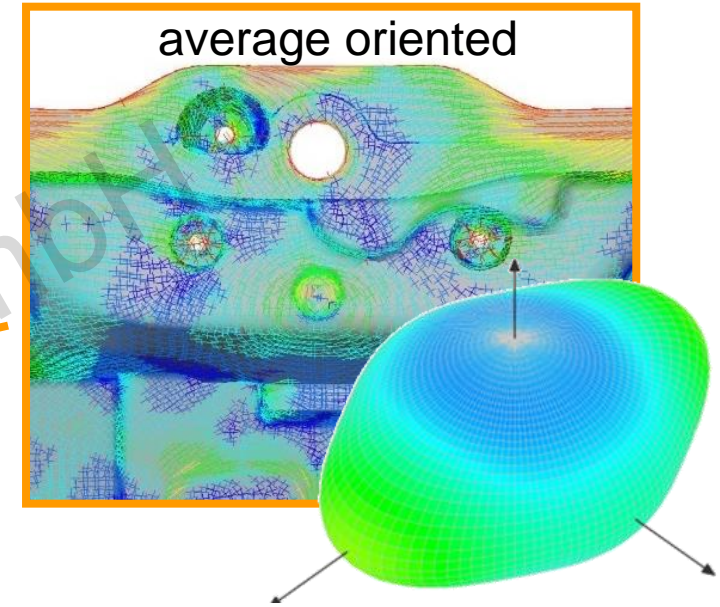
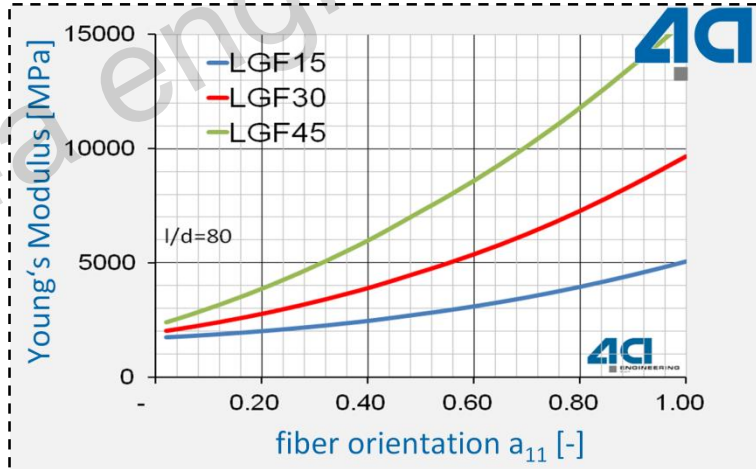
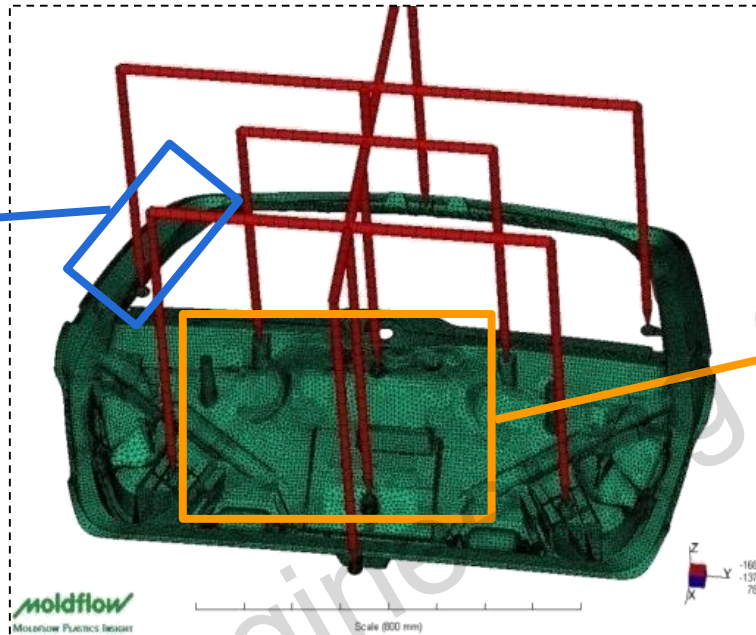
isotropic



Fiber orientation – development in typical part



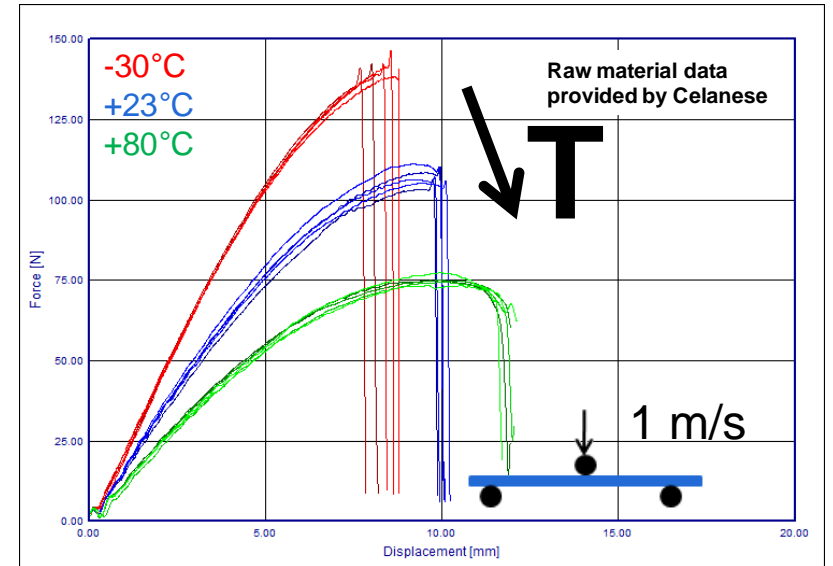
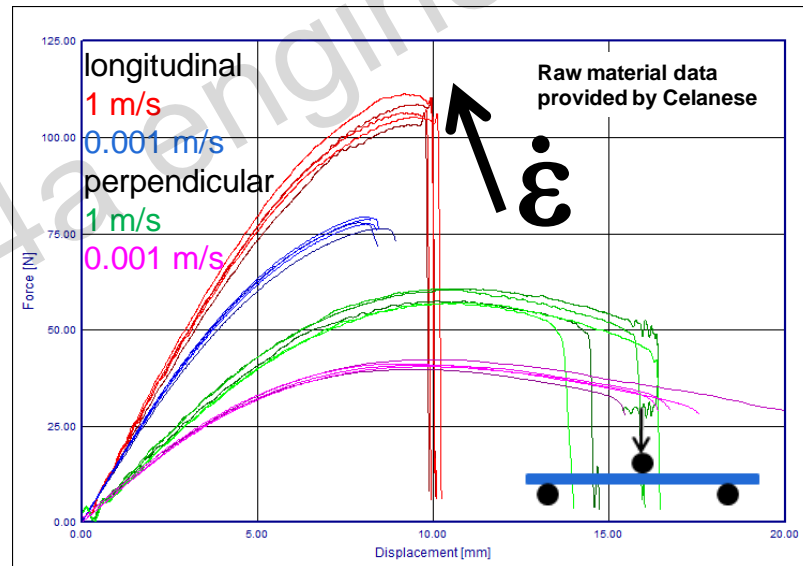
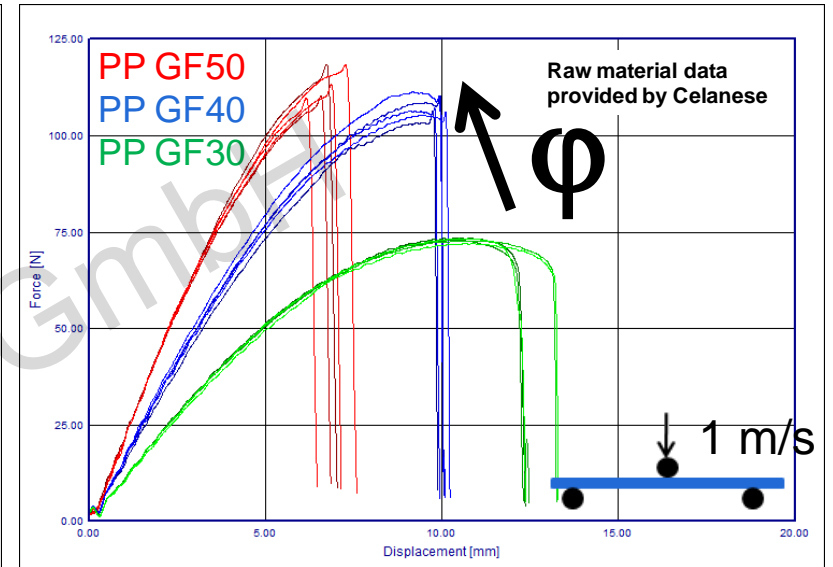
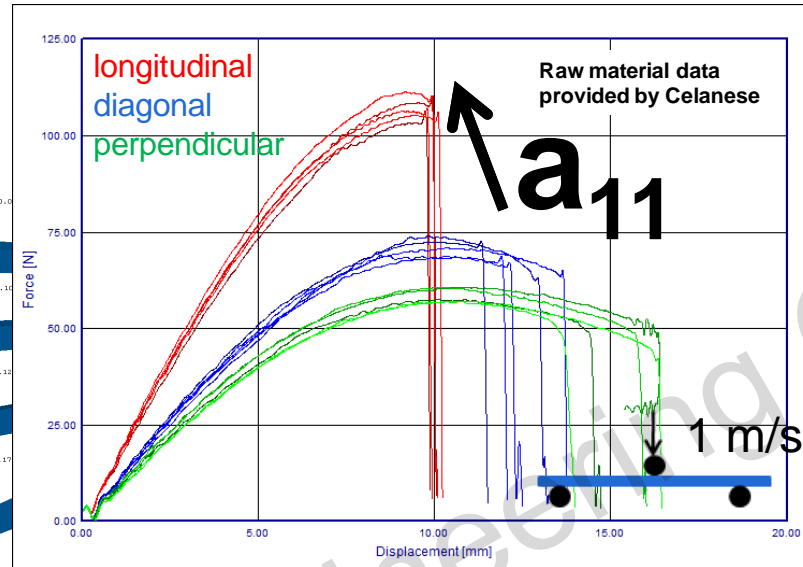
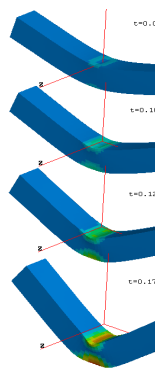
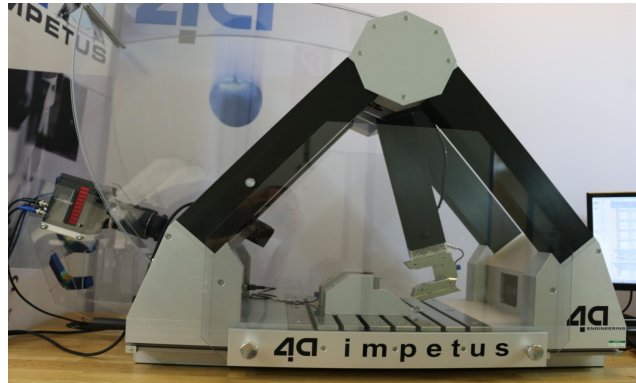
$$a_{ij} = \begin{bmatrix} 0,87 & 0 & 0 \\ 0 & 0,11 & 0 \\ 0 & 0 & 0,02 \end{bmatrix}$$



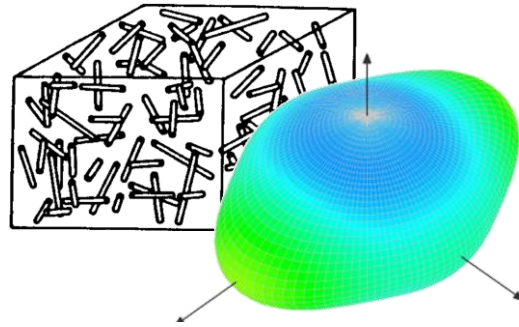
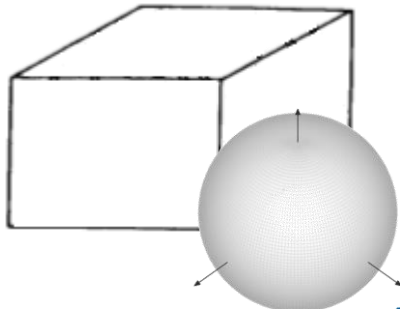
$$a_{ij} = \begin{bmatrix} 0,66 & 0 & 0 \\ 0 & 0,32 & 0 \\ 0 & 0 & 0,02 \end{bmatrix}$$

Source: P. Reithofer - Integrative Simulation – Berücksichtigung der prozessbedingten Anisotropie, 4a Technologietag 2011

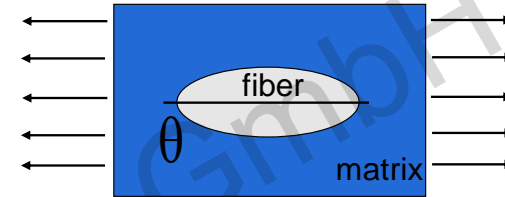
Typical material behavior – SFRT / LFRT



Typical material models in LS-DYNA



$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$



Eshelby Tensor

macro scale

constitutive law

Mises plasticity

- quick & d...
- critic...
- orientation

***MAT = 024**

→ composition

elastic

- orthotropic
- anisotropic
- elastic
- plasticity

***MAT = 157**

α – orientation dependent

micro scale

homogenization

M... matrix

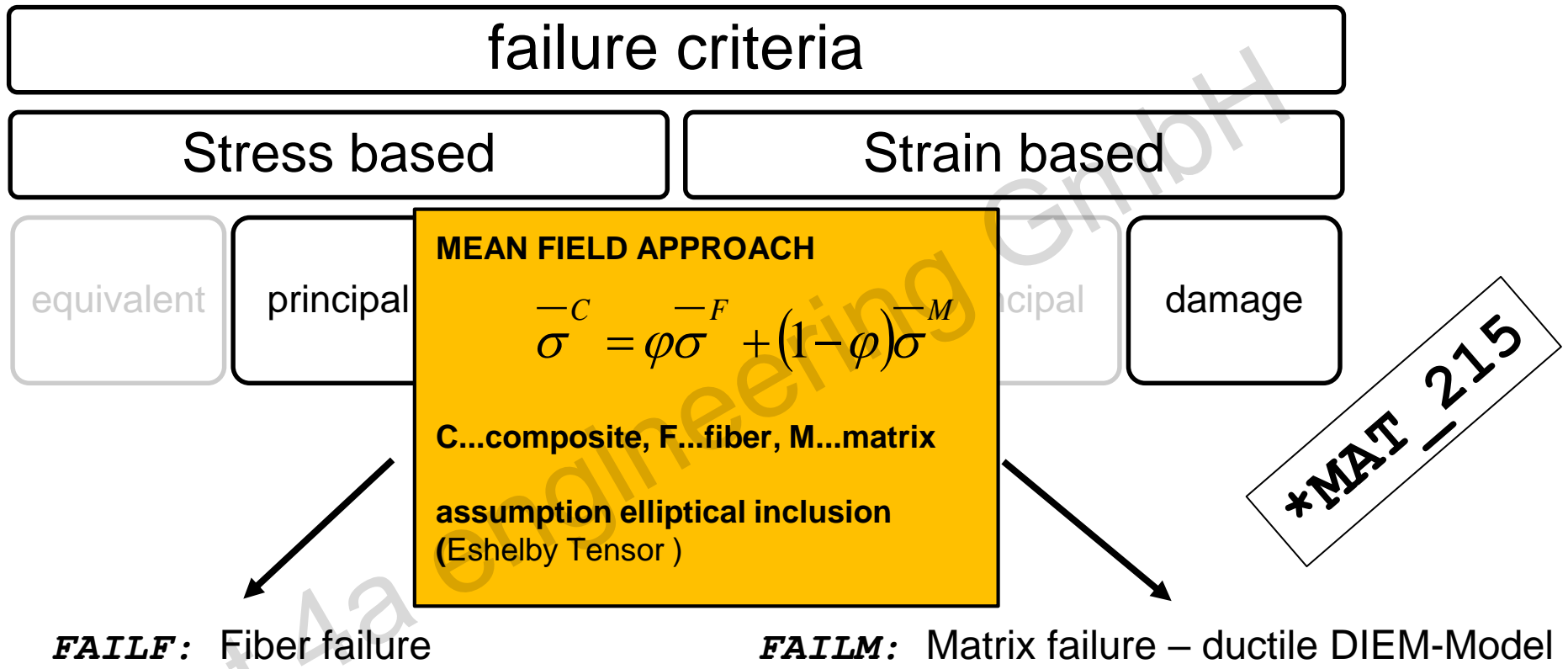
- isotropic elastic
- viscoplastic

F... fiber

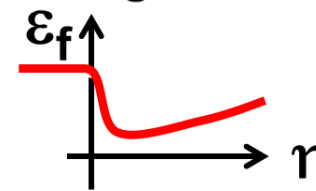
- isotropic
- plastic

***MAT = 215**

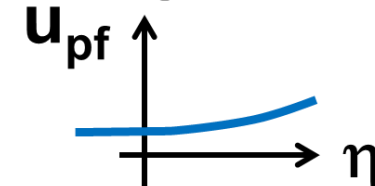
Micro mechanical motivated failure



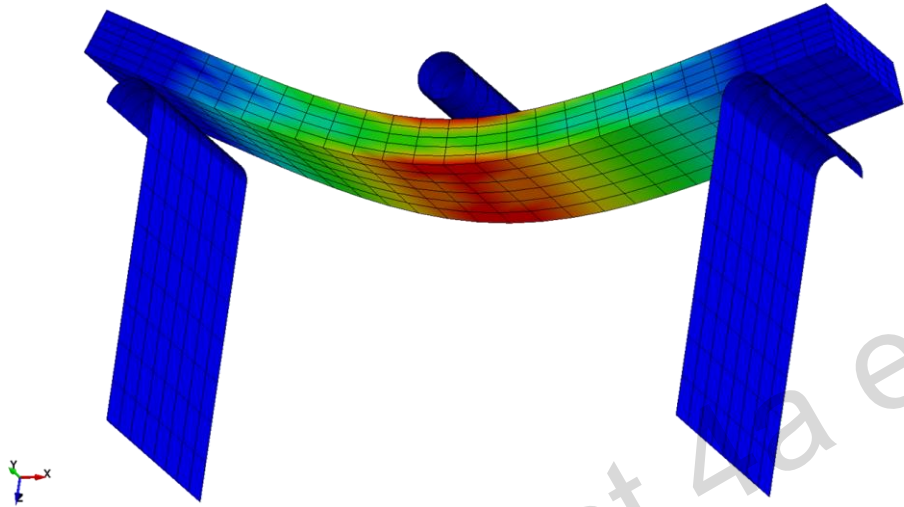
Damage Initiation



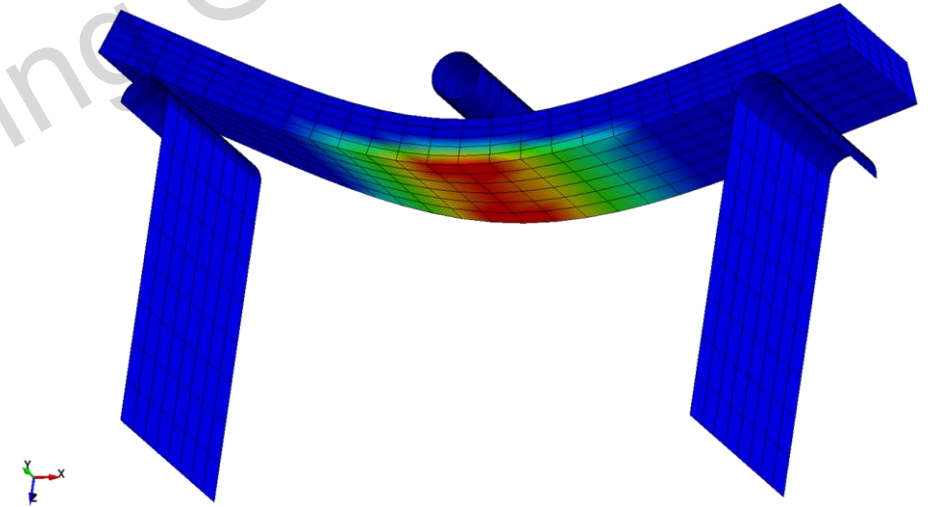
Damage Evolution



Micro mechanical motivated failure



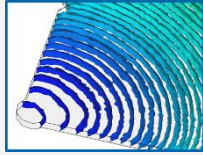
*History#6 (step8: 0-0.13):
Fiber damage init.*



*History#4 (step8: 0-0.81):
dm - matrix damage init.*

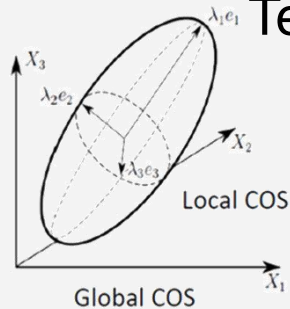
Material models – present approaches

Process simulation



$$a_{ij} = \begin{bmatrix} a_{xx} & a_{xy} & a_{xz} \\ & a_{yy} & a_{yz} \\ & & a_{zz} \end{bmatrix}$$

Tensor 2nd order



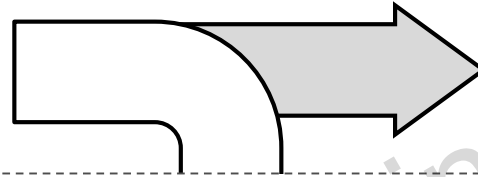
CADMOULD
3D-F SIMULATION

Moldex3D
MOLDING INNOVATION

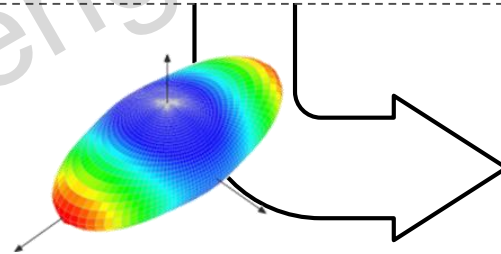


MOLDFLOW

FIBERMAP

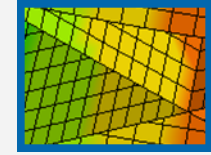


$$C^{-1} = \begin{bmatrix} \frac{1}{E_1} & -\frac{\nu_{21}}{E_2} & -\frac{\nu_{31}}{E_3} & 0 & 0 & 0 \\ -\frac{\nu_{12}}{E_1} & \frac{1}{E_2} & -\frac{\nu_{32}}{E_3} & 0 & 0 & 0 \\ -\frac{\nu_{13}}{E_1} & -\frac{\nu_{23}}{E_2} & \frac{1}{E_3} & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1}{G_{23}} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{G_{31}} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1}{G_{21}} \end{bmatrix}$$



MICROMECH

Structural simulation

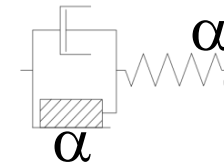


Homogenization (Micro Scale)
Mean Field Theory

$$\bar{\sigma}^C = \phi \bar{\sigma}^F + (1 - \phi) \bar{\sigma}^M$$

*MAT_215

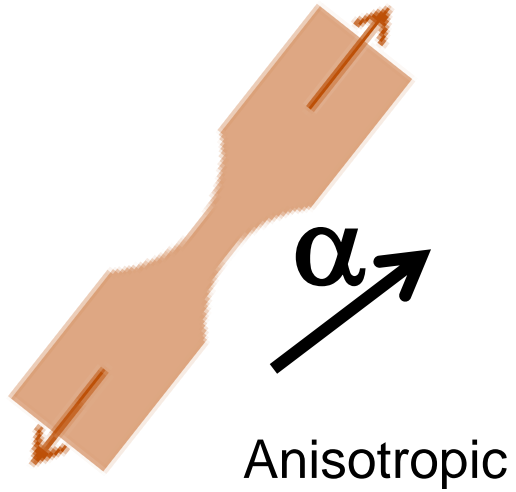
Composite (Macro Scale)
Hill Plasticity



*MAT_157

LSTC
Livermore Software
Technology Corp.
LS-DYNA®

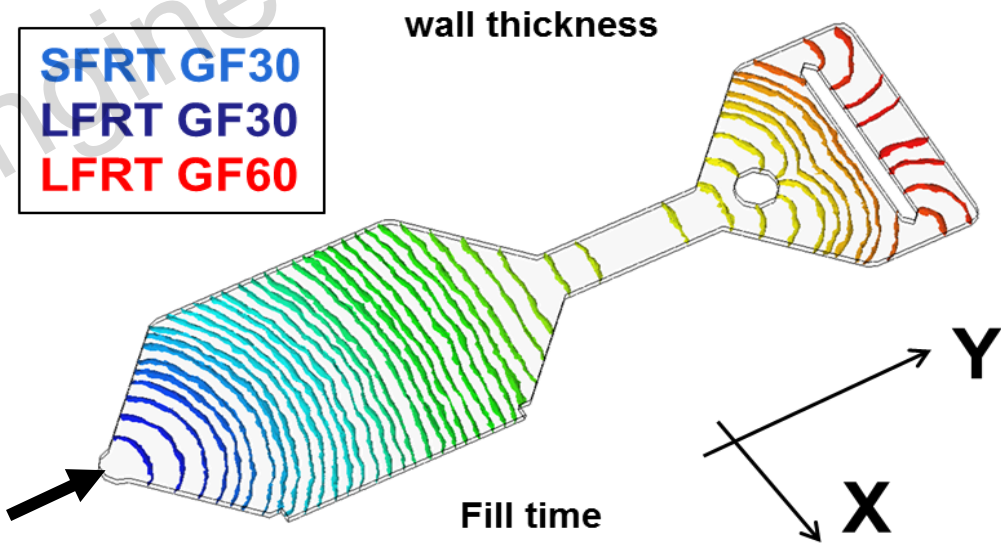
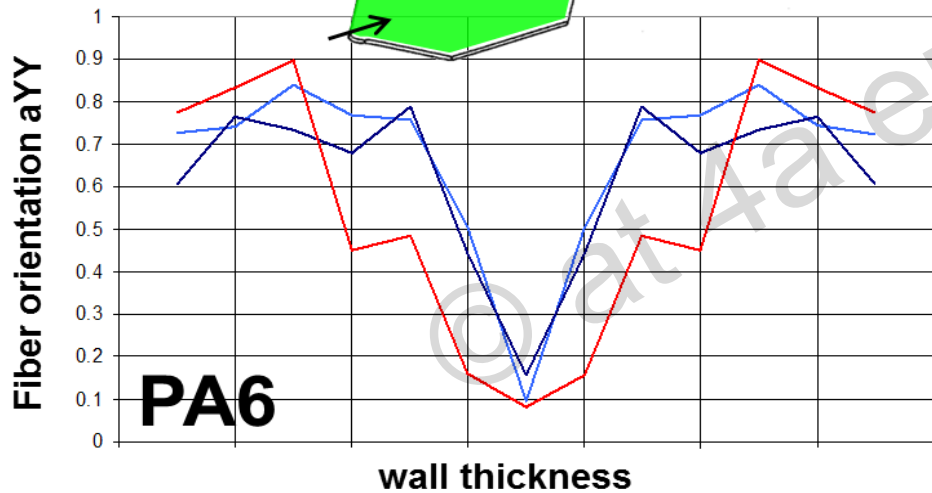
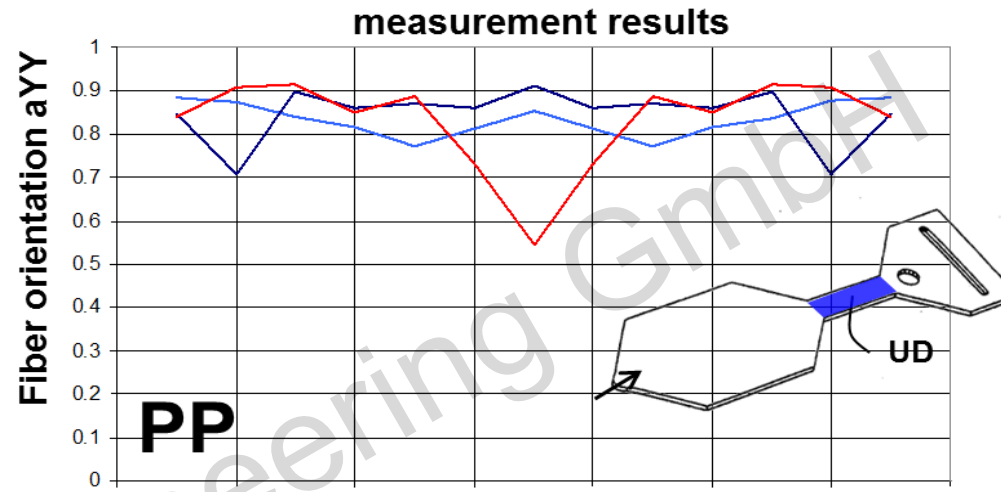
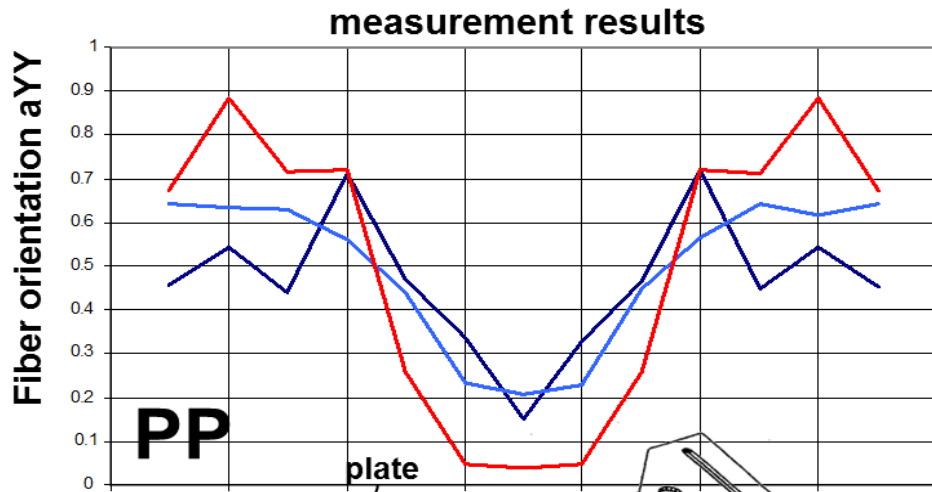
From test to material card



Why not tension (only)?

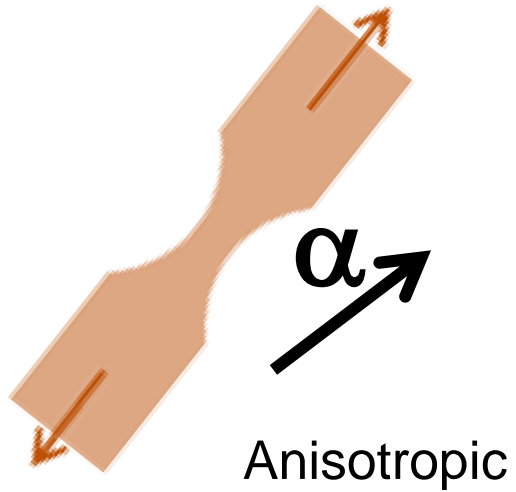
© at 4a engineering GmbH

Fiber orientation – development based on flow / viscosity

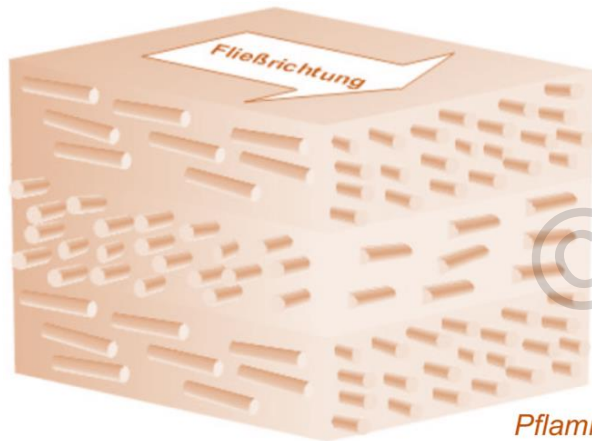
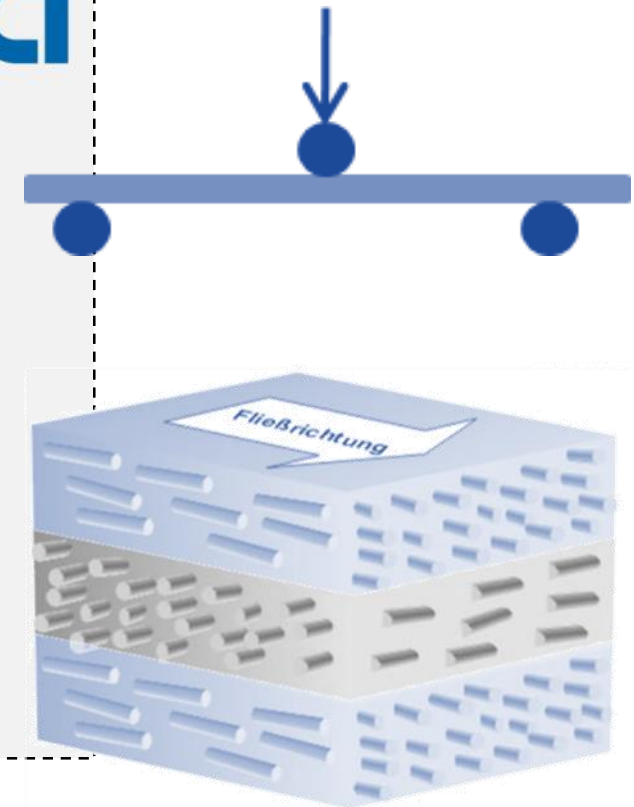
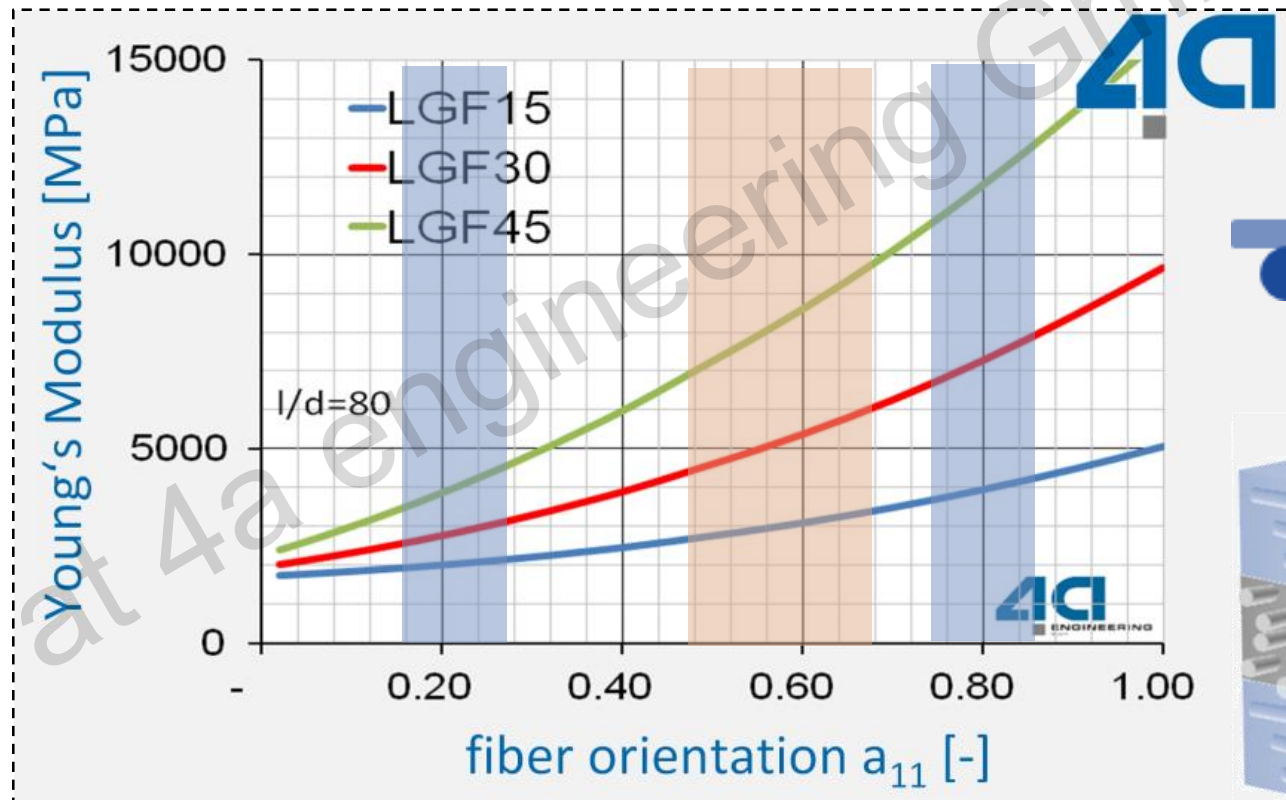


Source: 4a – EU Nelofite project , 2005

From test to material card

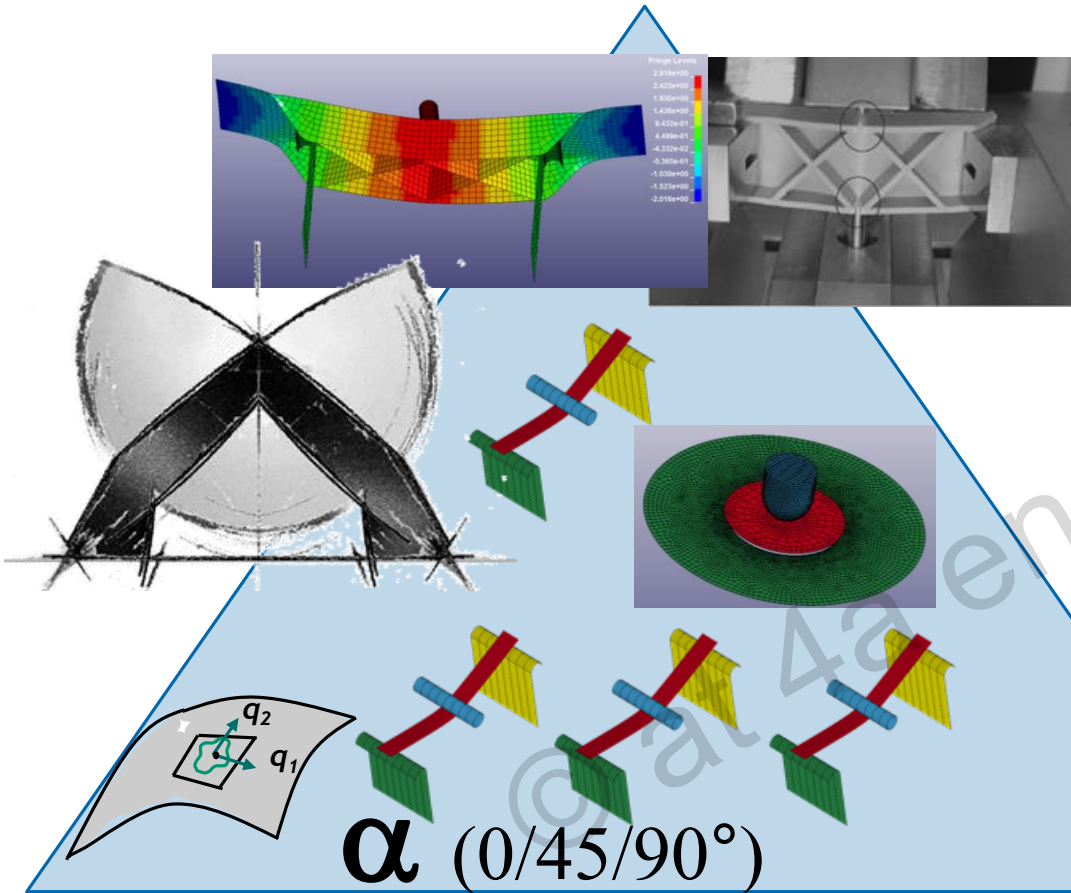


Why not tension (only)?

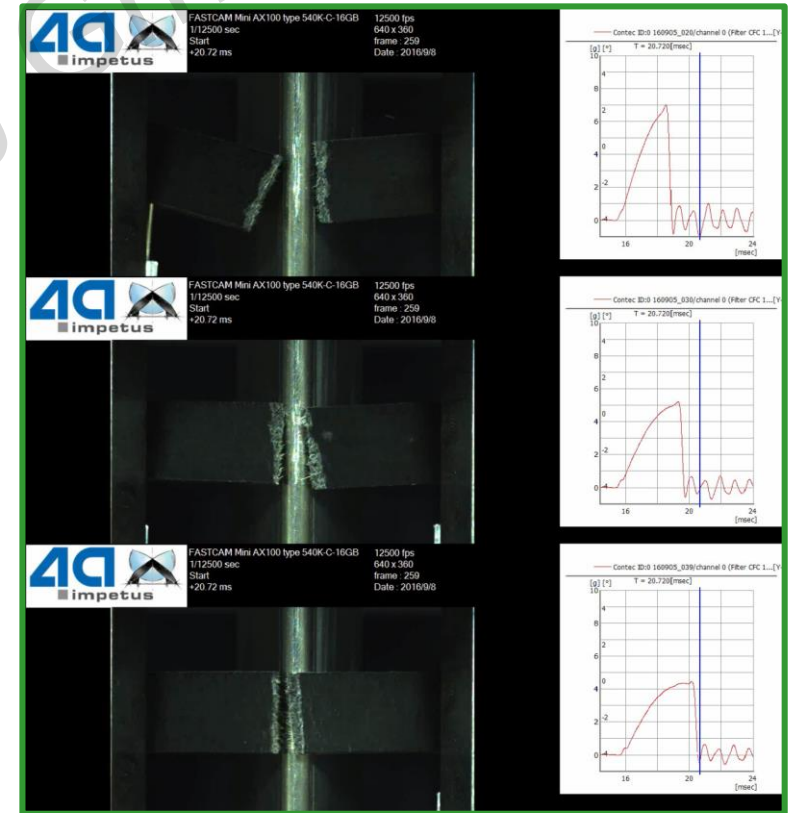
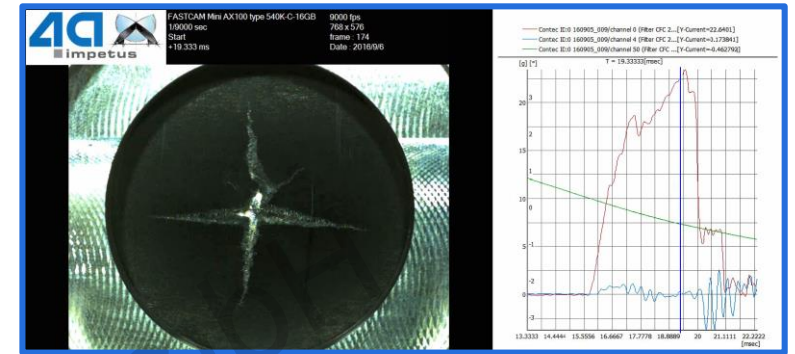
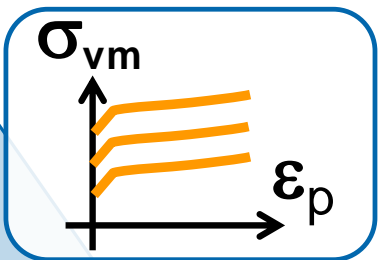
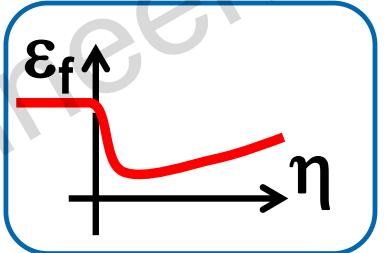


Pflamm-Jonas 2001

From test to material card

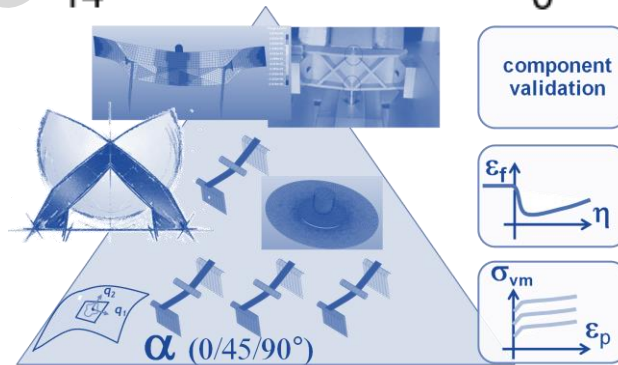
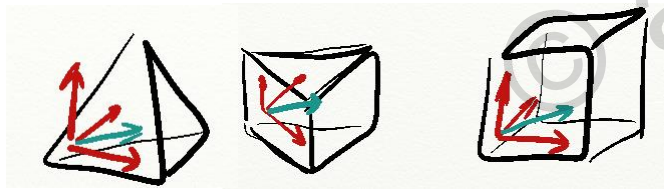
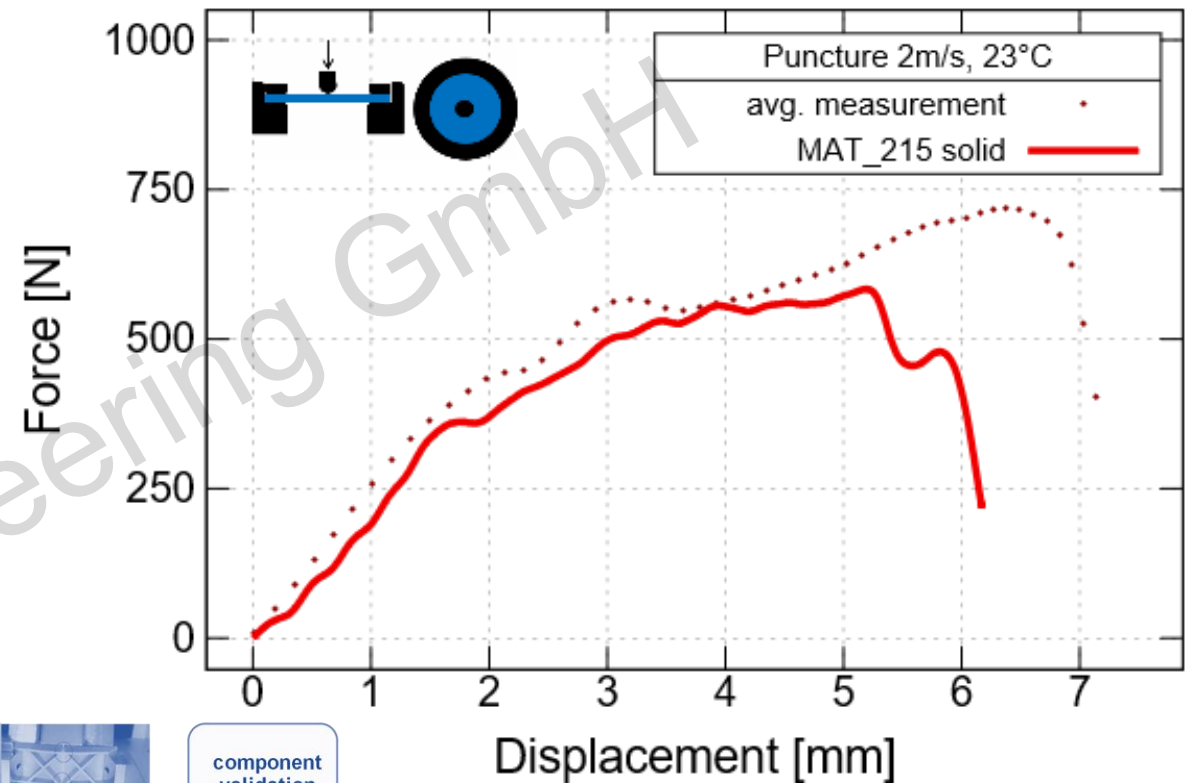
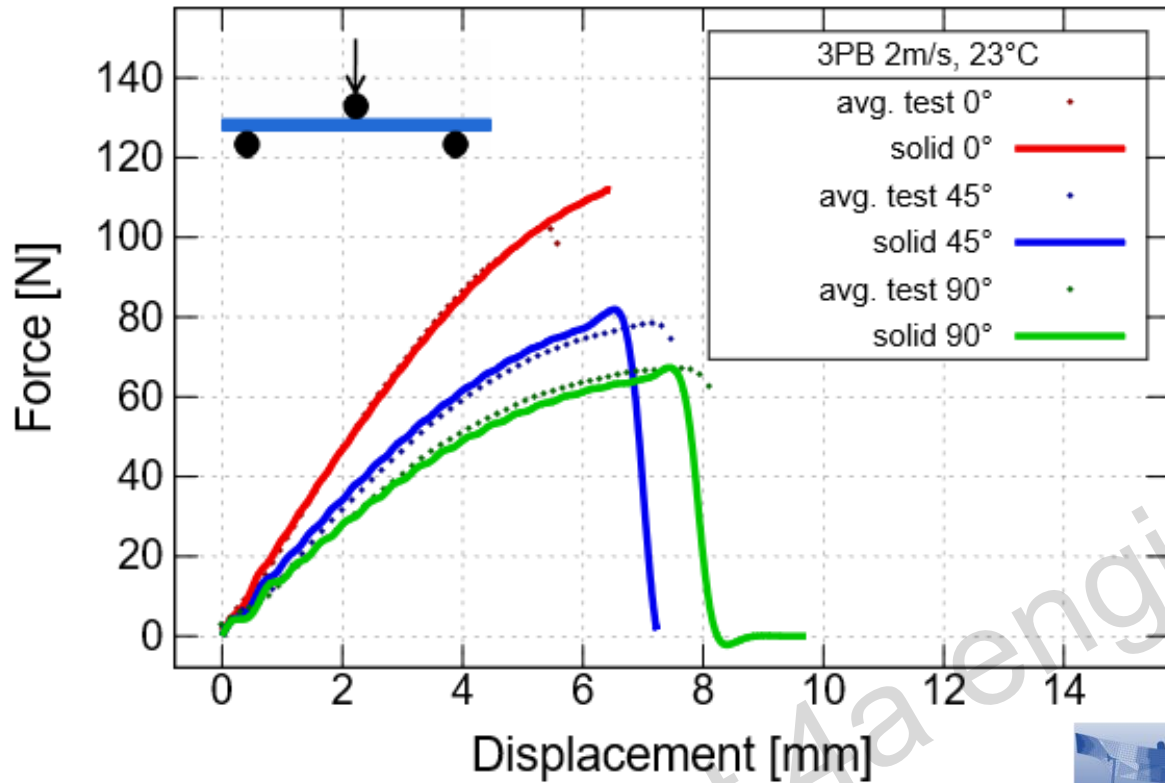


component validation



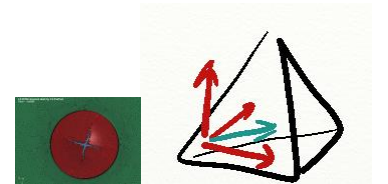
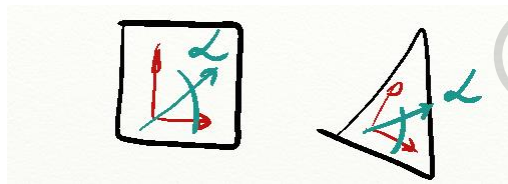
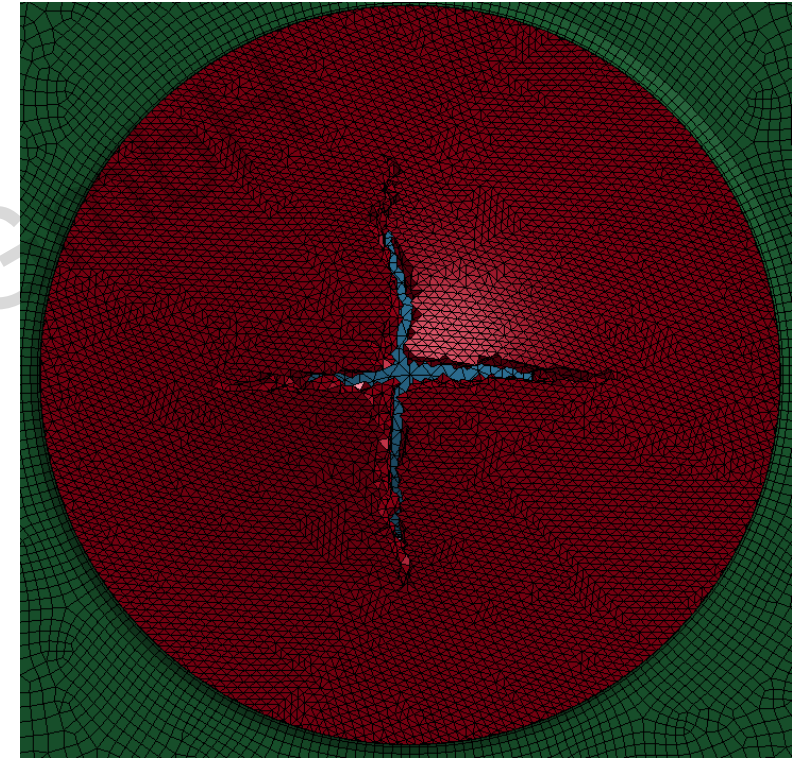
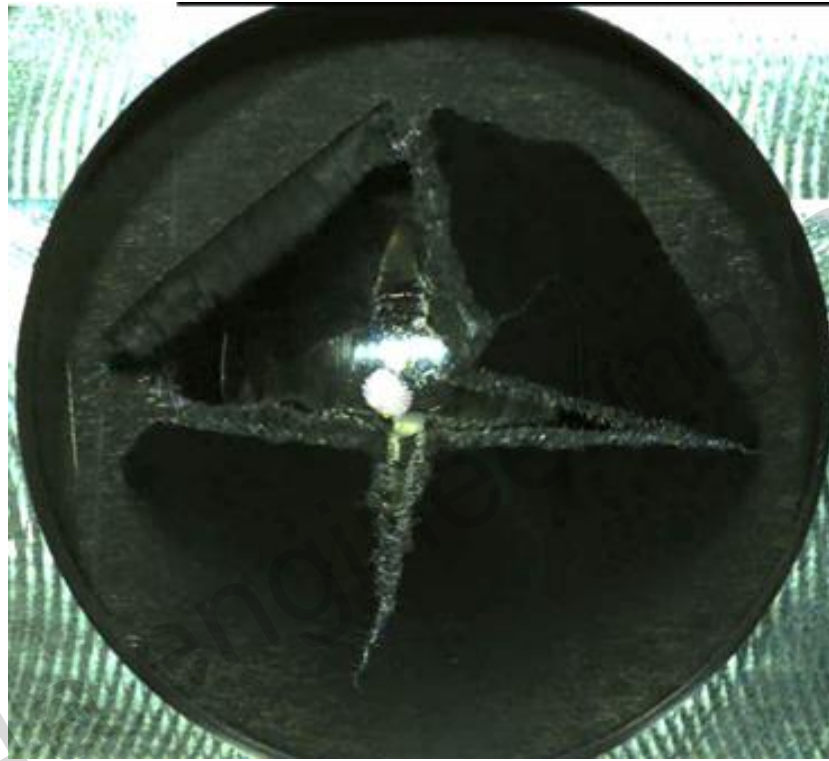
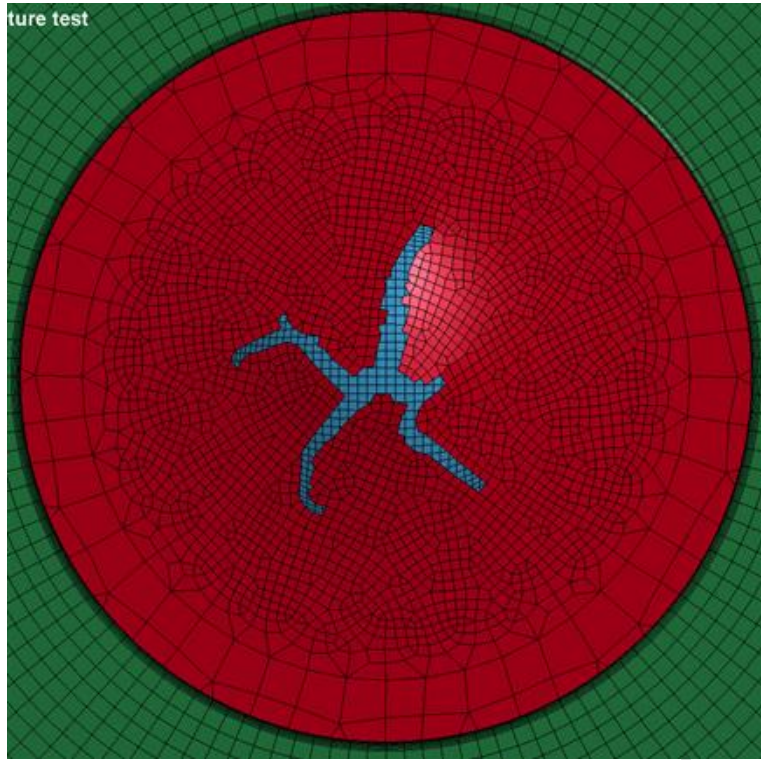
See more: P Reithofer, et.al., Versagen von faserverstärkten Kunststoffen bei dynamischer Beanspruchung, 4a Technologietag -2017

From test to material card: PP LGF30

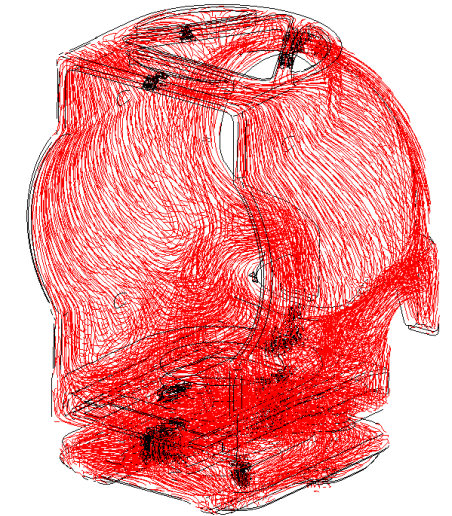
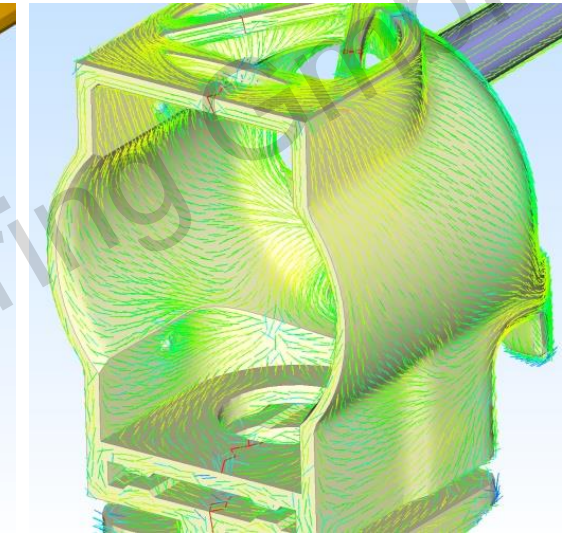
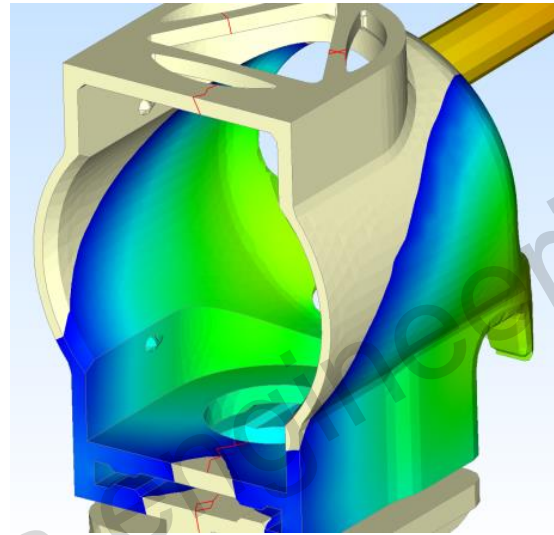
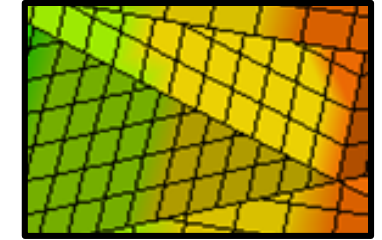
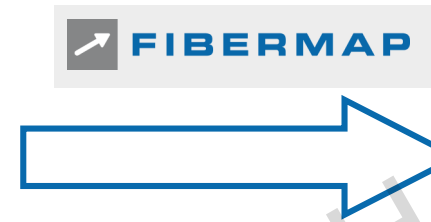
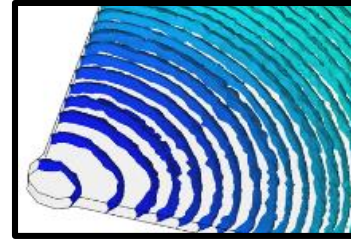
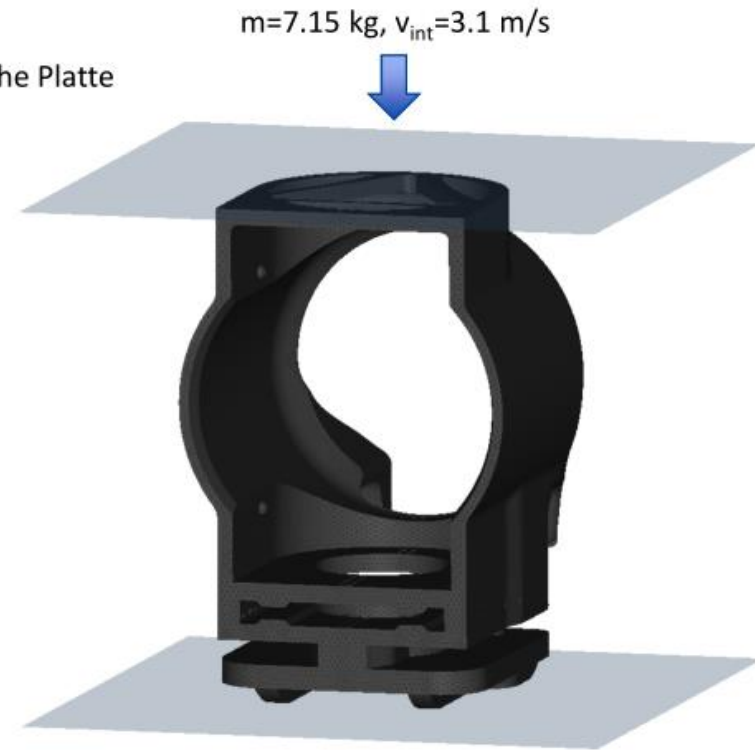


..... averaged test curves
 — result of simulation

Validation for PP LGF30



Casestudy - sleeve



Typische Elementgröße: 0.25mm
Elementtyp: Tetrahedron Type 10
Elementanzahl: 469 470



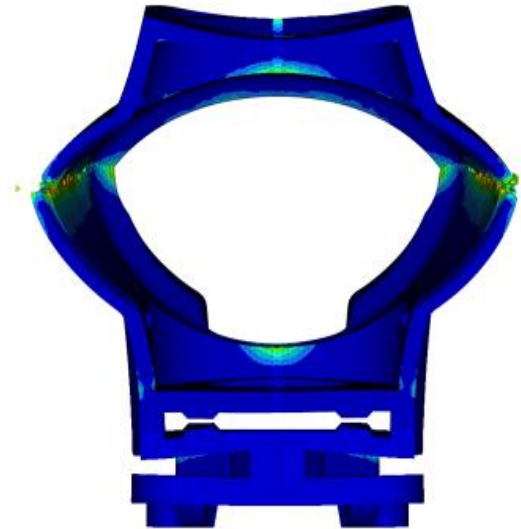
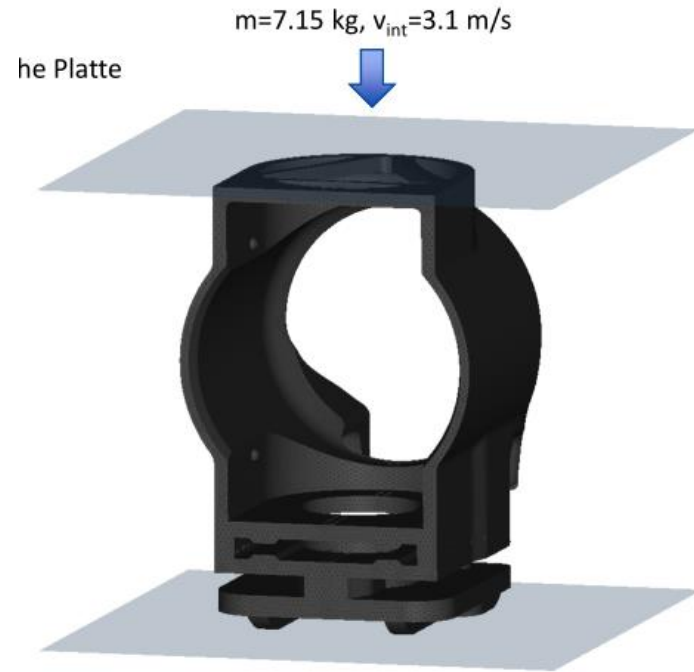
See more: R. Steinberger, et.al. Hirtenberger Automotive Group – *Considering the Local Anisotropy of Short Fiber Reinforced Plastics*, European Dynaforum 2017

Casestudy - sleeve

test

**MAT_157/215*
local anisotropy

**MAT_24*
isotropic



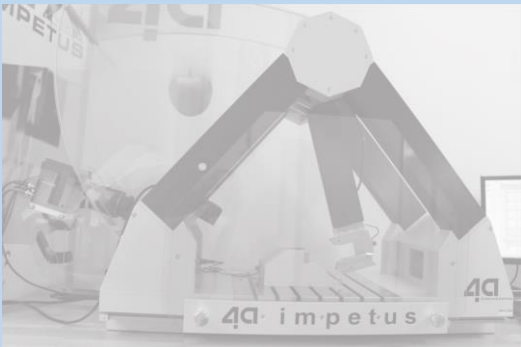
Typische Elementgröße: 0.25mm
Elementtyp: Tetrahedron Type 10
Elementanzahl: 469 470



See more: R. Steinberger, et.al. Hirtenberger Automotive Group – *Considering the Local Anisotropy of Short Fiber Reinforced Plastics, European Dynaforum 2017*

Intelligent reliable solutions for plastics, composites, metals, foams, ...

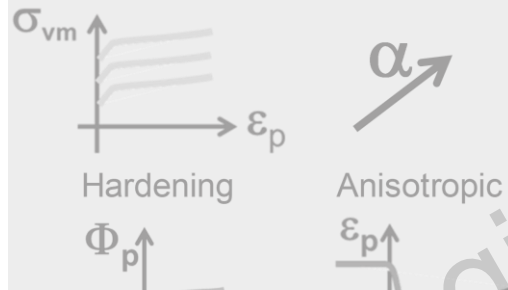
 **IMPETUS**



Composites (Carbon)

efficient
dynamic testing

 **VALIMAT**



from test to validated
material cards

 **MICROMECH**



3D anisotropic
material cards

 **FIBERMAP**



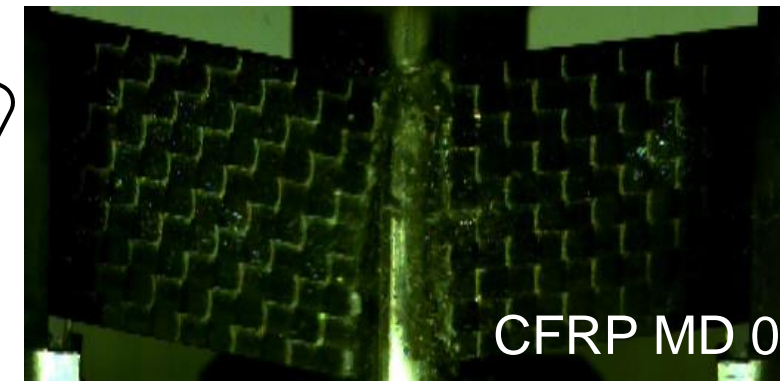
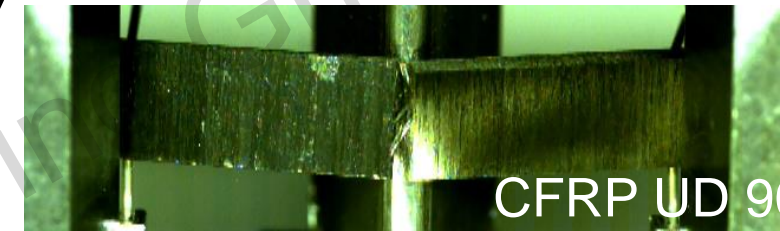
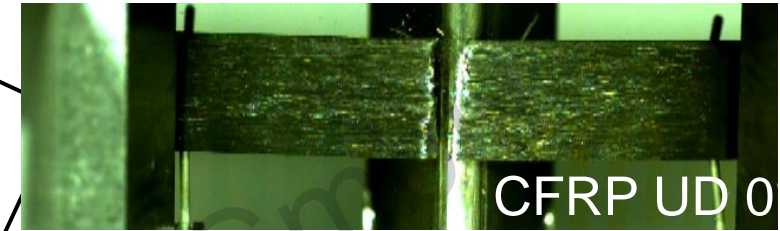
individual mapping
process information

Composites – typical test setup

specimen		0°	45°	90°
	UD	static		
	MD		static, cyclic	
	UD	static, dynamic		
	MD	static, dynamic		
	MD	Puncture		

Material Card

Validation



© at 4a engineering

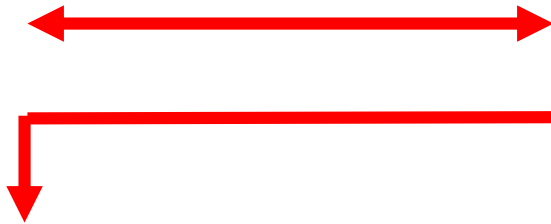
Composites – available LS-DYNA material models



22	Orthotropic	None	None	None	Orientation dependent	Carbon, Glass, Kevlar endless & fabric
54/55	Orthotropic	None	Elastic Orthotropic	Strength	Chang-Chang/ Tsai-Wu Orientation dependent	
58	Orthotropic	None	Elastic Orthotropic	Strength, Stiffness	mod. Hashin Orientation dependent	
158	Orthotropic	None	Elastic Orthotropic	Visco-elasticity	Orientation dependent	
261	Orthotropic	None	Elastic Orthotropic	None	failure Pinho (Puck) Orientation dependent	
262	Orthotropic	None	Elastic Orthotropic	None	failure Camanho (Puck) Orientation dependent	

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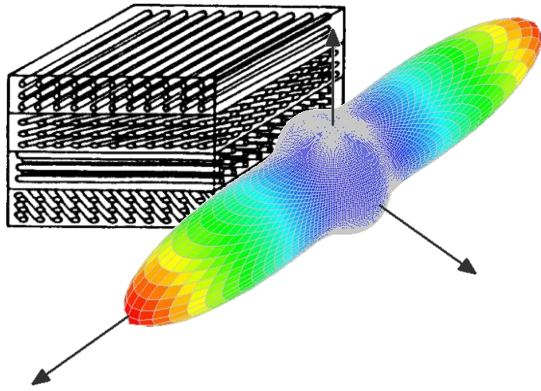
***Part_Composite**



Material behaviour	
Material source	Implemented
Elasticity	Not isotropic elastic
Plasticity	Not selected
Failure/Damage	Not selected
Material card	
Deformation	*MAT_COMPOSITE_DAMAGE (*MAT_022)
Damage/Failure	*MAT_ENHANCED_COMPOSITE_DAMAGE (*MAT_054)
Materialcard id	*MAT_LAMINATED_COMPOSITE_FABRIC (*MAT_058)
Density	*MAT_RATE_SENSITIVE_COMPOSITE_FABRIC (*MAT_158)
Plasticity	*MAT_LAMINATED_FRACTURE_DAIMLER_PINHO (*MAT_261)
Function (Hardening, Elastic curve form)	*MAT_LAMINATED_FRACTURE_DAIMLER_CAMANHO (*MAT_262)
Strain rate dependency	*MAT_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_157)
Micromec	*MAT_MICROMECC (*MAT_215)
Fracture	*MAT_MICROMECC (*MAT_215)+Carbon
Postfracture	None

Model settings	
Material	
Idealization	
Material behaviour	
Material source	Implemented
Materialcardcase	7300_MAT22
Damage/Failurecase	Chang Chang
Materialcard id	1000000
Density	1480
Plasticity	None
Function (Hardening, Elastic curve form)	
Strain rate dependency	None
Micromec	Endless fiber reinforced plastics
Matrix	
Density of the matrix	1093
E-Modulus	3000
Poisson's ratio	0.3
Yield strength	50
Strength at Break	70
Failure strain	0.05
Fiber	
Fillerlength	20000
Fillerdiameter	20
Phi or Psi	φ
Phi	58
Psi	71.7
Fillermaterial	T300
Orientation	
Fillerorientationtype	UD
Strength	
Strength evaluation	
XT	2300
XC	2000
Fracture	
Postfracture	Composite

Available LS-DYNA materialcards in VALIMAT™



$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$

C...composite, F...fiber, M...matrix

160826_004	
Material	Designvariablen
Model settings	
Material	
Idealization	
Material behaviour	
Material source	Implemented
Material card	*MAT_COMPOSITE_DAMAGE (*MAT_022)
Materialcardcase	7500_MAT22
Damage/Failurecase	Chang Chang
Materialcard id	1000000
Density	1480
Plasticity	None
Function (Hardening, Elastic curve form)	
Strain rate dependency	None
Micromec	Endless fiber reinforced plastics
Matrix	
Density of the matrix	1093
E-Modulus	3000
Poisson's ratio	0.3
Yield strength	50
Strength at Break	70
Failure strain	0.05
Fiber	
Fillerlength	20000
Fillerdiameter	20
Phi or Psi	φ
Phi	58
Psi	71.7
Filler material	T300
Orientation	
Fillerorientationtype	UD
Strength	
Strength evaluation	Fiber strength
XT	2300
XC	2000
Fracture	Composite
Postfracture	None

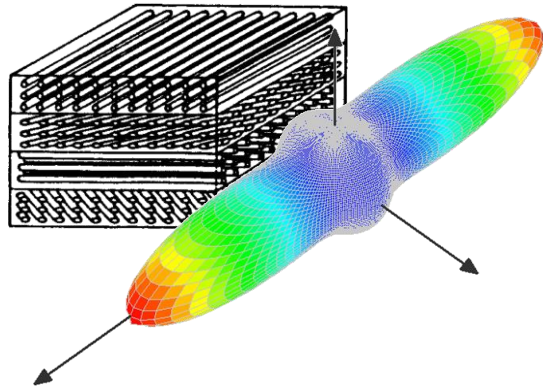
Matrix properties

Filler properties

Orientation

Strength

© at 4a engineering GmbH



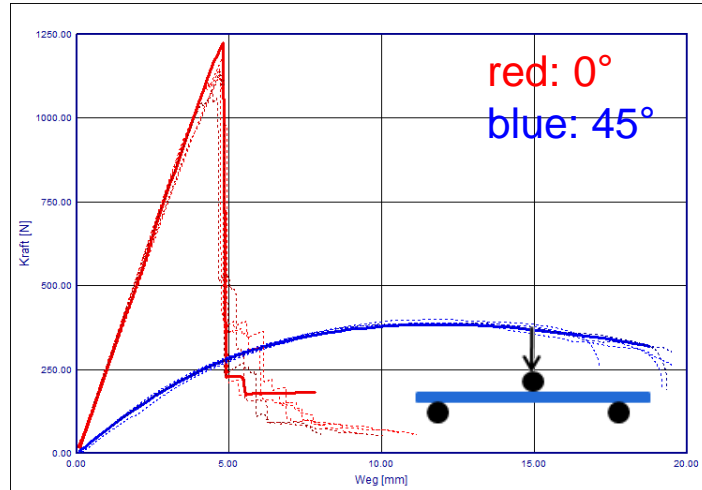
$$\bar{\sigma}^C = \varphi \bar{\sigma}^F + (1 - \varphi) \bar{\sigma}^M$$

C...composite, F...fiber, M...matrix

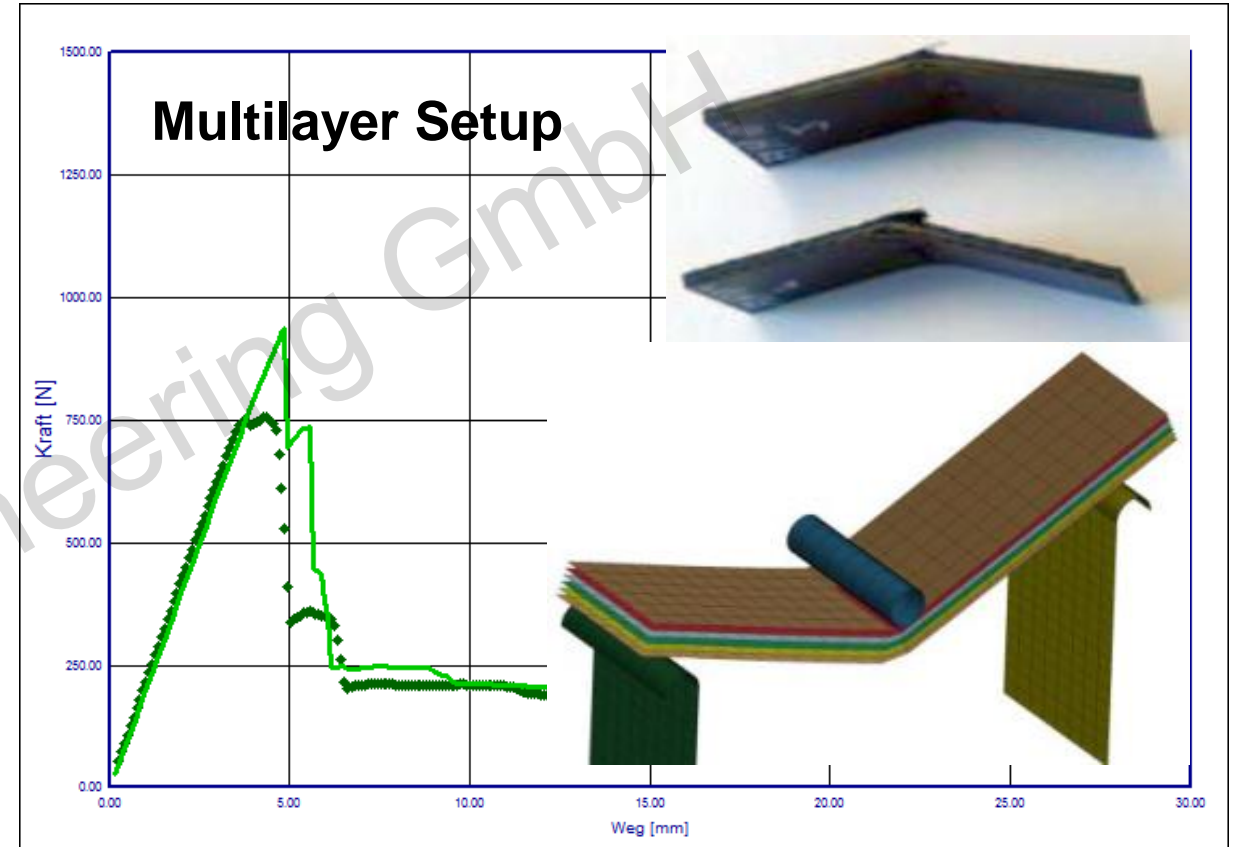
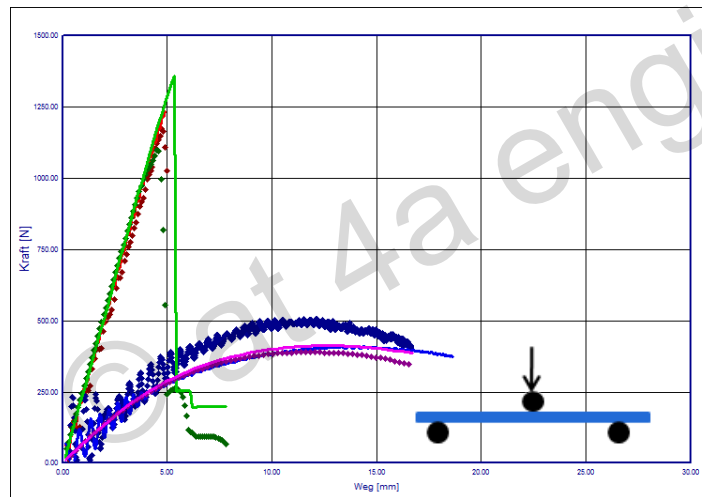
Typical Design Variables for *MAT_022

Name	Start	const...	from	to	Variance	Condi...	Description
^ GroupName: 10_elasticity							
c_E11	MMEC	<input type="checkbox"/>	100000	180000	(NULL)		young modulus tensile in 1 direction
c_E22	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		young modulus tensile in 2 direction
c_E33	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		young modulus tensile in 2 direction
c_nue21	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 21 plane
c_nue31	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 31 plane
c_nue32	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		poisson ration in 32 plane
c_G12	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 12 plane
c_G23	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 23 plane
c_G31	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		shear modulus in 31 plane
^ GroupName: 51_failure							
fc_R11T	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R11C	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R22T	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R22C	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		
fc_R12	MMEC	<input checked="" type="checkbox"/>	(NULL)	(NULL)	(NULL)		

Orientation



static versus dynamic

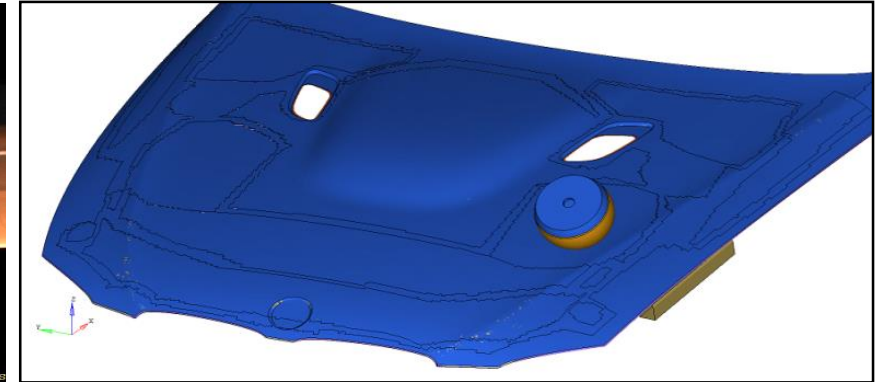
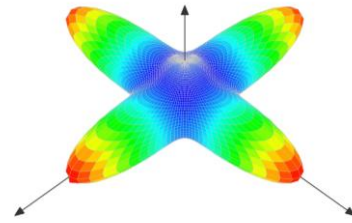


.... test
— simulation

P. Reithofer (4a engineering GmbH) & B. Fellner (MAGNA STEYR Engineering Austria) - Materialcharakterisierung von Composites; 4a Technologietag 2015

Composite – case study

- Front hood
 - Stiffness versus pedestrian safety
- Material card
 - Composite layup with anisotropic material behavior
 - Core material – Honeycomb different compression levels



[SOURCE: LINK to PAPER](#)

intelligent reliable solutions for plastics, composites, metals, foams, ...

 **IMPETUS**

 **VALIMAT**

 **MICROMECH**

 **FIBERMAP**

Thermoplastics

Fiber reinforced Plastics (SFRT & LFRT)

Composites (Carbon)

efficient
dynamic testing

from test to validated
material cards

3D anisotropic
material cards

individual mapping
process information

Summary

- LS-DYNA offers a lot of different material models for
 - thermoplastic materials
 - short and long fiber reinforced thermoplastics
 - classical composites
- all materials show different mechanical response dependent on different aspects like anisotropy, viscosity, temperature, moisture, ...
- material characterization must focus on the main behavior and material card generation must reflect that
- tools are needed to handle data and to fit complex failure models



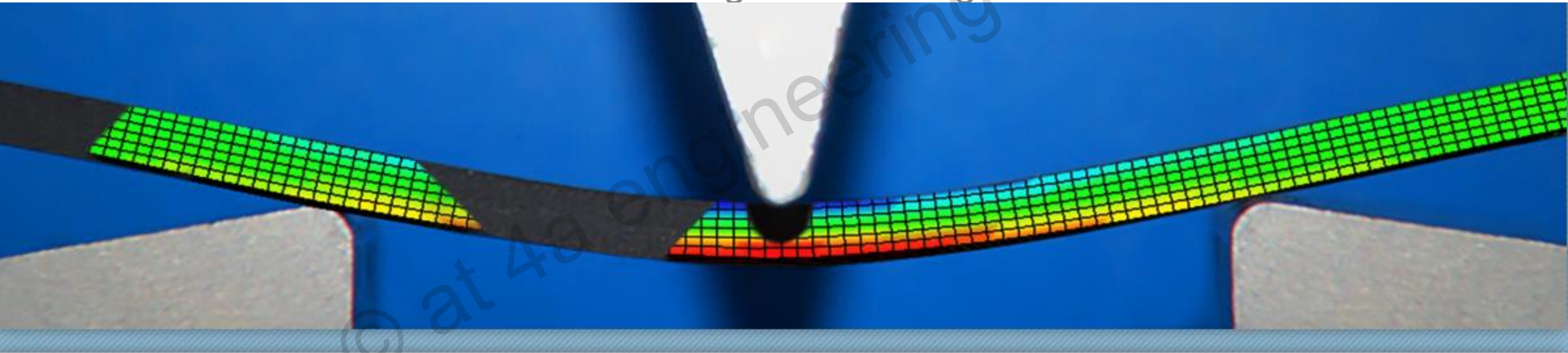
IMPETUS



VALIMAT

Thanks for your attention

[interested in more ...](#)
join us from 2.-4.3.2020
Salzburg Werfenweng



Technology Day 2020 - Plastics on the test rig - Testing and simulation

Appendix Additional overview

 **IMPETUS**  **VALIMAT**

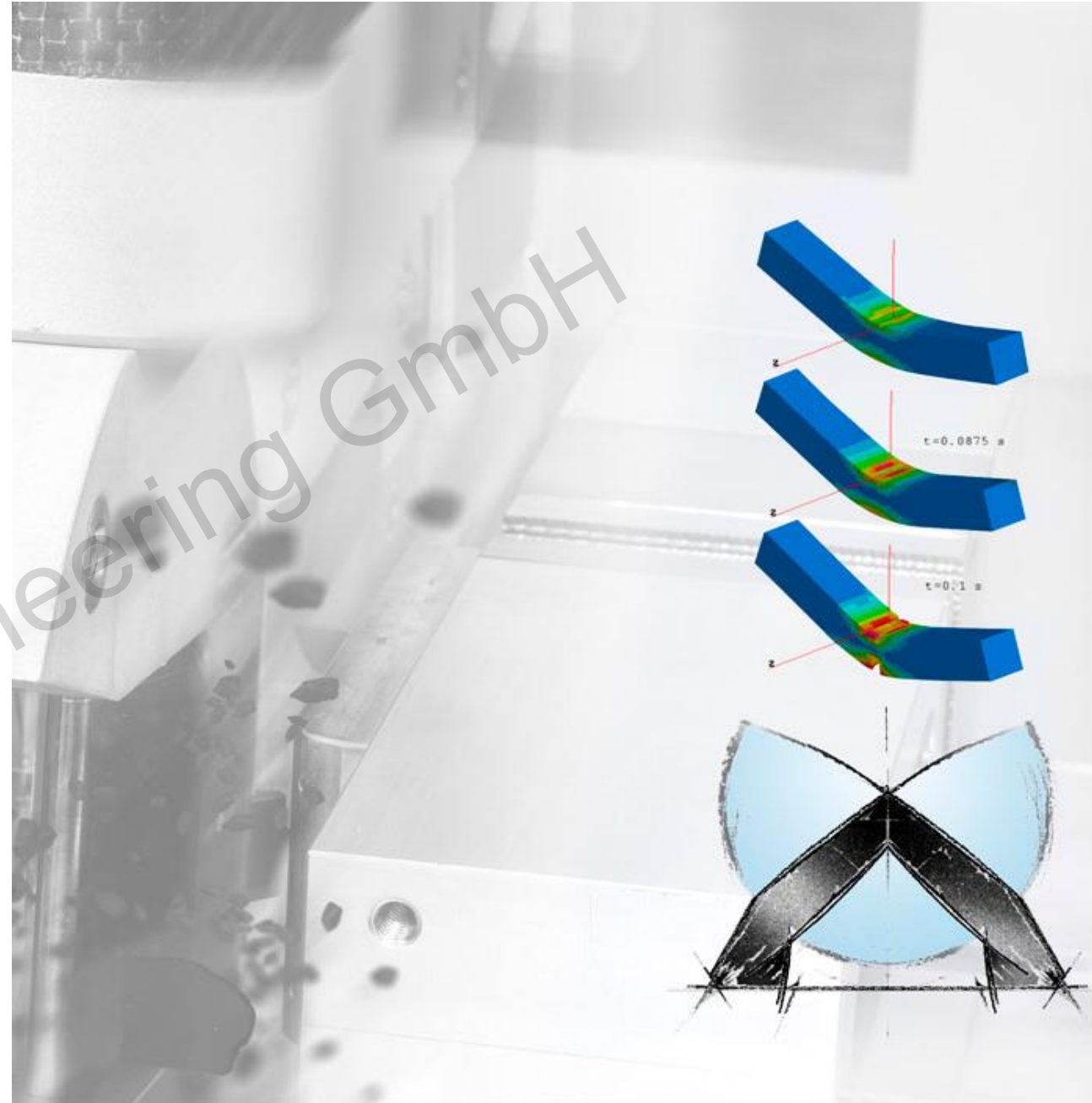
© at 4a engineering GmbH

efficient dynamic testing



IMPETUS

engineering plastics production
excellence in testing
simulation
concepts simulation
lightweight prototypes

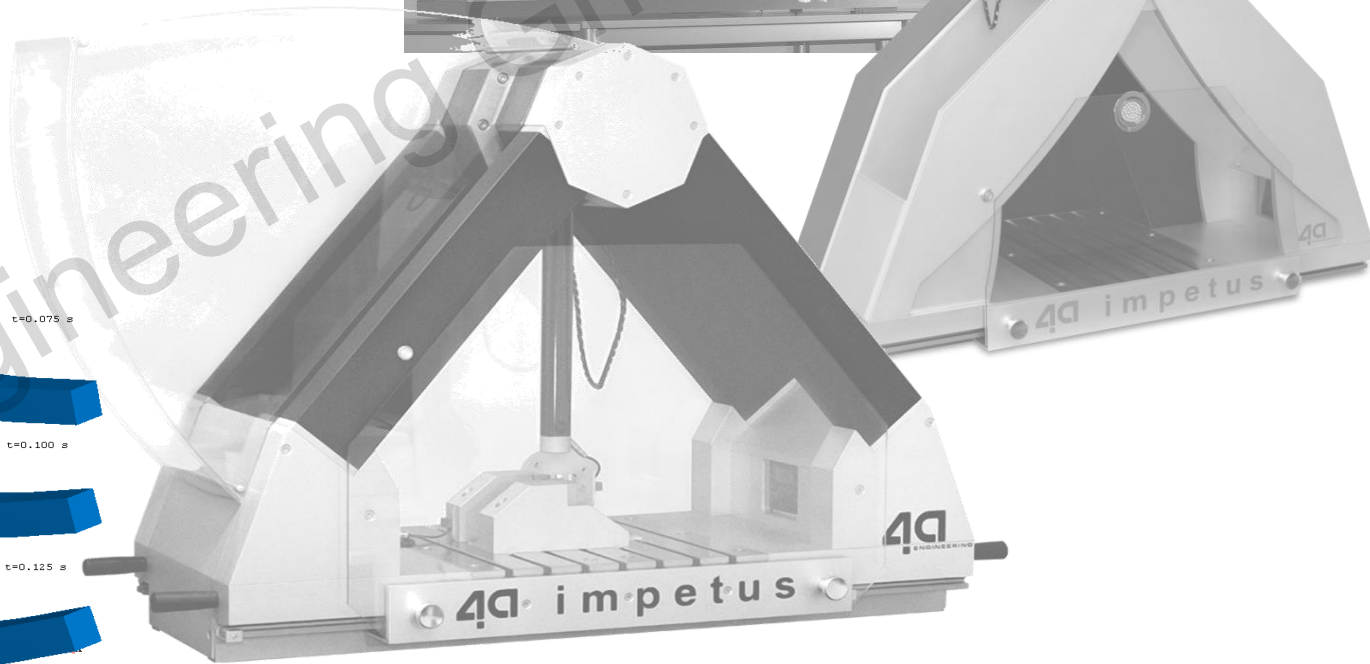
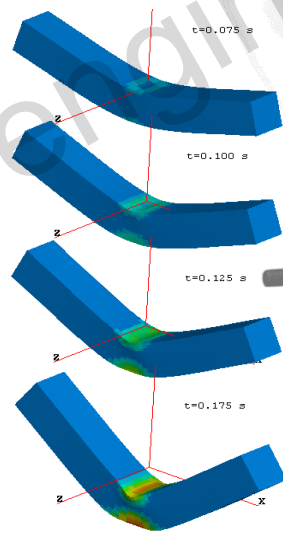


Efficient dynamic testing

- desktop testing device
- instrumented high-speed testing
 - acceleration \rightarrow force / displacement
- impact velocity 0.5 – 4.5 m/s



IMPETUS



IMPETUS™ data specification



technical specifications

maximum energy	50J
length of swing arm	500mm
mass of swing arm	1.5 - 3.0kg
impact velocity	0.5 - 4.4m/s

weights and dimensions

L x W x H	1400 x 600 x 850mm
mass	165kg

desk load and dimensions minimum required

L x W x H	1500 x 800 x 800mm
minimum load	250kg

electrical supply data

230 VAC 50 Hz	0.5A
115 VAC 60 Hz	1.0A

5V camera trigger

output level high	>2.5V
output level low	<0.5V

Highspeed camera is an optional equipment and can be ordered separately.

Photron High Speed Camera data specification



Photron

FASTCAM	MINI AX200 540K	NOVA S6 800K	NOVA S9 900K	NOVA S12 1000K
CMOS Image Sensor	1024 x 1024	1024 x 1024	1024 x 1024	1024 x 1024 px
max. fps full resolution	6400	6400	9000	12800 fps
max. Frame Rate	540000	800000	900000	1000000 fps
Light Sensitivity	40000	64000	64000	64000 ISO
L x W x H	94 x 120 x 120	217.2 x 120 x 120	217.2 x 120 x 120	217.2 x 120 x 120 mm
weight	1.5	3.3	3.3	3.3 kg

Vision Devices lighting data specification

LED VD7000	
operating voltage	24 - 36V
rated power	17 - 72W
Luminous flux	2100lm
Luminous flux boost	7280lm
color temperature	6000K
L x W x H	100 x 46 x 46 mm

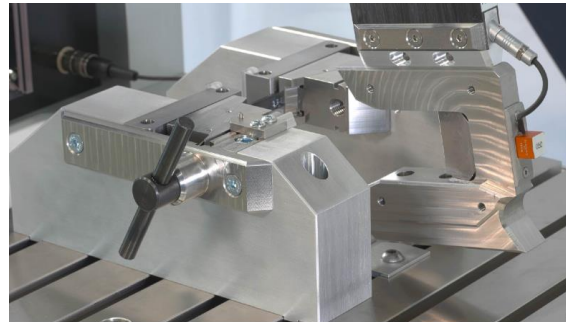


**VISION
DEVICES**

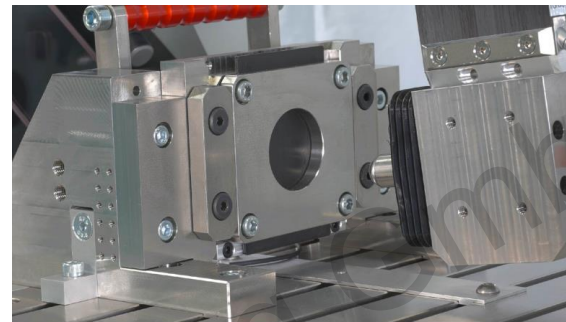
IMPETUS™ - configurations



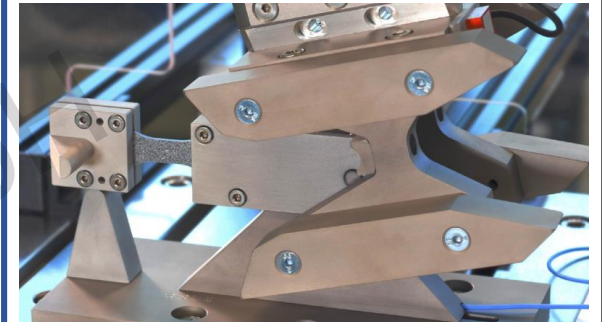
3 POINT BENDING



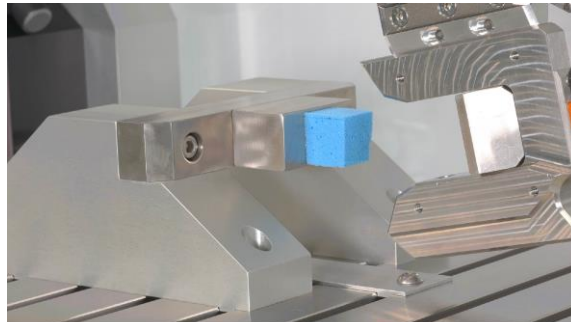
TENSION BENDING



PUNCTURE TEST



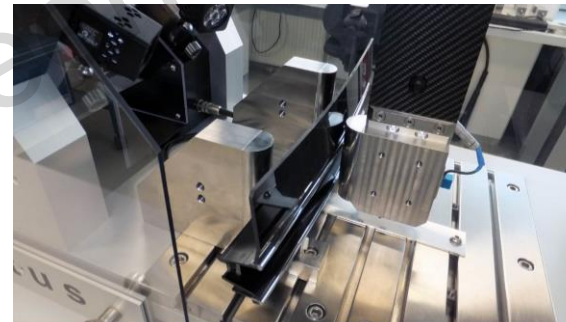
TENSION TEST



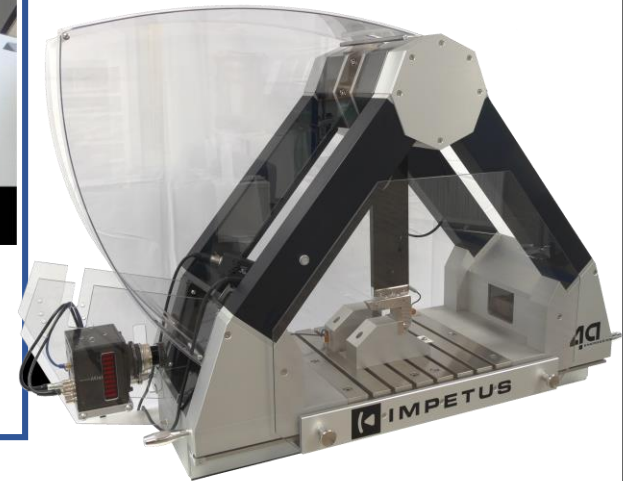
COMPRESSION TEST



SAMPLE MAGAZIN



COMPONENT TEST



BASIC

STANDARD

PROFESSIONAL

Efficient dynamic testing



Material (*Typical thickness*)

COMPRESSION TEST

3 POINT BENDING

TENSION BENDING

PUNCTURE TEST

TENSION TEST

Plastic (*1 - 4 mm*)



Foam (*20 - 30 mm*)



Composite (*1 - 4 mm*)



Aluminum (*1 - 2.5 mm*)



Metals (*0.5 - 1.5 mm*)



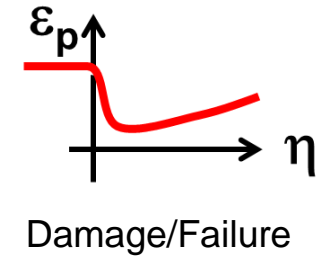
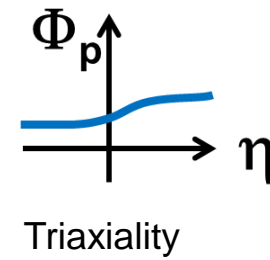
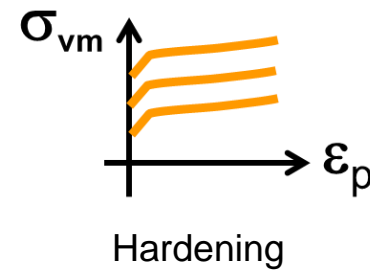
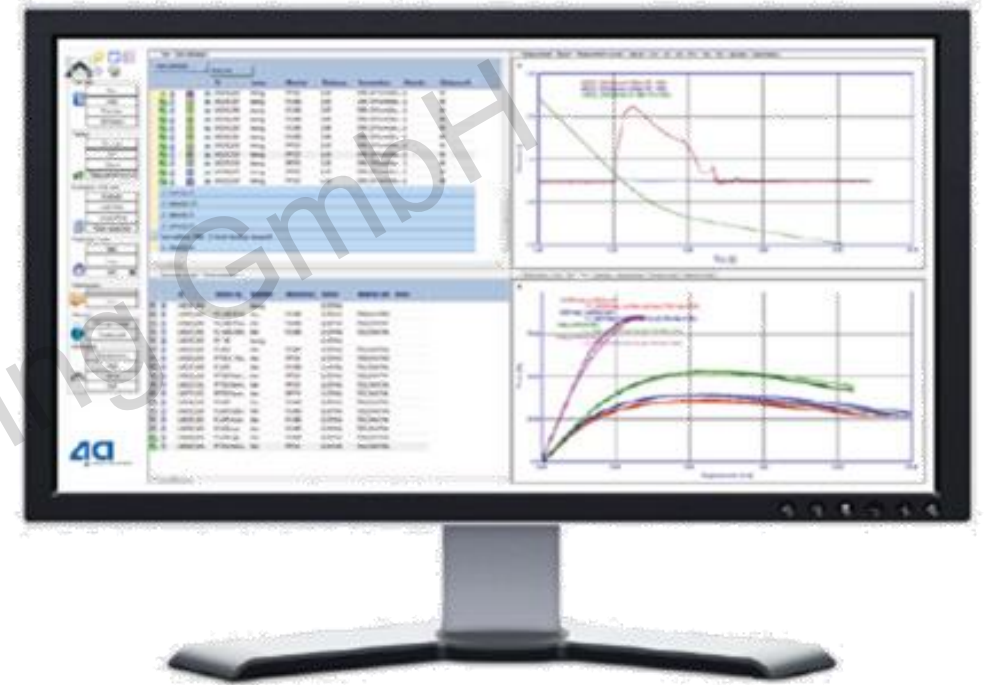
© at 4a engineering GmbH

From test to material card



VALIMAT

engineering plastics production
 concepts excellence in validation simulation
 lightweight prototypes



Anisotropic

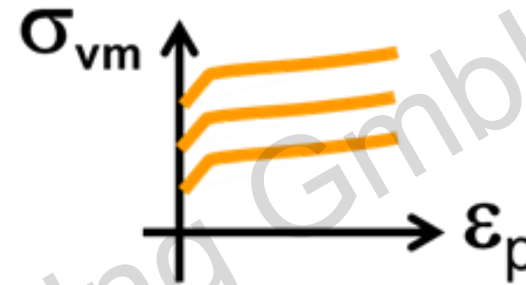
Material data generation for simulation

Current Situation

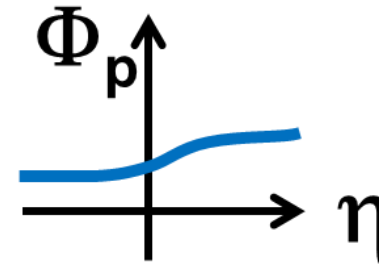
- more and more data
- Not only tension
 - Different loadcases (compression, shear,)
- More complex simulation models
Investigations on failure

NEEDED

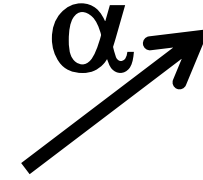
- Smart USER INTERFACE
- Optimization
- DATABASE handling data



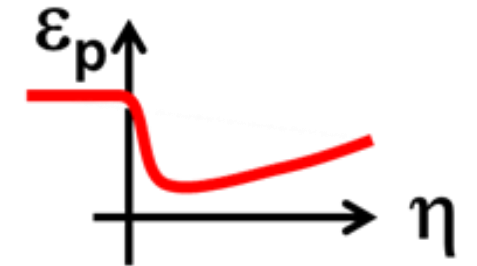
Hardening



Triaxiality



Anisotropic



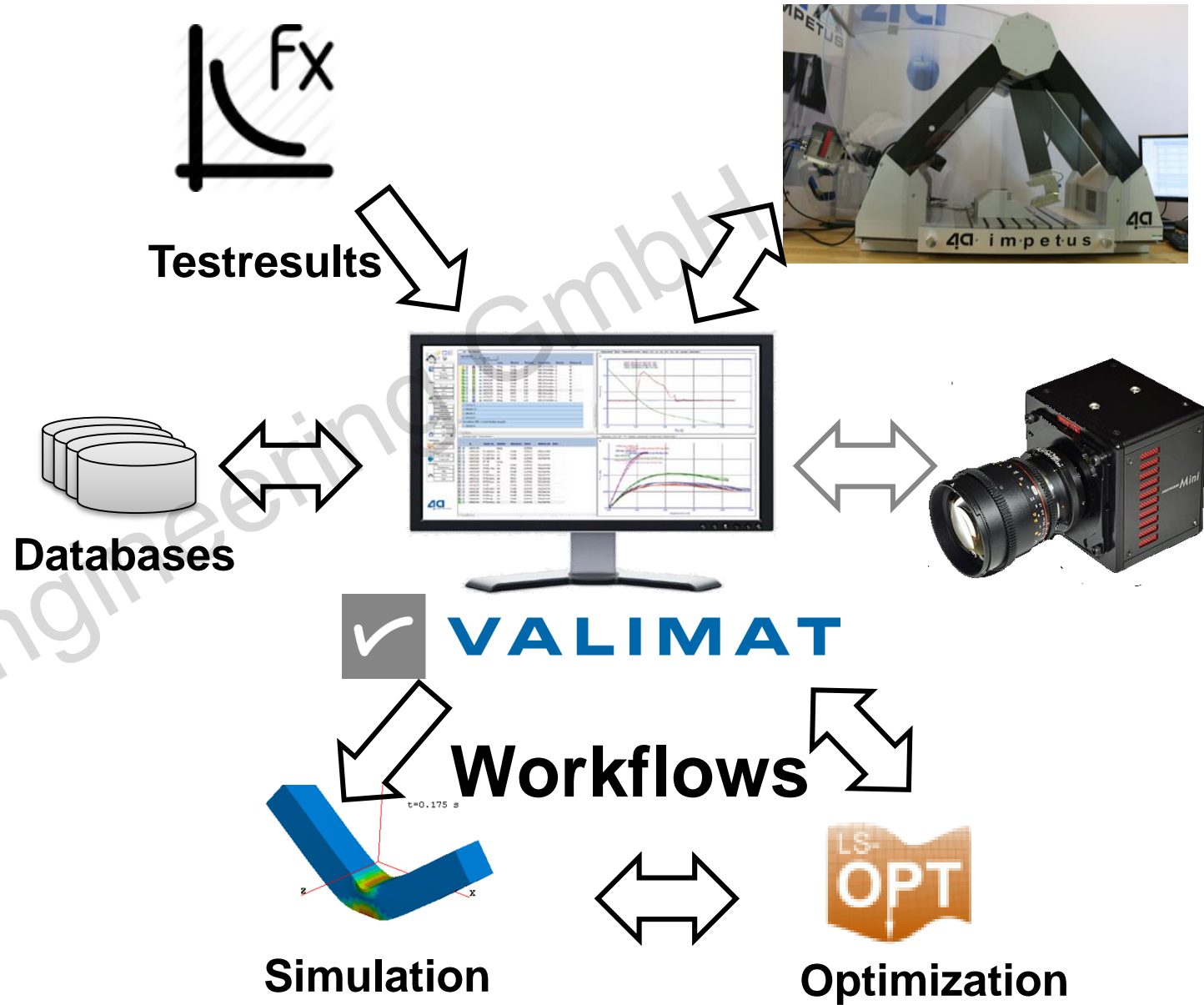
Damage/Failure

From test to material card

VALIMAT™

Advantage

- Handling of bigdata
- Complex models
- Good correlation to simulation



Efficient dynamic testing

3 POINT BENDING TENSION BENDING COMPRESSION PUNCTURE TENSION

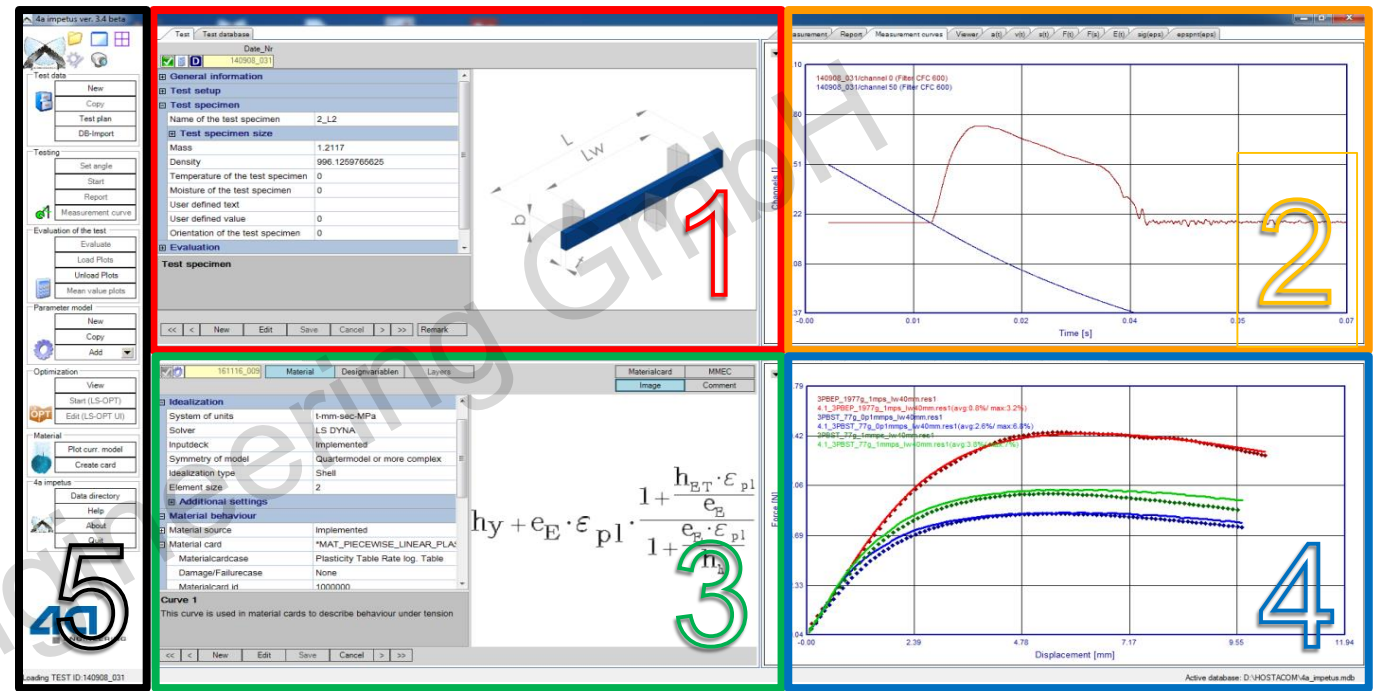
Plastic
Foam
Composite
Aluminum
Metals

typical thickness
(1 - 4 mm)
(20 - 40 mm)
(1 - 4 mm)
(1 - 2.5 mm)
(0.5 - 1.5 mm)

automated FE-model generation

VALIMAT

GUI - the graphic user interface is divided into five parts:



basic menu (left margin, (5))

window top left (1) → test; data base

window top right (2) → measurements; info; measurement results

window bottom left (3) → model parameter; optimization settings

window bottom right (4) → optimization; results of the optimization

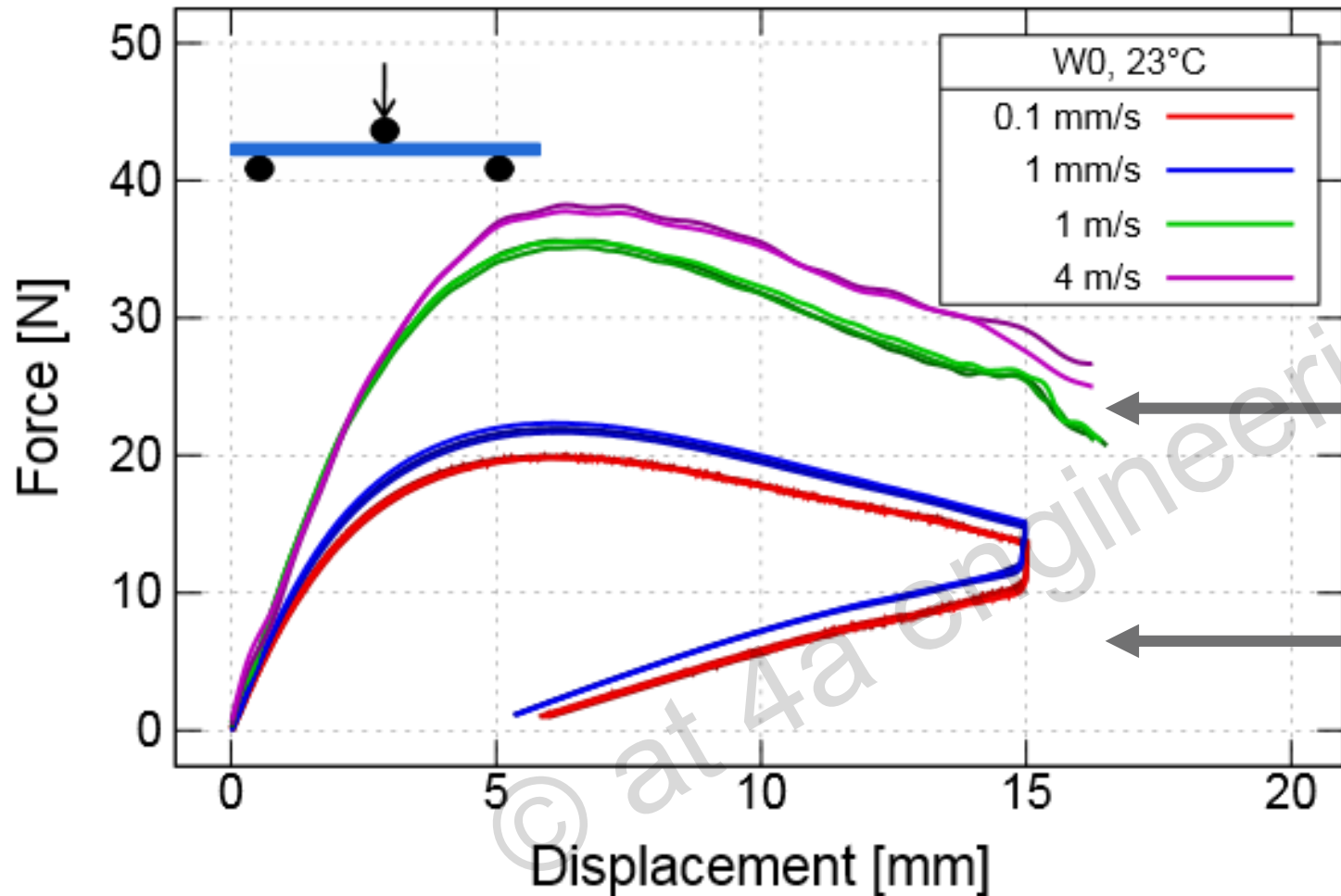
the basic menu describes the principal process from the test to the completed material model and allows a simple and fast access of the most important functions.

- Plenty of direct implemented **LS-Dyna** material models (*also Abaqus, PamCrash*)

Material card	
Materialcardcase	*MAT_ELASTIC (*MAT_001)
Damage/Failurecase	*MAT_PIECEWISE_LINEAR_PLASTICITY (*MAT_024)
Materialcard id	*MAT_PLASTICITY_COMPRESSION_TENSION (*MAT_124)
Density	*MAT_SAMP-1 (*MAT_187)
Plasticity	*MAT_FU_CHANG_FOAM (*MAT_083)
Function (Hardening, Elastic curve)	*MAT_COMPOSITE_DAMAGE (*MAT_022)
Strain rate dependency	*MAT_ENHANCED_COMPOSITE_DAMAGE (*MAT_054)
Micromec	*MAT_LAMINATED_COMPOSITE_FABRIC (*MAT_058)
Fracture	*MAT_RATE_SENSITIVE_COMPOSITE_FABRIC (*MAT_158)
Postfracture	*MAT_LAMINATED_FRACTURE_DAIMLER_PINHO (*MAT_261)
	*MAT_LAMINATED_FRACTURE_DAIMLER_CAMANHO (*MAT_262)
Loadcases	*MAT_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_157)
Results	*MAT_MICROMECC (*MAT_215)
	*MAT_MICROMECC (*MAT_215)+Carbon

- Whole number** of LS-Dyna material models is available through **userdefined material cards**

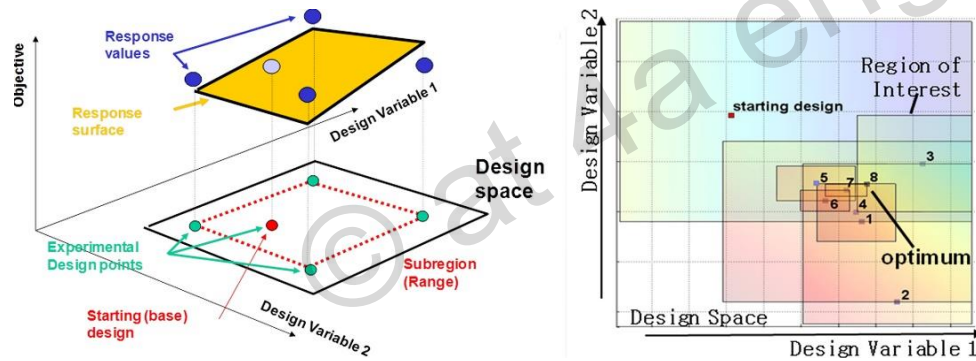
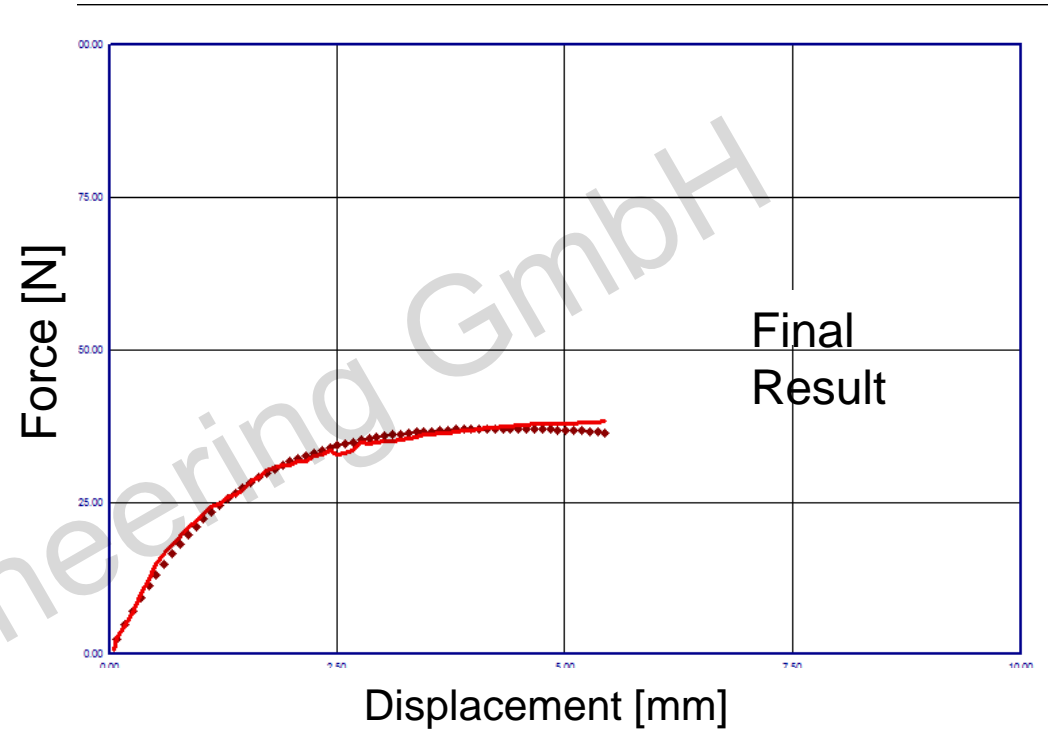
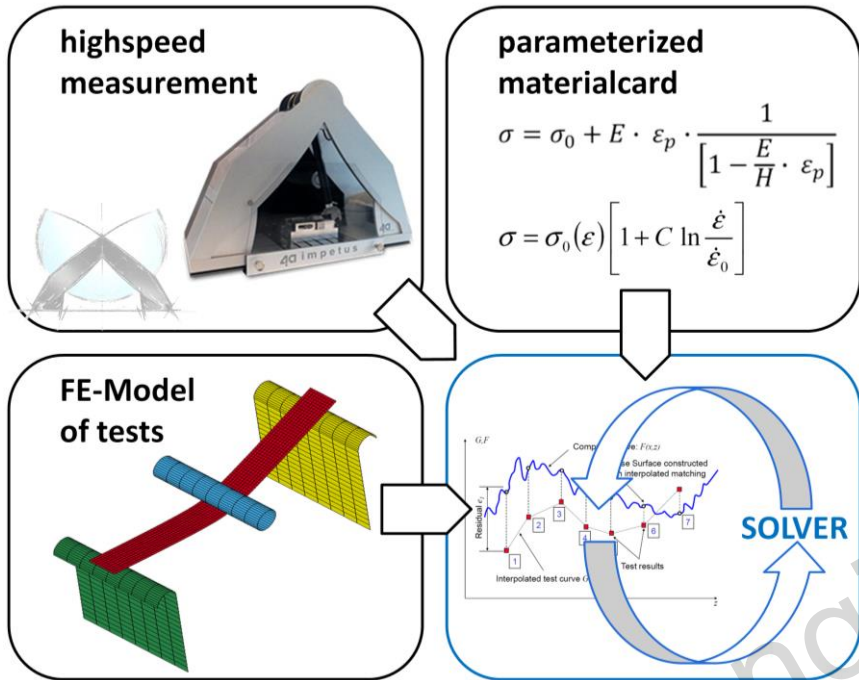
Efficient dynamic testing



IMPETUS

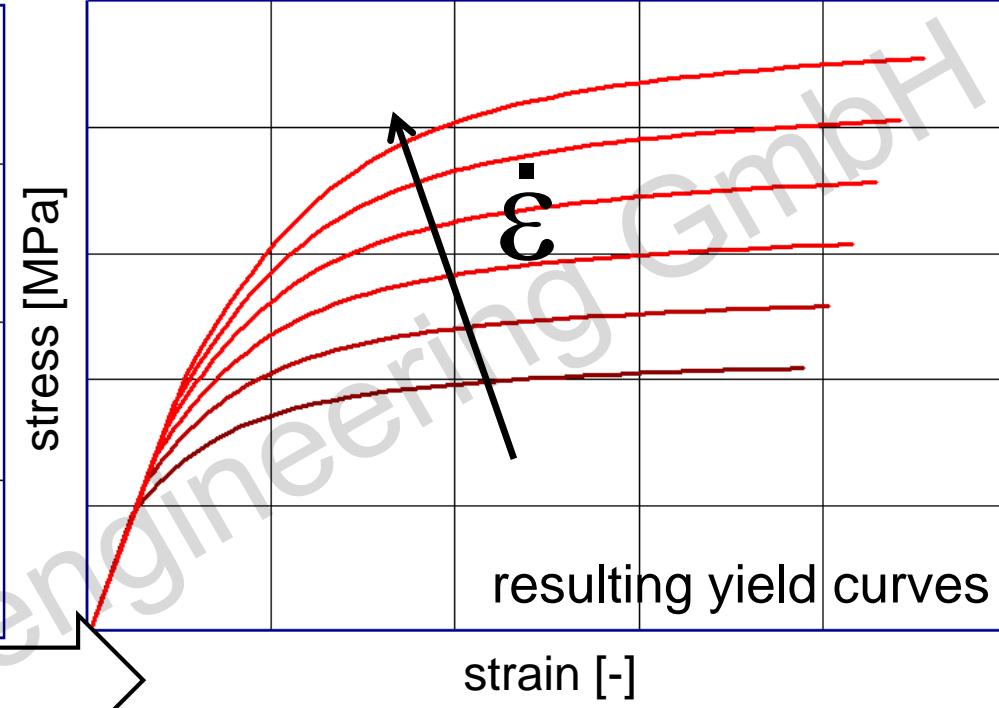
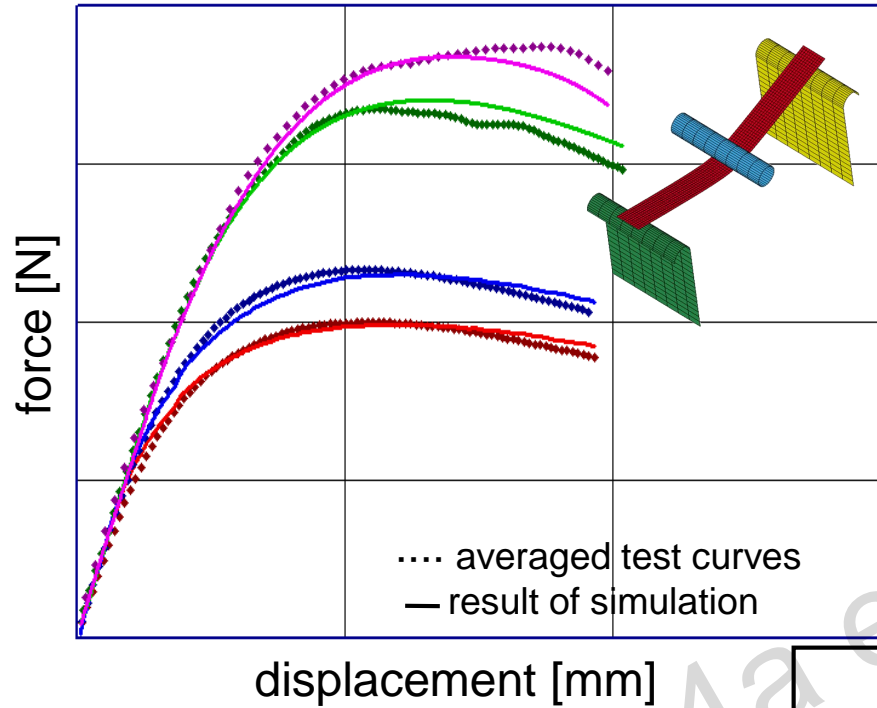
Universal static testing

Reverse engineering

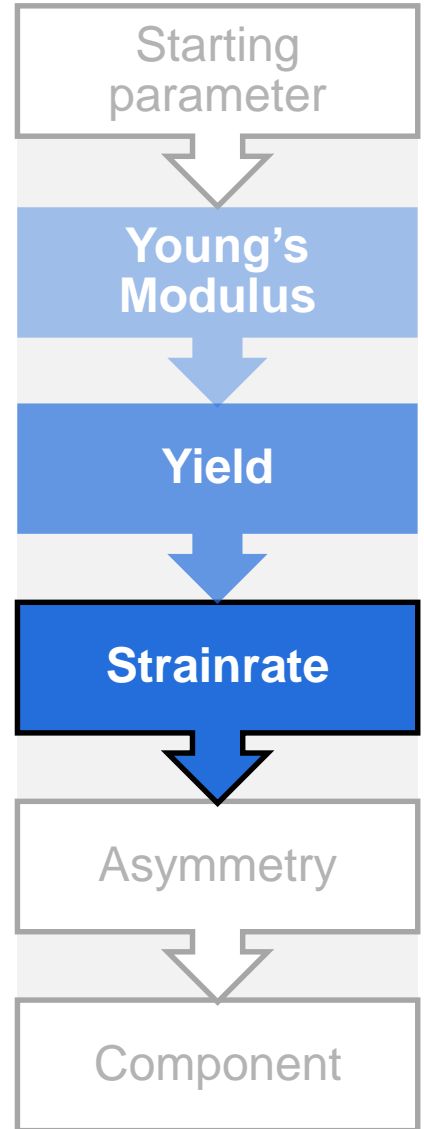
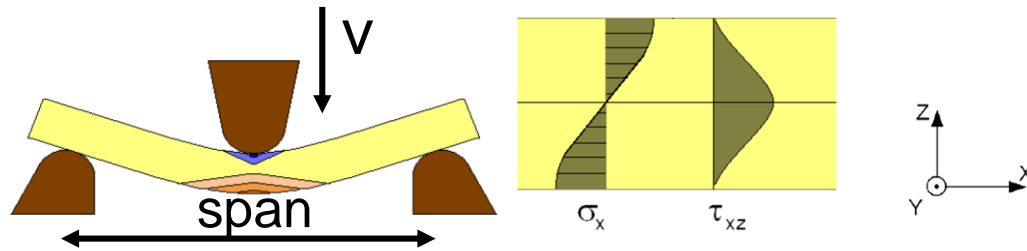


Source: Dynamic Material Characterization Using 4a impetus – PPS Conference 2015, Graz

From bending → *MAT_024



v [m/s]	span [mm]
0.0001	40
0.001	40
1	40
4	40



Intelligent reliable solutions for plastics, composites, metals, foams, ...

VALIMAT

- manage test results
(import, export, filter, evaluation)
- statistics
- automatic report
- material card generation
- material card validation

for all material types

from test to validated material cards

IMPETUS

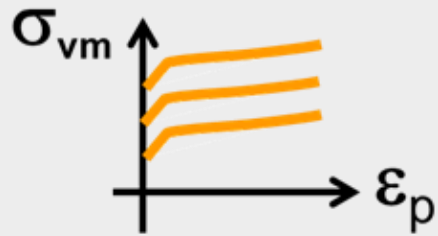
- single pendulum up to 4.5 m/s
- double pendulum up to 8 m/s
- standard test methods
- specialized test methods
- component testing
- advanced measurement

efficient dynamic testing

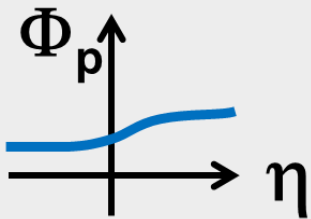
plastics and composites

Intelligent reliable solutions for plastics, composites, metals, foams, ...

✓ VALIMAT



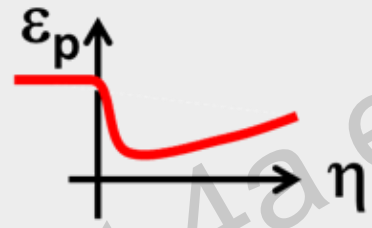
Hardening



Triaxiality



Anisotropic

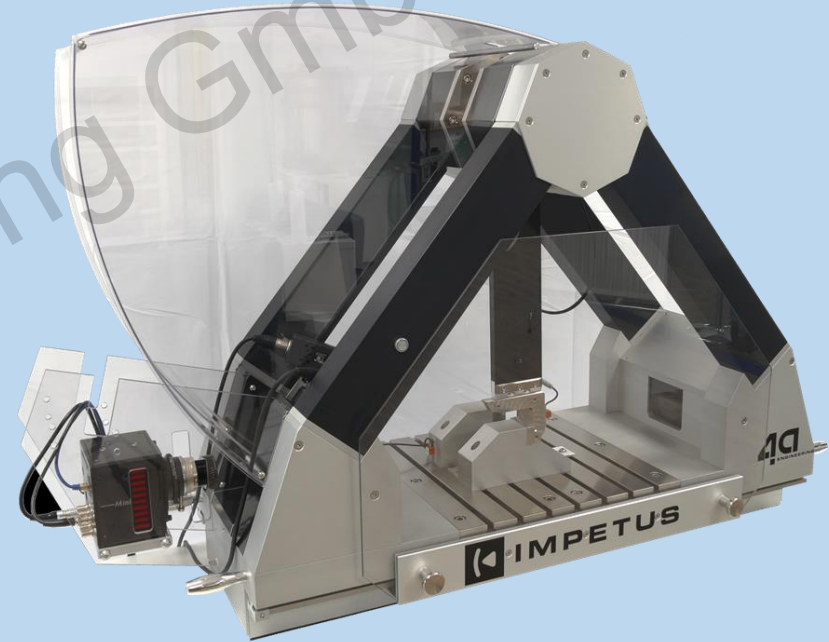


Damage/Failure

for all material types

from test to validated material cards

◀ IMPETUS



efficient dynamic testing

plastics and composites



IMPETUS

<http://impetus.4a.at>



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