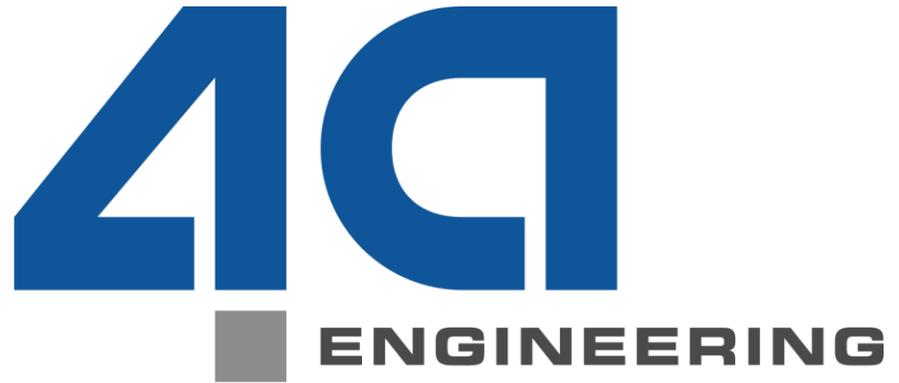


Thermo-mechanical characterization and modelling of battery cell components with IMPETUS® and VALIMAT®

13th European LS Dyna conference 6th October 2021

M. Schwab, H. Pothukuchi, B. Hirschmann, M. Rollant



excellence in ...
plastics simulation
testing equipment
lightweight products



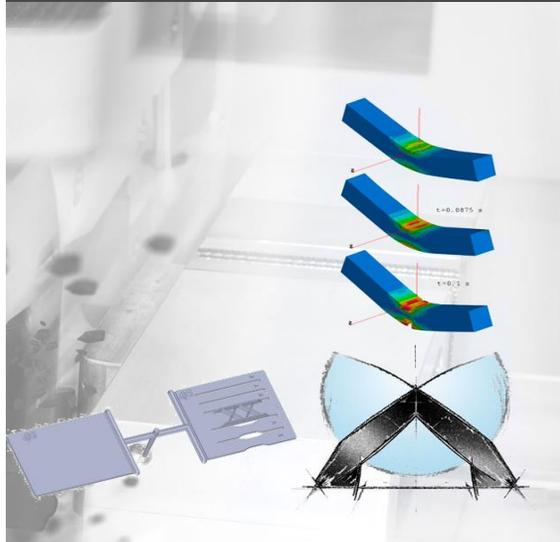
4a-engineering - Business Units

Testing hard- and software



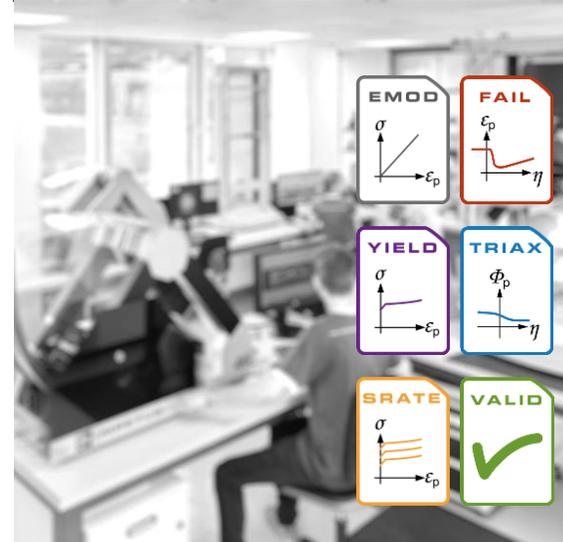
Seamless testing and simulation solution for automated material characterization

Material characterization



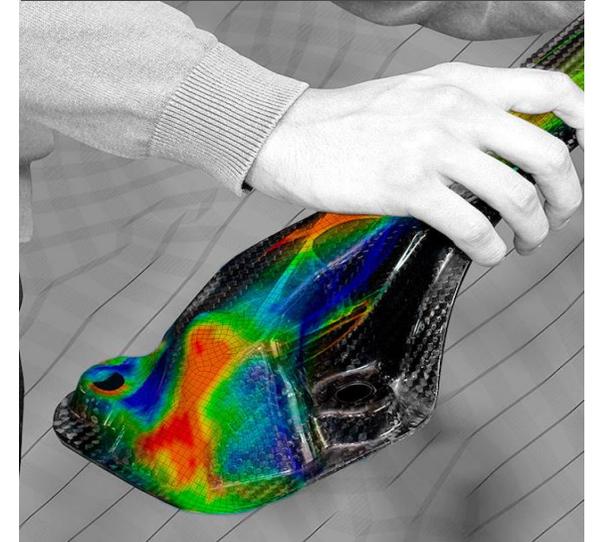
Static and dynamic material characterization from specimen to component validation – all under one roof

Validated material cards



Optimized packages for common material models for LS-Dyna, PamCrash and Abaqus.

Product development



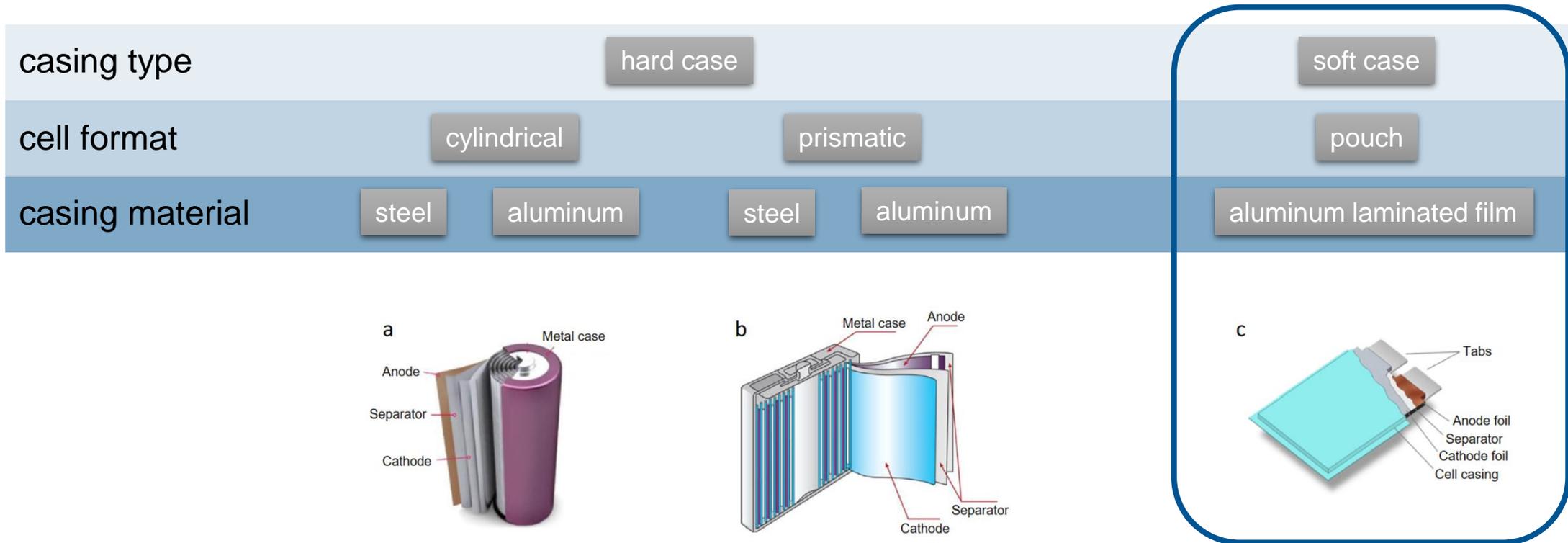
From draft to craft – Engineering, simulation and prototyping

Agenda

- Motivation
- Mechanical behaviour of pouch foils
- Modelling and validation in LS Dyna
- Application Example
- Summary

Motivation

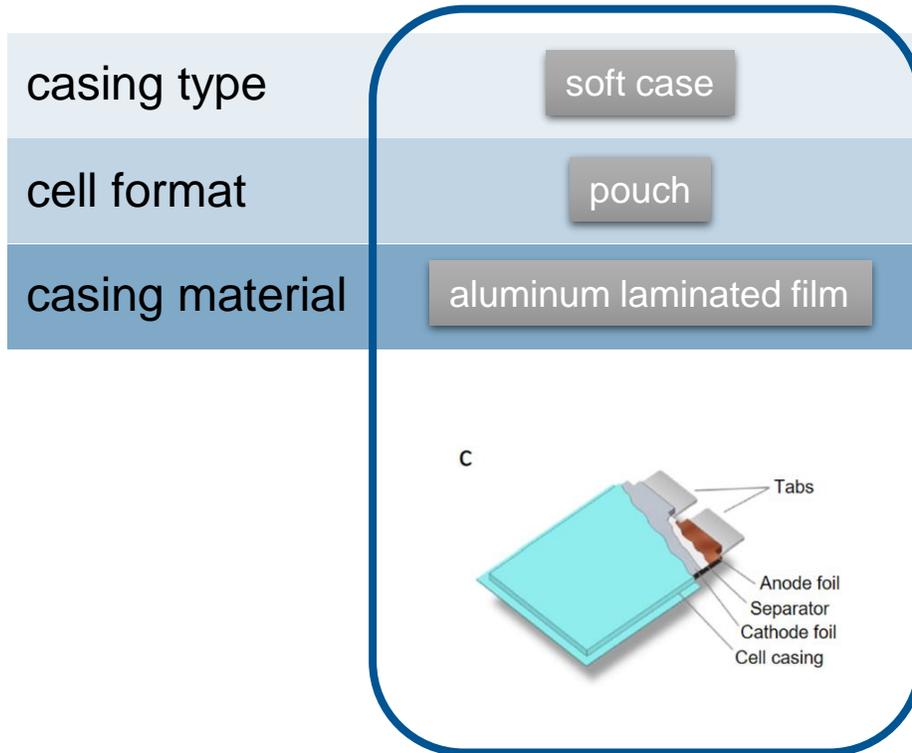
- different types of automotive Li-Ion battery cells:



Zubi, G.; Adhikari, R.S.; Sánchez, N.E.; Acuña-Bravo, W. Lithium-ion battery-packs for solar home systems: Layout, cost and implementation perspectives. J. Energy Storage 2020, 32, 101985

Motivation

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Zubi, G.; Adhikari, R.S.; Sánchez, N.E.; Acuña-Bravo, W. Lithium-ion battery-packs for solar home systems: Layout, cost and implementation perspectives. J. Energy Storage 2020, 32, 101985

- Cell consists of many layers of thin foils (current collector, separators) and granular active material
- all internal components are flooded by liquid electrolyte, which ensures ion transport capability
- Cell casing: pouch foil (aluminum laminated film)
 - environmental protection (moisture, handling, ...)
 - tightness
 - keep internal components in place
 - prone to mechanical loads

Motivation

Typical loads acting on pouch foil:

- external loads (e.g. shock, vibration, crash) introduced through:
 - cell fixation (e.g. bottom or circumferential)
 - terminal area
 - penetration
- internal loads:
 - gas generation
 - swelling
 - thermal runaway



Motivation

Typical loads acting on pouch foil:

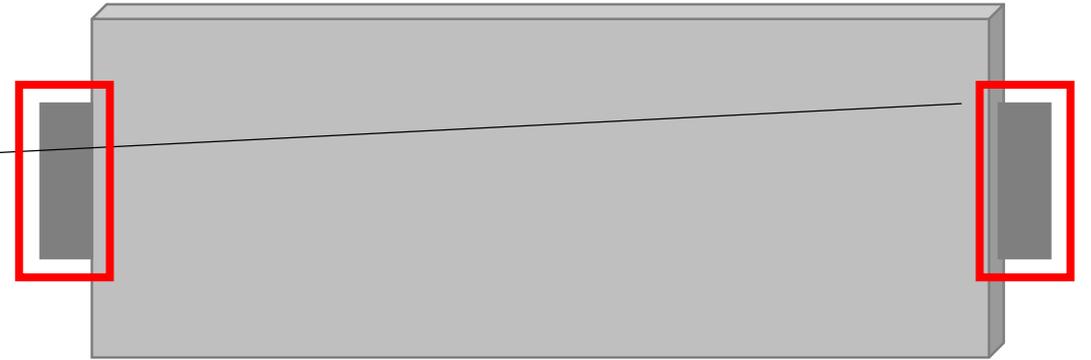
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Motivation

Typical loads acting on pouch foil:

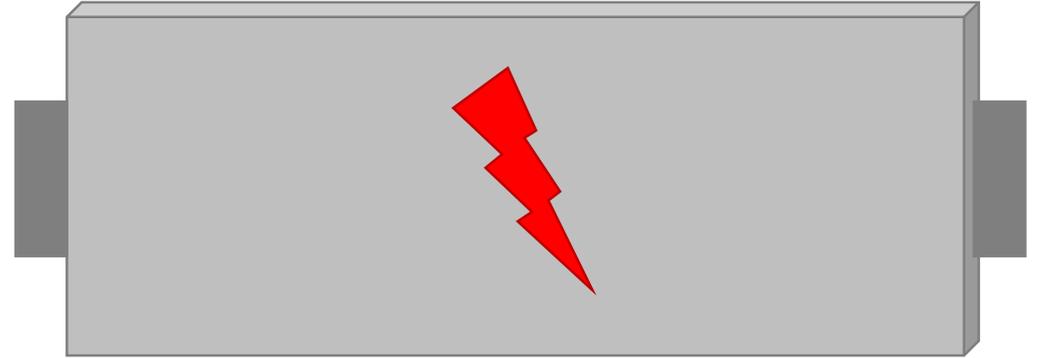
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Motivation

Typical loads acting on pouch foil:

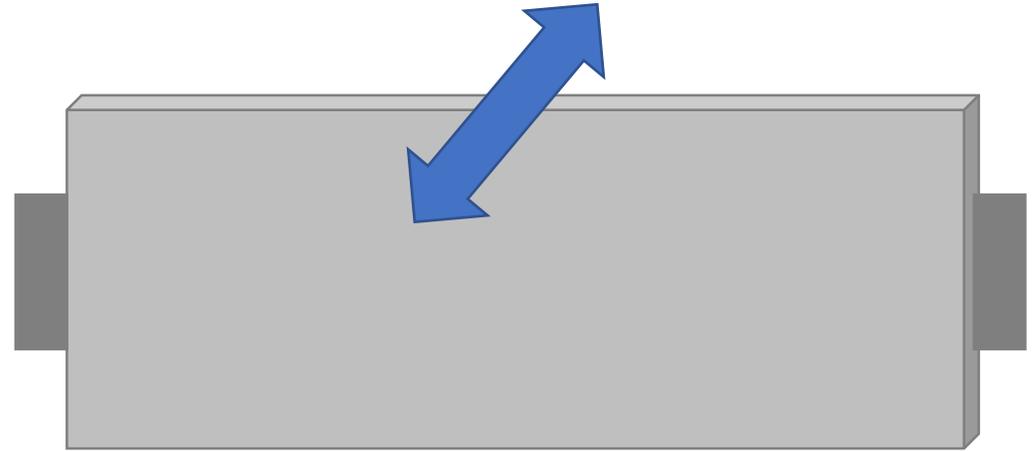
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Motivation

Typical loads acting on pouch foil:

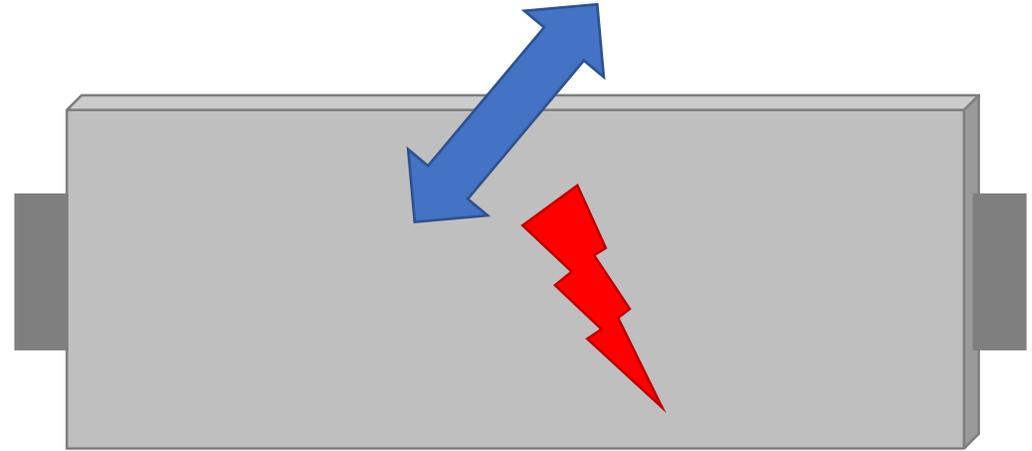
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Motivation

Typical loads acting on pouch foil:

- external loads (e.g. shock, vibration, crash) introduced through:
 - cell fixation (e.g. bottom or circumferential)
 - terminal area
 - penetration
- internal loads:
 - gas generation
 - swelling
 - **thermal runaway**



Motivation

- rupture of pouch foil leads to elektrolyte leakage → loss of electrical function
- various external loads are transmitted through the pouch foil
- internal loads are directly acting on pouch foil

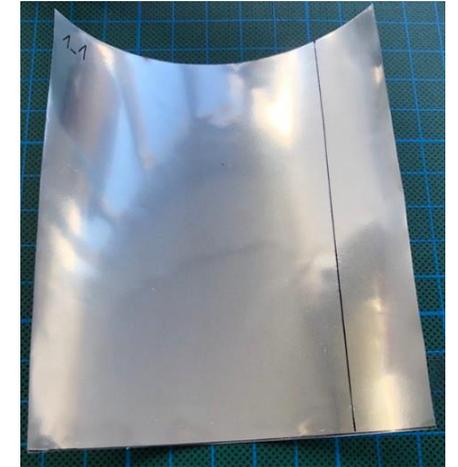
- FEM model of cell should represent casing and jelly separately
- need of accurate material models of pouch foils

Mechanical characterization

Pouch foil constitution

- Composite of thin foils glued together

PA6
Al
PP

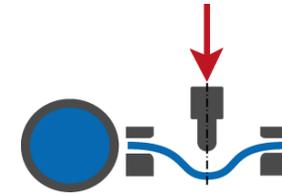


Layer material	thickness		Area weight g/m ²
	M	SD	
Polyamide (JIS Z1714)	0.025	0.0025	-
Adhesive (Polyester-polyurethane)	-	-	4-5
Aluminium foil (JIS A8021)	0.04	0.004	-
Adhesive (Urethane-free Adhesive)	-	-	2-3
Polypropylene	0.04	0.004	-
Total	0.111	0.011	



Mechanical characterization

Material Testing Setups

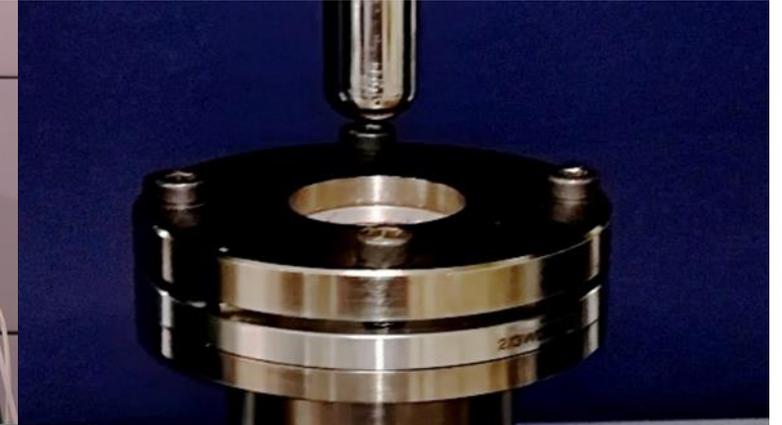


SHIMADZU AG-X

Quasistatic Test



TENSION TEST



PUNCTURE TEST

IMPETUS

Dynamic Tests



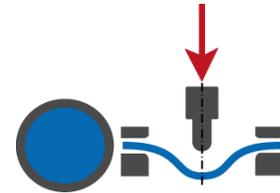
TENSION TEST



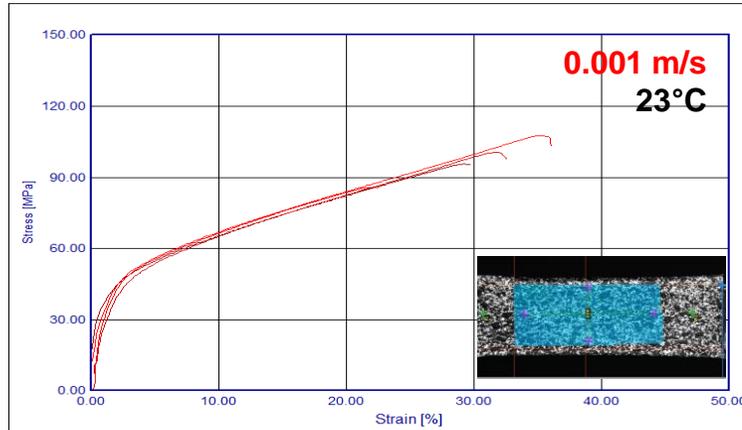
PUNCTURE TEST

Mechanical characterization

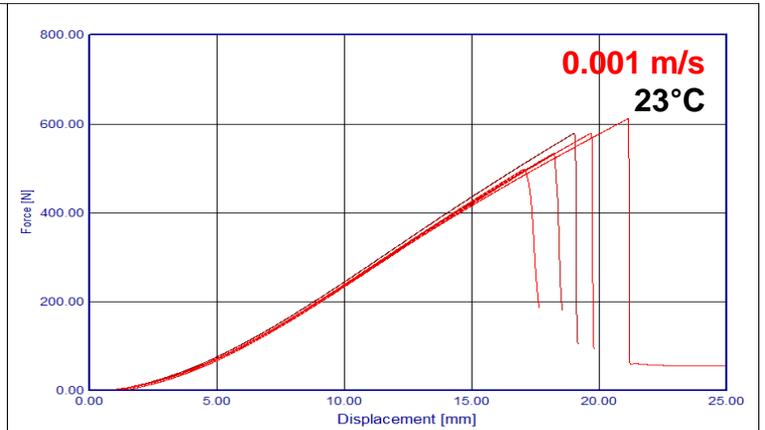
Material Measurement Results at 23°C



SHIMADZU AG-X Quasistatic Test

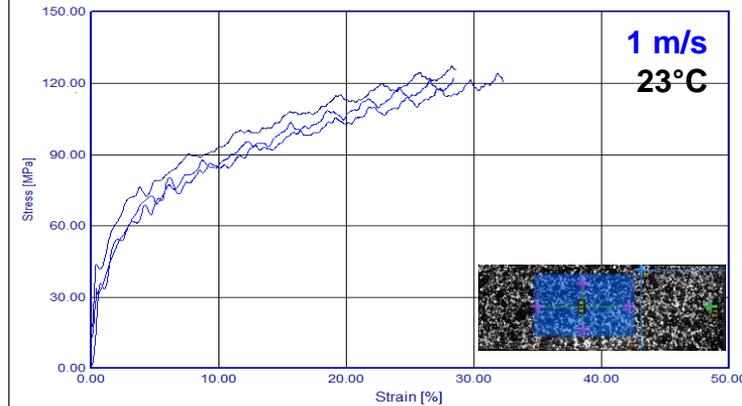


TENSION TEST

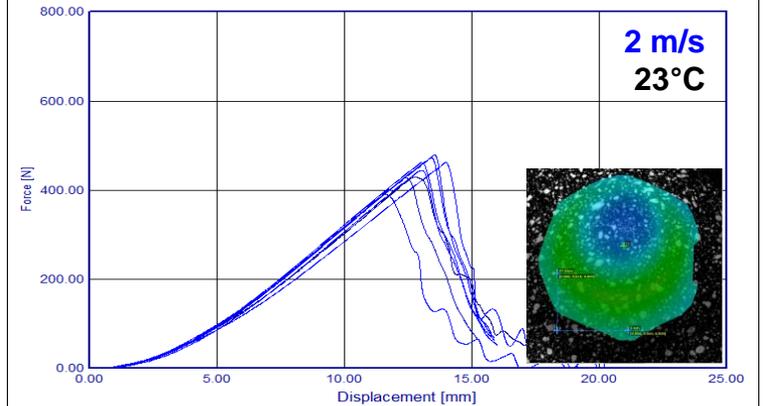


PUNCTURE TEST

IMPETUS Dynamic Tests



TENSION TEST

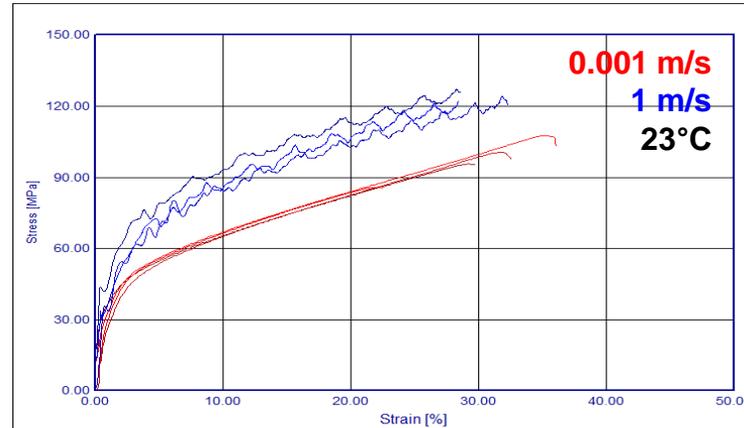
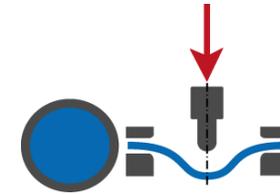


PUNCTURE TEST

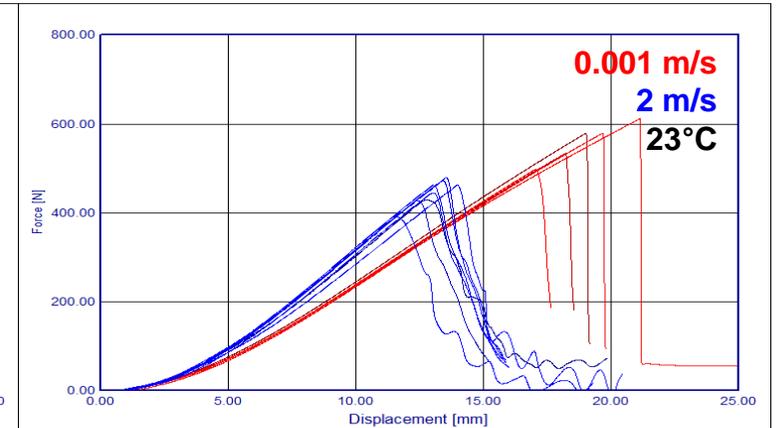
Mechanical characterization

Material Testing Setups

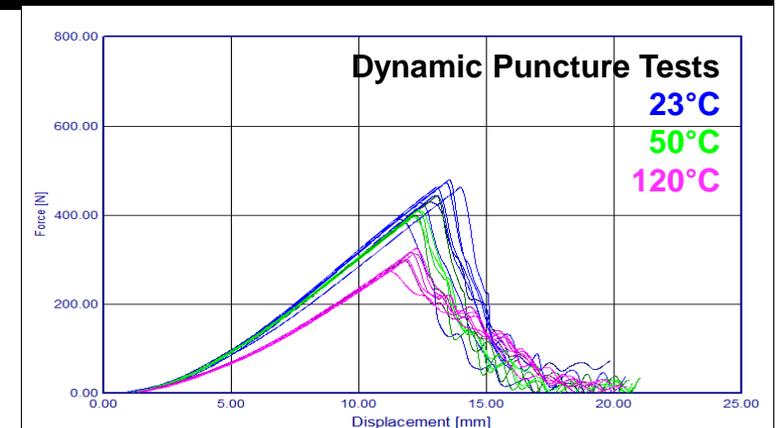
- higher velocity $v \uparrow$:
 - Force $\rightarrow \sigma_y \uparrow$
 - failure strains $\epsilon_f \downarrow$
- Higher Temperature $T \uparrow$:
 - Force $\rightarrow \sigma_y \downarrow$
 - failure strains $\epsilon_f \downarrow$



TENSION TEST



PUNCTURE TEST



PUNCTURE TEST

— measurement curves

Mechanical characterization

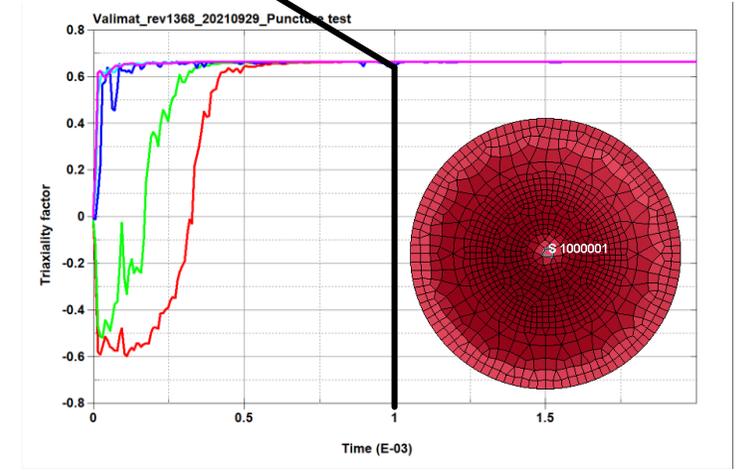
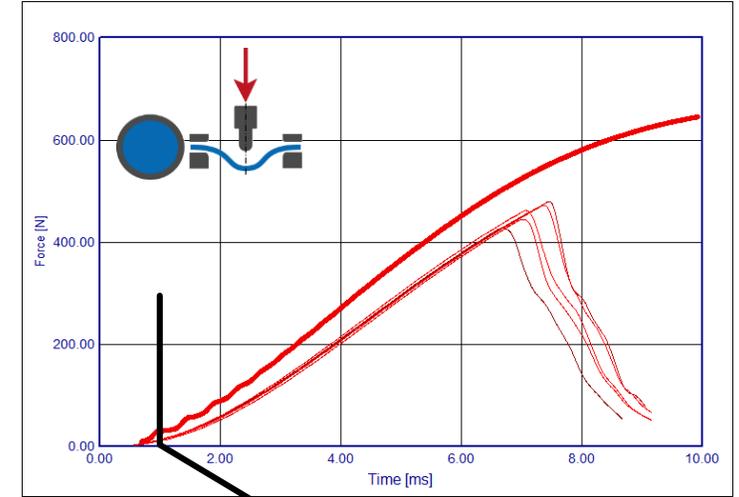
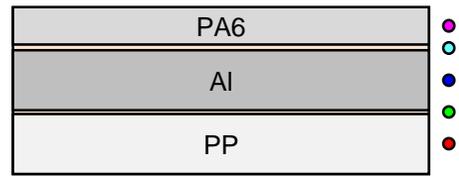
Modelling approach

Initial Idea: ***PART_COMPOSITE:**

- E.g. ***MAT_187L** — PA6
- E.g. ***MAT_024** — Al
- E.g. ***MAT_187L** — PP

- Can we use a simplification? ✔
 - Basic ***MAT_024** for each layer → ***PART_COMPOSITE**
 - SHELL ELFORM=16, 5IP
 - stress state homogeneous right after beginning
 - foil thickness small

→ **Membrane Elements**
 → **Homogenized Material**



— measurement curves — simulation curves

Mechanical characterization

Modelling approach

Homogenized Approach:

- One material model ***MAT_?** which can depict tests

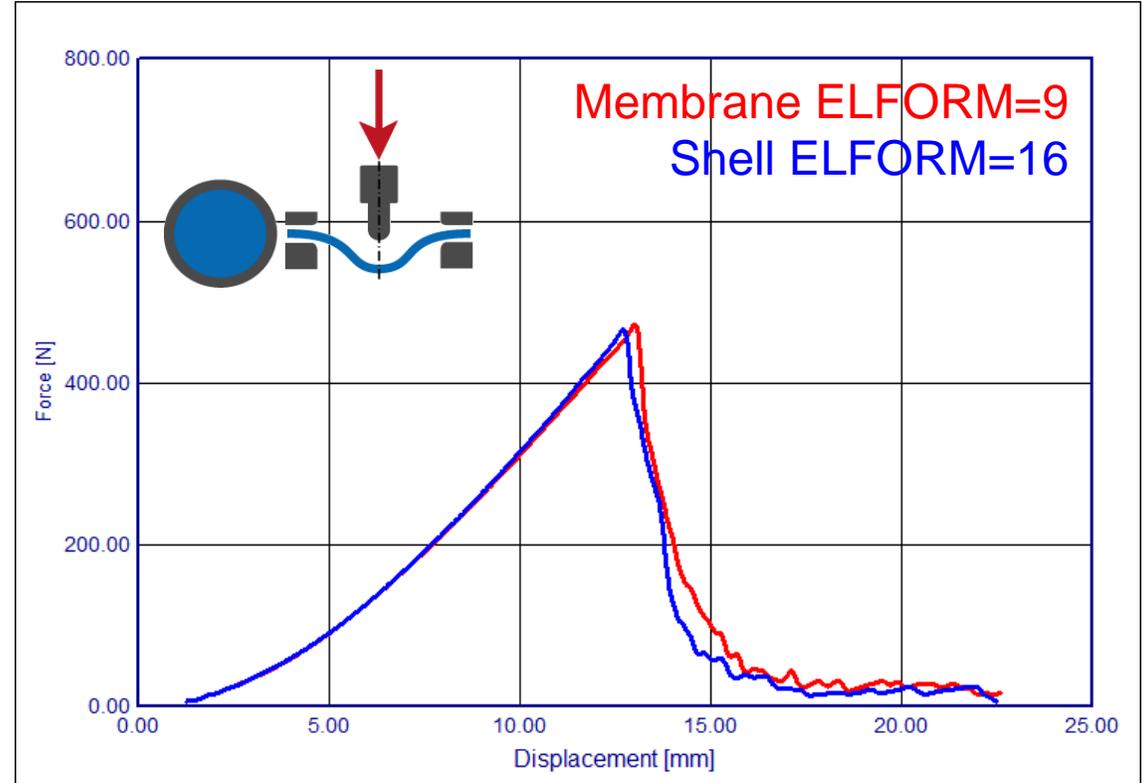
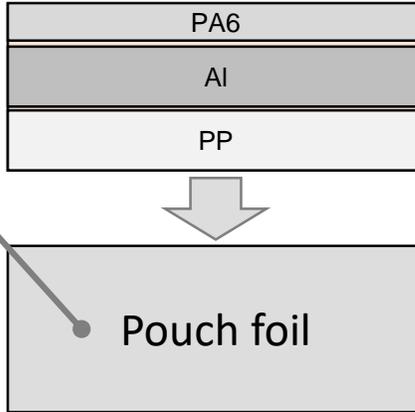
Material Tests showed:

- Temperature dependency: σ_y, ϵ_f
- strain rate dependency: σ_y, ϵ_f

→ ***MAT_106**

→ ***MAT_ADD_DAMAGE_GISSMO**
(**LCSDG** → **TABLE_3D**; temp, strain rate, triax.)

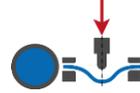
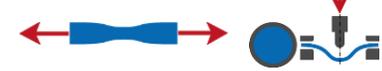
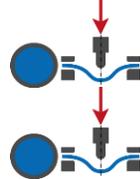
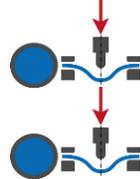
(can't describe load type dependency of the polymers)



— simulation curves

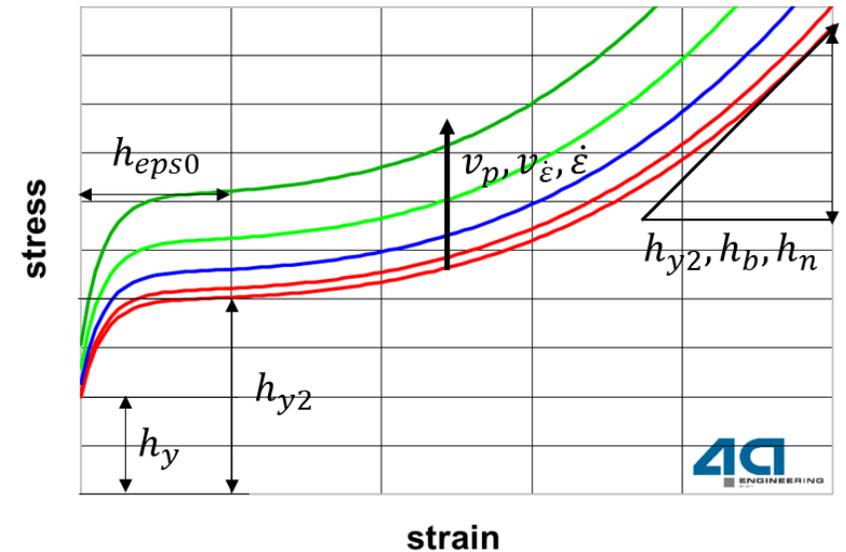
Mechanical characterization

Fitting approach

- Elasticity (mixture formula) (**R**everse **E**ngineering **RE**) 
- Hardening at 23°C (**RE**) 
- Viscoplasticity at 23°C (**RE**) 
- 3D-DIC → Friction Coefficient Settings 
- Failure at 23°C (**RE**) 
- Hardening Scaling Factor 50°C and 120°C (**RE**) 
- Failure Scaling Factor 50°C and 120°C (**RE**) 

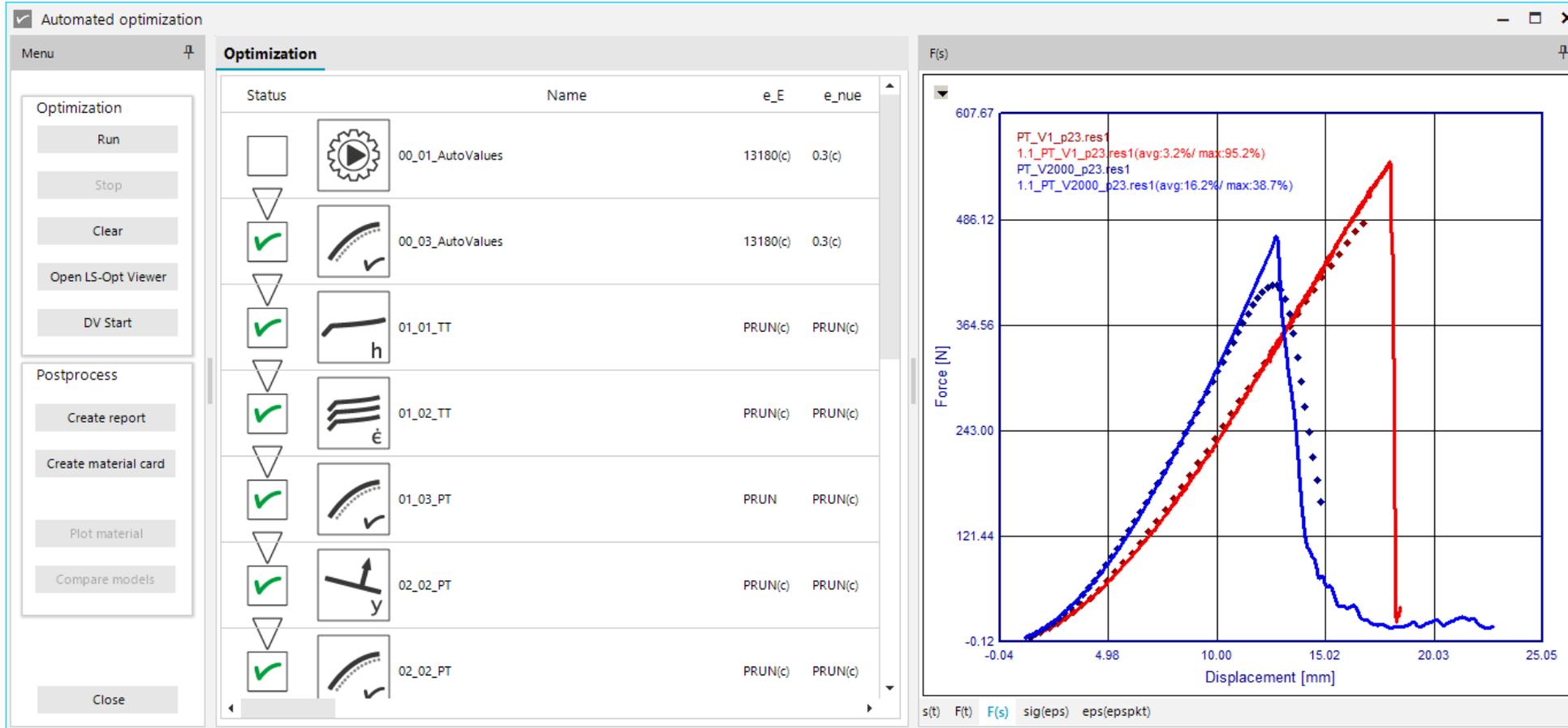
$$\sigma_{y,0} = (1 - h_b \cdot \varepsilon_{pl}^{h_n}) \cdot \left(h_{y2} - (h_{y2} - h_y) \cdot e^{-\frac{\varepsilon_{pl}}{h_{eps0}}} \right)$$

$$\sigma_y = \sigma_{y,0} \cdot \left(1 + \frac{1}{v_p} \cdot \log \left(\frac{\max(\dot{\varepsilon}_{pl}, v_{\dot{\varepsilon}})}{v_{\dot{\varepsilon}}} \right) \right)$$



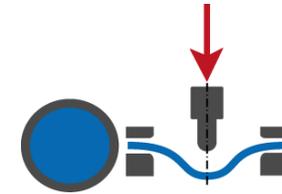
Mechanical characterization

Fitting approach – VALIMAT (AutoFit)



Mechanical characterization

Local Evaluation PT – 3D DIC



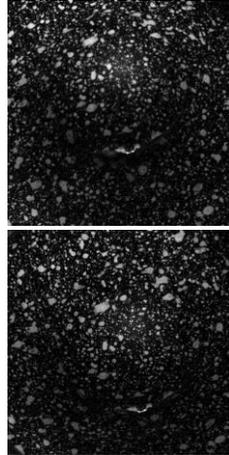
measurement

Photron



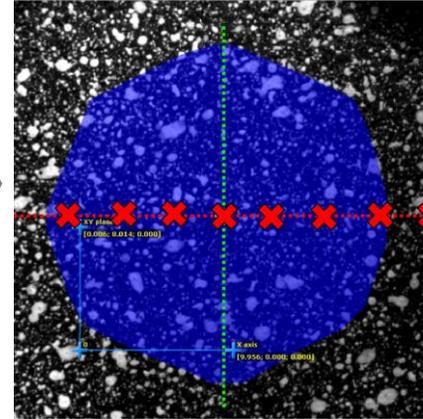
cam0

cam1



&

MERCURY[®] RT



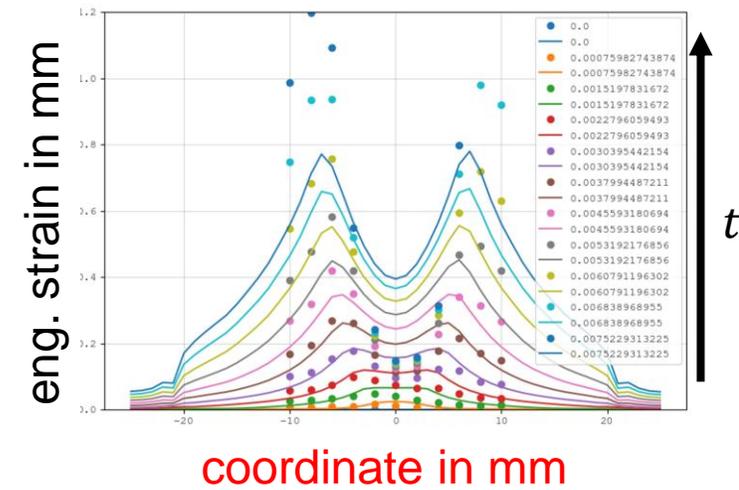
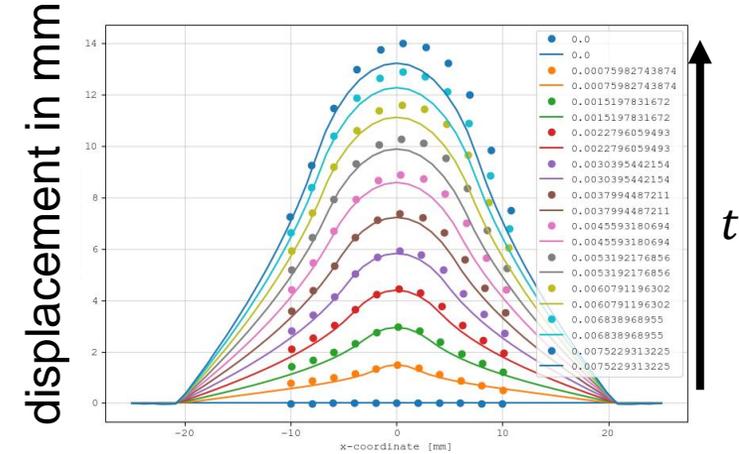
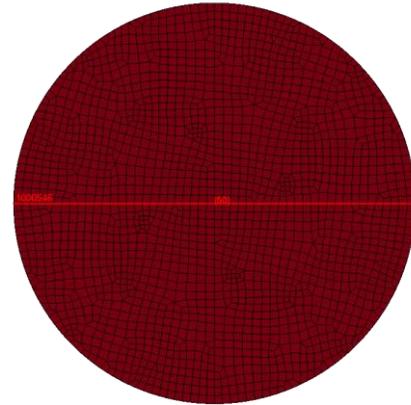
points



lines

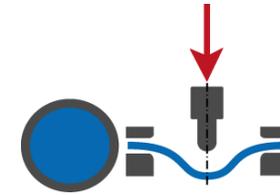
simulation

FEM
Nodal displacements
Over time
for all nodes in box



Mechanical characterization

Local Comparison PT – 3D DIC vs. *MAT_024 (homogenized)



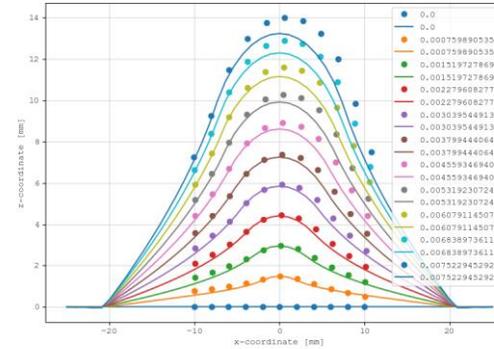
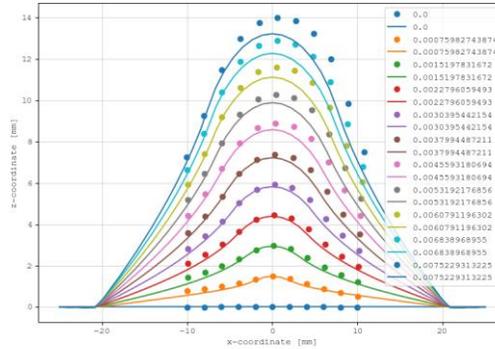
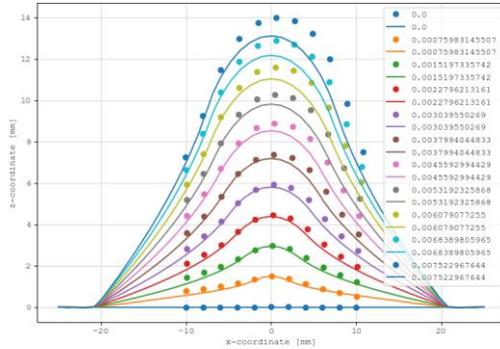
- Friction coefficient influences local strains → failure strains

Friction coeff. 0.1

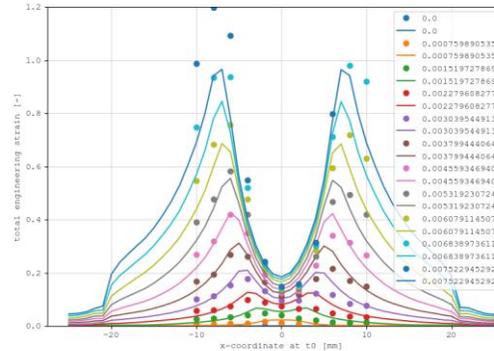
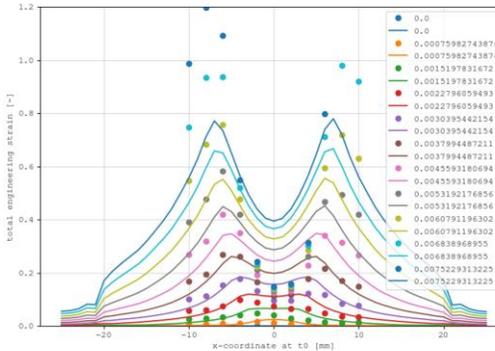
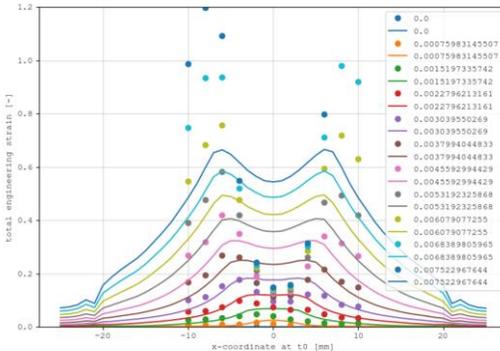
Friction coeff. 0.3

Friction coeff. 1.0

local z-disp



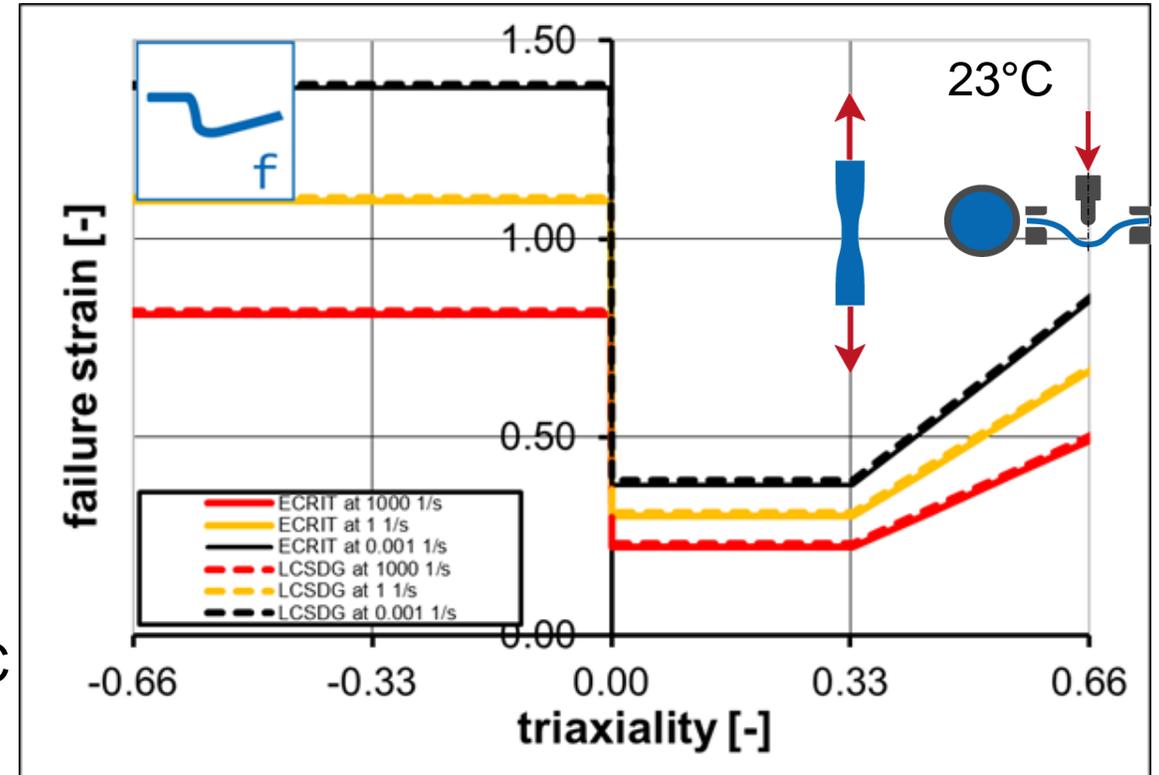
local eng. strains



Mechanical characterization

failure modelling

- Failure occurs abruptly
- Measurements 2 load types:
 - Tensile test (triaxiality $\sim 1/3$)
 - Puncture test (triaxiality $\sim 2/3$)
- Fitted the failure strains for 23°C
→ `*MAT_ADD_DAMAGE_GISSMO`
 - Tensile Test at 23°C strain rate dependent
 - Puncture Test 23°C
 - Scaled Failure strains to Puncture tests at 50°C and 120°C



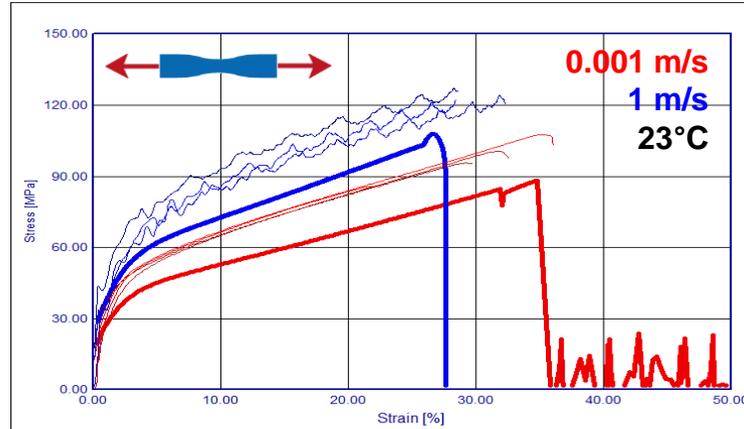
LCSDG: Failure strain curve/table or function

ECRIT: Critical plastic strain (material instability)

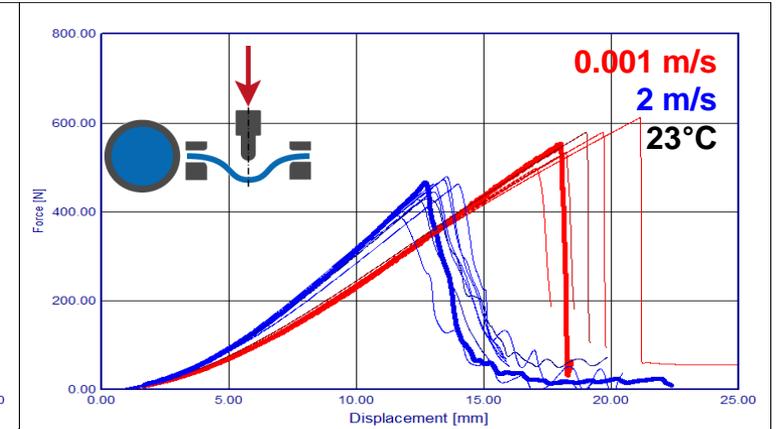
Mechanical characterization

Calibrated Material Model

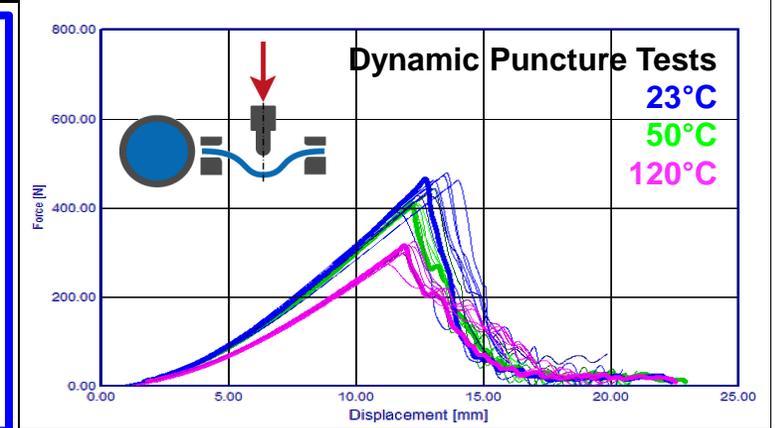
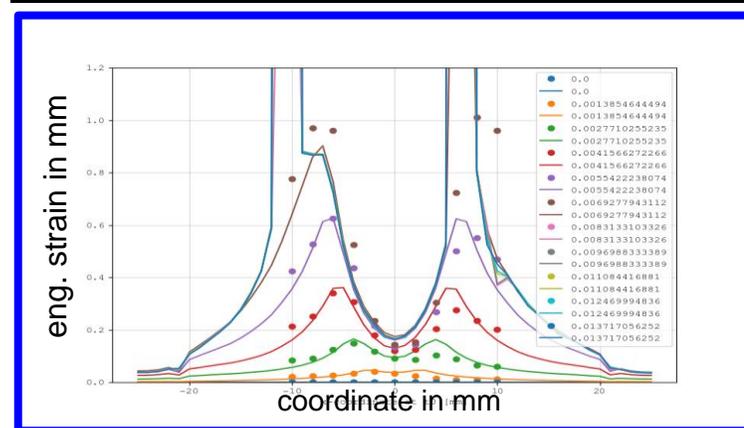
- Load type dependency:
 - *MAT_106 (simple Mises)
 - *MAT_255 (just UT → UC, no further reduction BT)
- Membrane Idealization → BT more important



TENSION TEST



PUNCTURE TEST



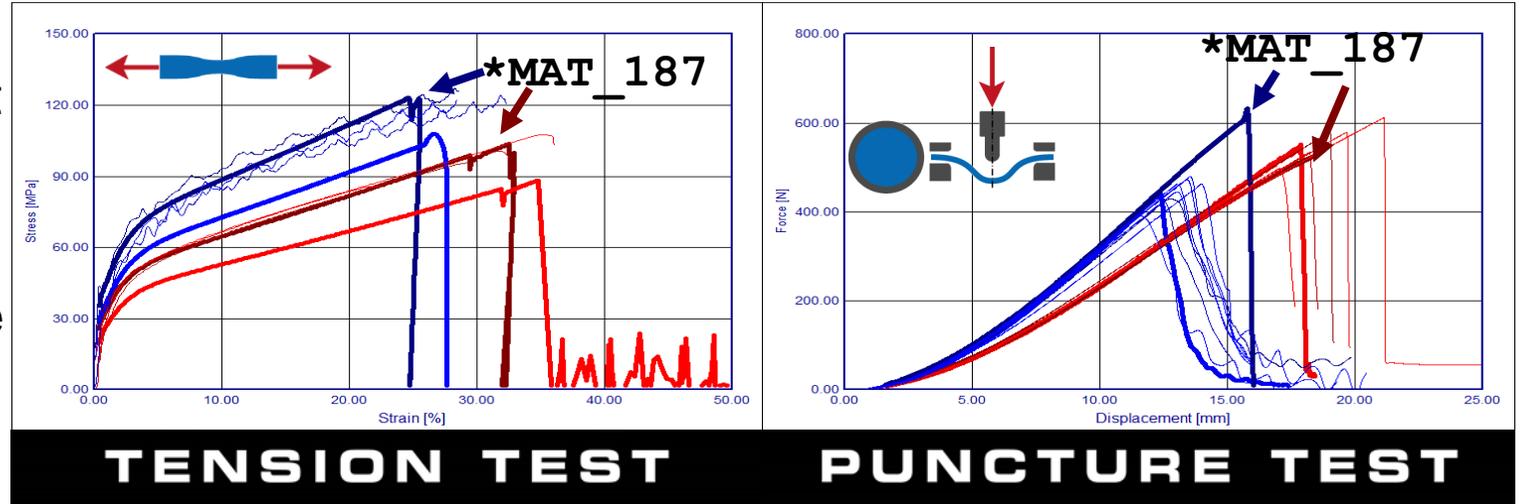
PUNCTURE TEST

— measurement curves — simulation curves

Mechanical characterization

yield surface *MAT_024 vs *MAT_187

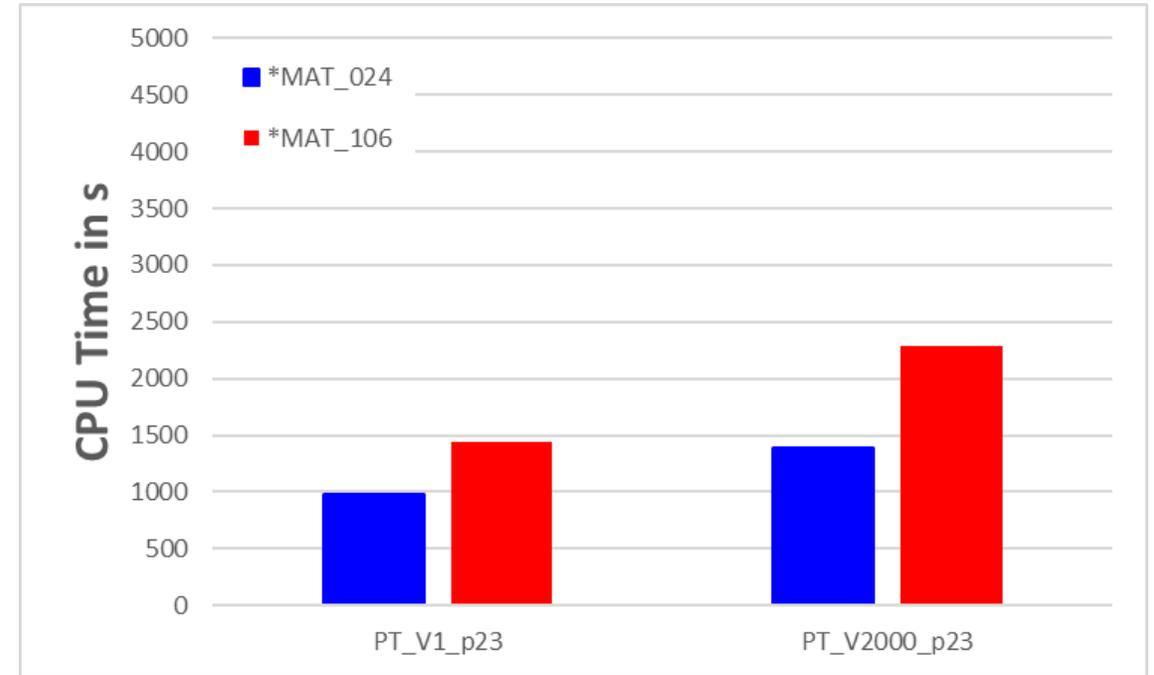
- With a different shape of the yield surface (*MAT_187) the tensile test and the puncture test can be depicted.
- The failure strains would have to be adjusted for this material mode.
- With this formulation we lose the temperature dependency.



Mechanical characterization

computational efficiency (`*MAT_024`/`*MAT_106` + `*MAT_ADD_DAMAGE_GISSMO`)

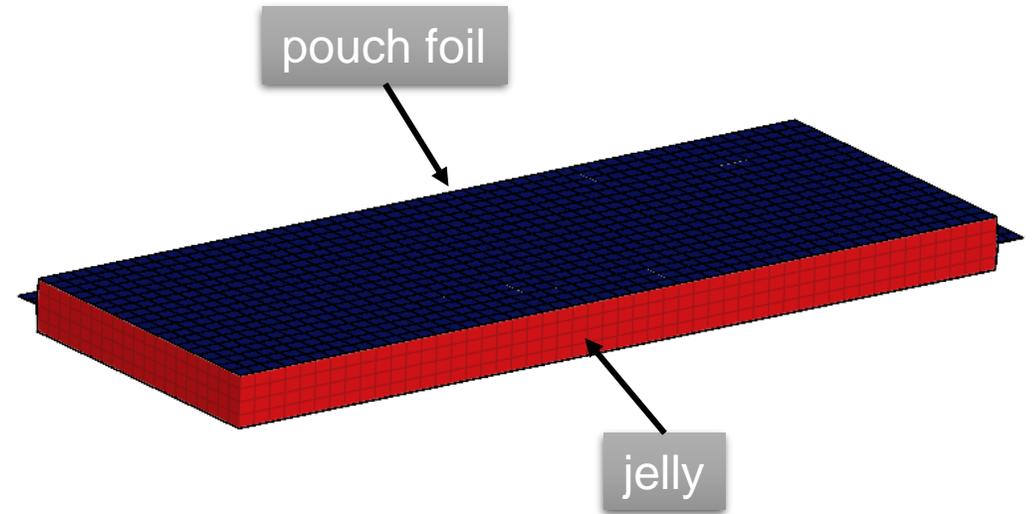
- Only slight computational time increase
- No thermal Solver just:
`*LOAD_THERMAL_LOAD_CURVE`



Demonstrator model: pouch cell

`*MAT_106 + *MAT_ADD_DAMAGE_GISSMO`

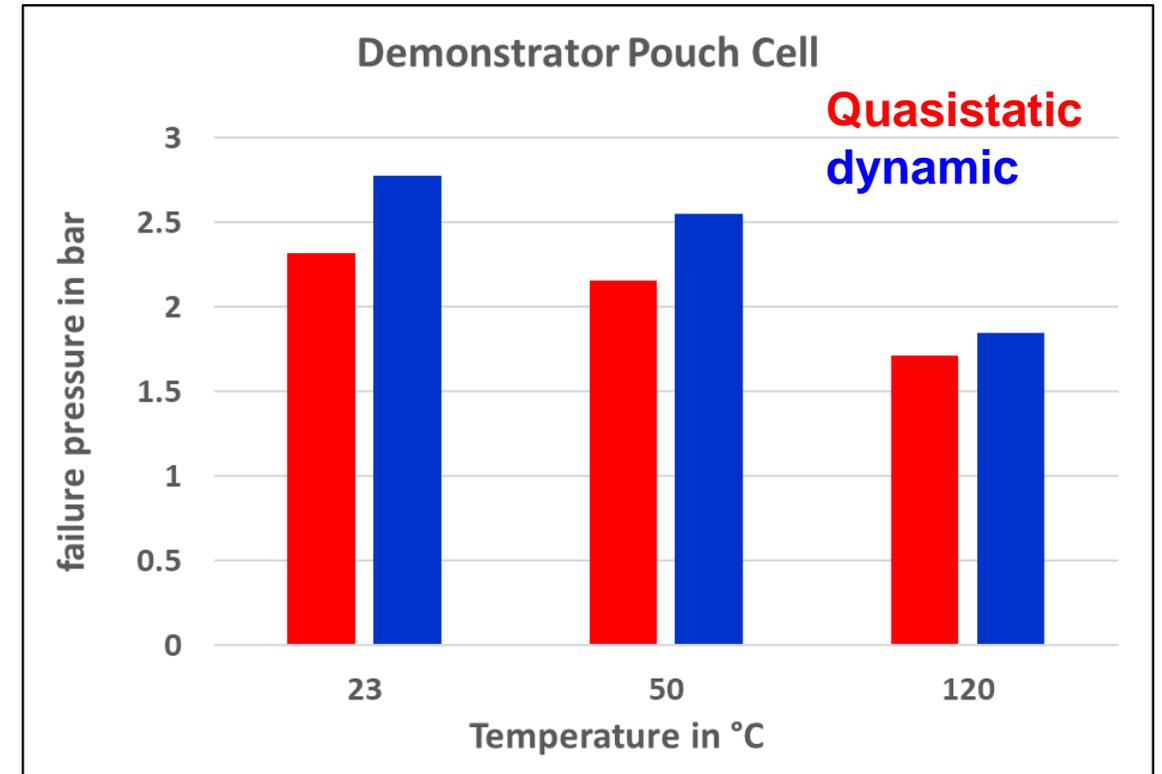
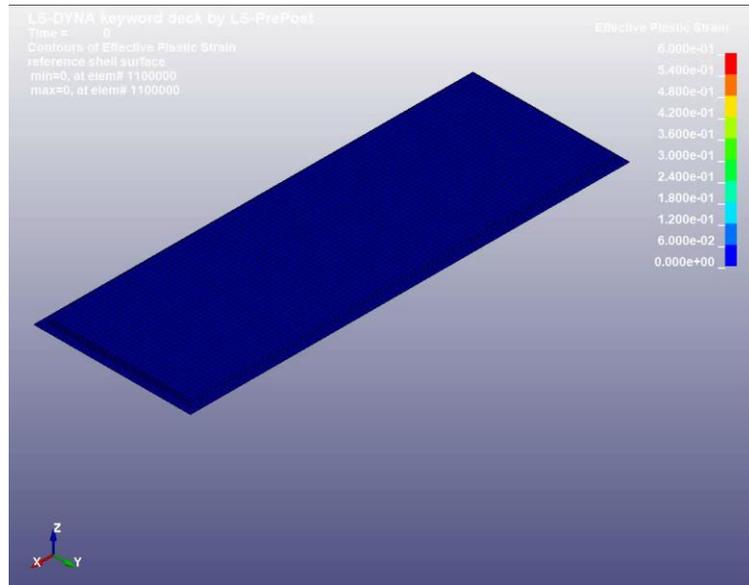
- Test of calibrated material model in demonstrator model:
 - simplified model of pouch cell
 - pouch: **8976** Membrane Elements (ELFORM=9)
 - jelly: solid elements
 - cell surface not constrained
 - simulation of internal pressure due to gas generation (`*LOAD_SEGMENT`)
 - variation of gas generation rate
 - variation of temperature (`*LOAD_THERMAL_LOAD_CURVE`)
 - prediction of leakage pressure level



Demonstrator model: pouch cell

*MAT_106 + *MAT_ADD_DAMAGE_GISSMO

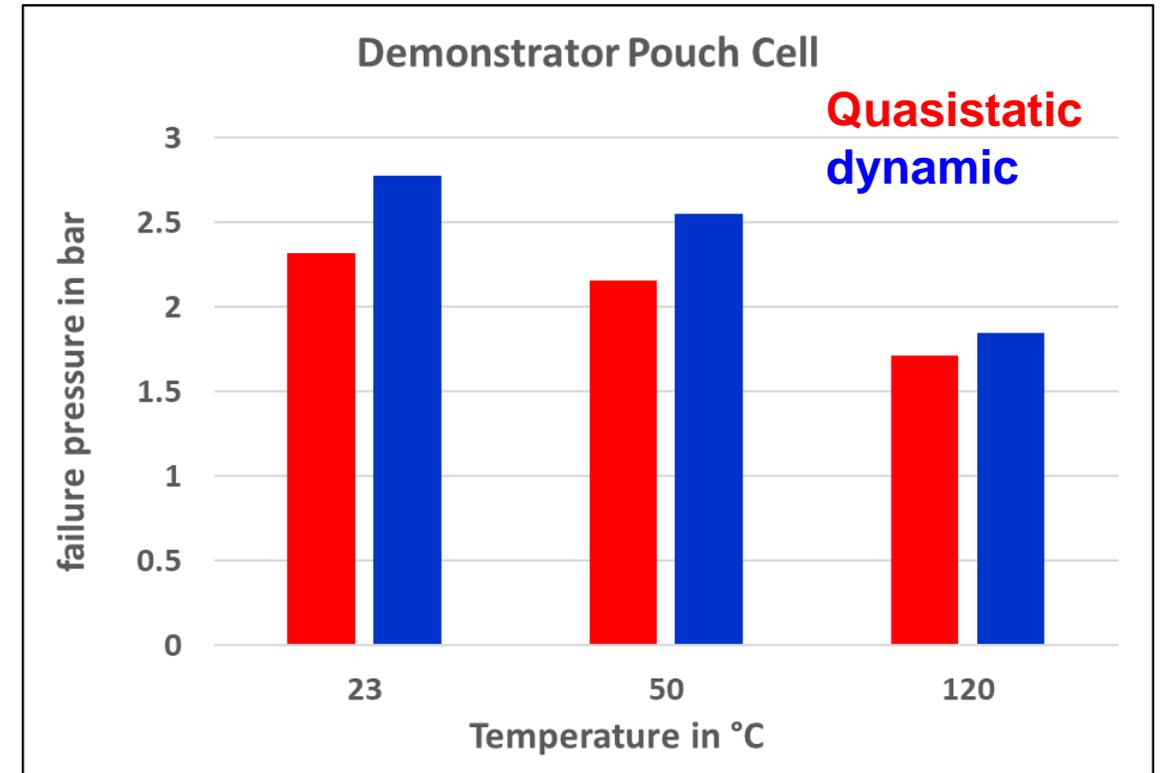
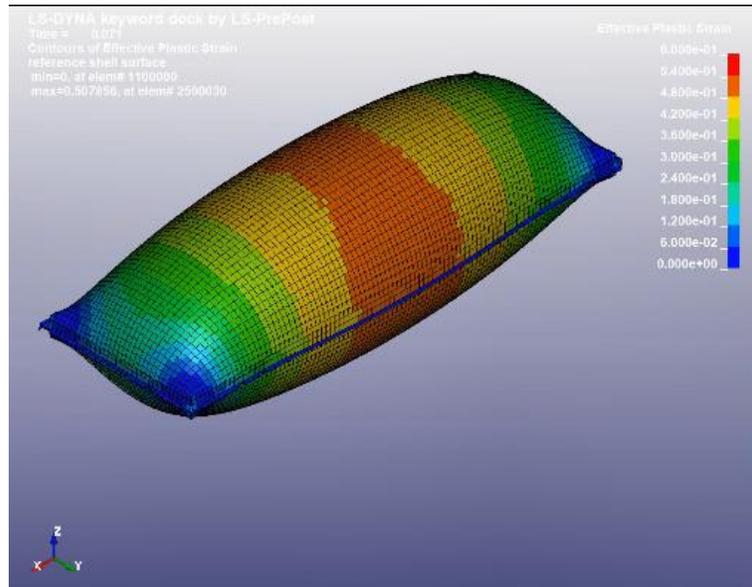
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 - simulation of internal pressure due to gas generation (**LOAD_SEGMENT*)
 - prediction of leakage pressure level



Demonstrator model: pouch cell

*MAT_106 + *MAT_ADD_DAMAGE_GISSMO

- Test of calibrated material model in demonstrator model:
 - simulation of internal pressure due to gas generation (**LOAD_SEGMENT*)
 - prediction of leakage pressure level



Summary

- rupture of pouch foil leads to electrolyte leakage → loss of electrical function
- various external loads are transmitted through the pouch foil
- internal loads are directly acting on pouch foil

- FEM model of cell should represent casing and jelly separately
- need of accurate material models of pouch foils

- pouch foils exhibit temperature and strain rate dependent mechanical behaviour
- homogenized modelling with membrane elements sufficient
- simulation of internal pressure due to gas generation to illustrate mechanical behaviour



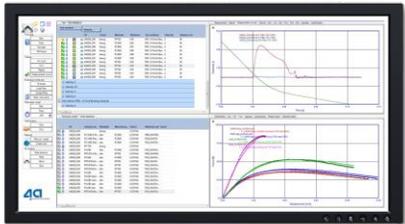
YouTube CHANNEL

MATERIAL
cards



VALIMAT

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α
Anisotropic

Φ_p
Triaxiality

ϵ_p
Damage/Failure

σ_{vm}
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η

ϵ_p

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